## **Supplementary Information**

## Ab-initio Study of Temperature-dependent Piezoelectric and Electronic Properties of Thermally Stable GaPO<sub>4</sub>

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Table S1 Band gaps (in eV) with lattice expansion (LE) effect, phonon vibration (VIB) effect and both of them are given at different temperatures.

	0 K_no ZPR	0 K_with ZPR	200 K	400 K	600 K	800 K	1000 K
LE	4.555	/	4.553	4.546	4.538	4.530	4.523
VIB	/	4.041	3.882	3.610	3.323	3.041	2.770
LE+VIB	/	3.719	3.556	3.266	2.959	2.659	2.374



Fig. S1 Simulations for  $\alpha$ -GaPO<sub>4</sub> at high temperatures (300 – 1100 K) for (a) lattice constant *a*, (b) lattice constant *c* and (c) volume. The red line is obtained by the quasi-harmonic approximation (QHA) method. The blue star symbols represent experimental data<sup>1</sup> and the green ones are obtained by *ab initio* molecular dynamics (AIMD) simulations for 20 ps with a time step of 2 fs.

Table S2 Elastic stability criteria for the mechanically stable crystal GaPO<sub>4</sub>.

(i)	$C_{11} > C_{12}$
(ii)	$2C_{13}^2 < C_{33}(C_{11} + C_{12})$
(iii)	$2C_{14}^2 < C_{44}(C_{11} - C_{12})$
(iv)	$C_{44} > 0$



Fig. S2 Snapshots of  $\alpha$ -GaPO<sub>4</sub> 4×4×2 supercell at (a) 300 K, (b) 700 K and (c) 1000 K after 20 ps AIMD simulations in the isothermal-isobaric (NPT) ensemble using a Langevin thermostat.



Fig. S3 (a) Snapshots of  $\alpha$ -GaPO<sub>4</sub> 3×3×2 supercell excluding the electron-phonon interaction and thus without zero-point renormalization (ZPR), and configurations including electron-phonon interaction at (b) 0 K with ZPR, (c) 200 K, (d) 400 K, (e) 600 K, (f) 800 K and (g) 1000 K.

$$e_{ik} = \begin{bmatrix} e_{11} & -e_{11} & 0 & e_{14} & 0 & 0 \\ 0 & 0 & 0 & 0 & -e_{14} & -2e_{11} \\ 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$
(S1)  
$$C_{kj} = \begin{bmatrix} C_{11} & C_{12} & C_{13} & C_{14} & 0 & 0 \\ C_{12} & C_{11} & C_{13} & -C_{14} & 0 & 0 \\ C_{13} & C_{13} & C_{33} & 0 & 0 & 0 \\ C_{14} & -C_{14} & 0 & C_{44} & 0 & 0 \\ 0 & 0 & 0 & 0 & C_{14} & C_{14} \\ 0 & 0 & 0 & 0 & C_{14} & C_{66} \end{bmatrix}$$
(S2)



Fig. S4 The Hubbard U<sub>eff</sub> dependences of (a) lattice a, (b) lattice c and (c) band gap for GaPO<sub>4</sub>.



Fig. S5 Temperature-dependent (a) elastic constants, (b) Young's modulus, (c) bulk modulus, and (d) Poisson's ratio. The star symbols in (a) represent the experimental data<sup>2</sup>. The hollow circle symbols are calculated by PBEsol+ $U(U_{\text{eff}} = 2 \text{ eV} \text{ for Ga atoms})$ .

Elastic modulus is one of the key properties in materials engineering and mechanics. Studying the effect of temperature on elastic modulus is particularly important for the application of high-temperature materials. According to the generalized Hooke's law, the four material parameters of elasticity in Fig. S5 can describe the reaction of materials when a load is applied, and the energy is a quadratic function of these parameters. The premise of obtaining a stable equilibrium point is that the quadratic form of the energy must be positive and definite, which imposes conditions on the elastic constant. Fig. S5(a) shows the predicted values for  $C_{11}$ ,  $C_{33}$ ,  $C_{14}$ ,  $C_{44}$ ,  $C_{66}$  compared to experimental data at different temperatures. The predicted elastic constants  $C_{1j}$  evolve smoothly with temperature, which comply with the stability criteria (in Table S2), confirming that  $\alpha$ -GaPO<sub>4</sub> remains mechanically stable even at high temperature, while the predicted  $C_{11}$  and  $C_{33}$  deviate from the experimental data when Hubbard U effect is not considered. One can note that the QHA simulation overestimates volume expansion with increasing temperature, as shown in Fig. S1. Since the elastic constants  $C_{11}$  and  $C_{33}$  decrease over volumetric expansion, the overestimated lattice parameters a and c would lead to underestimated  $C_{11}$  and  $C_{33}$  values.

The PBEsol+U method provides finer predictions to the lattice constants as compared to the experimental results (as shown in Table S3). It indeed provides finer predictions of  $C_{11}$  to the experimental value, while having little effect on  $C_{33}$ .

	Functional	PBE	LDA	PBEsol	PBEsol+U	experiment
GaPO4	a = b	5.01	4.82	4.91	4.91	4.92
	С	11.26	10.95	11.10	11.00	11.00
	V	244.66	220.47	232.09	229.86	230.60

Table S3 Lattice constants (Å) and volume (Å<sup>3</sup>) with different functionals (at 0 K) and experimental values of GaPO<sub>4</sub>.

The value of Young's modulus is often required for engineering designs of micro-electromechanical systems (MEMS) technology. Young's modulus can quantify and describe tensile elasticity or the tendency of an object to deform along an axis when opposing forces are applied along this particular axis, reflecting the stiffness of materials. Fig. S5(b) shows that the Young's modulus of GaPO<sub>4</sub> decreases slowly, with a change of only 0.73 GPa from 300 K to 1000 K. Bulk modulus is a vital physical parameter for advanced high-performance materials. It reflects the internal bonding character of atoms and the resistance of the material to volume change. We find that the bulk modulus of GaPO<sub>4</sub> decreases only by 3 GPa upon heating, and its softening resistance is strong. The bulk modulus of GaPO<sub>4</sub> thus presents better thermal stability than  $AIPO_4^3$ . Poisson's ratio is a specific value that describes the lateral deformation of a material. Fig. S4(d) displays that the Poisson's ratio of GaPO<sub>4</sub> is in the range of common materials and similar to that of SiO<sub>2</sub> (0.17)<sup>4</sup>. At elevated temperatures, the Poisson's ratio decreases accompanied by greater brittleness and better resistance to lateral deformation. In general, GaPO<sub>4</sub> turns out to be a typical brittle material with strong compressive strength, suitable for stable application in a high-temperature environment.

Table S4 Piezoelectric constants  $e_{ij}$  (C/m<sup>2</sup>), elastic constants  $C_{ij}$  (GPa) and piezoelectric modulus  $d_{ij}$  (pC/N) of APO<sub>4</sub> (A=B, Al, Ga, In).

Piezoelectric constants (C/m <sup>2</sup> )	BPO <sub>4</sub>	AlPO <sub>4</sub>	GaPO <sub>4</sub>	InPO <sub>4</sub>
$e_{11,i}$	0.37	0.30	0.43	0.62
$e_{11,c}$	-0.25	-0.15	-0.24	-0.28
$e_{11}$	0.12	0.15	0.18	0.35
$e_{14}$	0.03	0.03	0.13	-0.01
$C_{14}$	9.89	11.93	4.27	0.16
$C_{33}$	234.42	87.03	97.73	68.04
$C_{44}$	113.41	42.85	35.25	11.93
$C_{66}$	68.26	28.76	21.33	8.56
$d_{11}$	0.89	2.68	3.98	20.30
$d_{14}$	0.12	-0.78	3.18	-1.26

	Functional	PBE	LDA	PBEsol	PBEsol+U	other <sup>1, 5, 6</sup>
BPO <sub>4</sub>	$e_{11}$	0.11	0.13	0.12	1	0.11
	$e_{14}$	0.01	0.04	0.03	/	0.02
AlPO <sub>4</sub>	$e_{11}$	0.13	0.17	0.15	/	0.14
	$e_{14}$	0.01	0.05	0.03		0.02
GaPO <sub>4</sub>	$e_{11}$	0.17	0.20	0.18	0.17	0.21
	$e_{14}$	0.11	0.11	0.13	0.04	0.10
InPO <sub>4</sub>	$e_{11}$	0.28	0.46	0.35	0.30	1
	$e_{14}$	0.09	-0.63	-0.01	0.01	/

Table S5 Piezoelectric constants  $e_{ij}$  (C/m<sup>2</sup>) with different functionals (at 0 K) and experimental values of APO<sub>4</sub>.



Fig. S6 Bond length for APO<sub>4</sub> (A=B, Al, Ga, In). Pink dots are bonds between A and O, gray dots are bonds between P and O.



Fig. S7 Charge density difference of (a)  $BPO_4$ , (b)  $AIPO_4$ , (c)  $GaPO_4$  and (d)  $InPO_4$ . Isosurfaces level is set as  $\pm 0.027$ , with yellow and blue regions for charge cumulation and depletion, respectively. Red and purple spheres represent O and P atoms, respectively.

Following is about the piezoelectricity of  $\alpha$ -GaPO<sub>4</sub> as the temperature rises to 1000 K. There are two significant angles that link to the structural distortion of the piezoelectric  $\alpha$ -phase in Fig. S8(a). One is the inter-tetrahedral bridging angle  $\theta$  of Ga-O-P, while the other is the tilt angle  $\delta$  that reflects the degree of tetrahedral rotated distortion. The tilting  $\delta$  becomes 0 when transforming to  $\beta$ -phase, accompanied by the disappearance of piezoelectricity. The tilt angle  $\delta$  is also directly related to the bridging angle  $\theta$  with the following relationship<sup>7</sup>:

$$\cos\theta = \frac{3}{4} - \left(\cos\delta + \frac{1}{2\sqrt{3}}\right)^2.$$
(S3)

Fig. S8(b) shows the evolution of bridging angle  $\theta$  and tilt angle  $\delta$  as a function of temperature from 300 K to 1000 K. These two angles weakly depend on temperature. The bridging angle  $\theta$  increases slowly by about 2° as the temperature increases by 700 K. Similarly, the tilt angle  $\delta$  lowers slowly as a function of temperature, indicating that the geometry of  $\alpha$ -GaPO<sub>4</sub> remains distorted at high temperatures and is thus thermally stable. This feature of  $\alpha$ -GaPO<sub>4</sub> is different from  $\alpha$ -SiO<sub>2</sub>, whose tilt angle  $\delta$  drops fast when the temperature rises<sup>8</sup>. Therefore,  $\alpha$ -GaPO<sub>4</sub> crystal has far more profound high-temperature thermal stability than  $\alpha$ -SiO<sub>2</sub> and is suitable to work in a wide temperature range.



Fig. S8 (a) The inter-tetrahedral bridging angle  $\theta$  of Ga-O-P and the tilt angle  $\delta$  related to the rotation angle between  $\alpha$ -GaPO<sub>4</sub> and  $\beta$ -GaPO<sub>4</sub>. The green and gray tetrahedral are GaO<sub>4</sub> and PO<sub>4</sub>, respectively. (b) Dependence between the calculated angles ( $\theta$  and  $\delta$ ) and the temperature, the star symbols are experimental data of  $\delta^8$ . (c) Piezoelectric modulus  $d_{11}$  and  $d_{14}$  as a function of the temperature. (d) The temperature dependence of the electromechanical coupling coefficient  $k_{11}$  and  $k_{14}$ . The solid points are calculated by PBEsol without Hubbard U, and the hollow circle is calculated by PBEsol+ $U(U_{eff} = 2 \text{ eV})$ .

The degree of structural distortion has a direct impact on piezoelectric properties. The crystal of  $\alpha$ -GaPO<sub>4</sub> has only two independent piezoelectric constants displayed in Equation S1:  $e_{11}$  and  $e_{14}$ . Piezoelectric modulus  $d_{ij}$  reflects the ability to transform between the mechanical and electrical energy. To investigate the piezoelectric behavior during the temperature change, we calculate  $d_{ij}$  based on first principles and QHA, from which  $d_{ij}$  can be obtained through the thermodynamic relationship between  $e_{ik}$ and  $S_{kj}$  matrices. The elastic compliance tensor  $S_{kj}$  is the inverse matrix of elastic constants  $C_{kj}$  (Equation S2), and relates to the deformation produced by the application of a stress. Eventually,  $d_{11}$  and  $d_{14}$  can be expressed as:

$$d_{11} = e_{11}(S_{11} - S_{12}) + e_{14}S_{14}$$
(S4)

$$d_{14} = 2e_{11}S_{14} + e_{14}S_{44}. \tag{S5}$$

The  $d_{11}$  and  $d_{14}$  values as a function of temperature are reported in Fig. S8(c).  $d_{11}$  is almost independent from temperature and the general trend is consistent with experiment, although our results

are about 16% smaller than the measured data<sup>9</sup>.  $d_{14}$  decreases slightly from 2.0 pC/N to 1.5 pC/N over this temperature interval, which agrees well with the experimental value. The piezoelectric modulus  $d_{11}$ and  $d_{14}$  are also calculated by PBEsol +  $U(U_{eff} = 2 \text{ eV})$ , which deviate significantly from the experimental results.

The electromechanical coupling coefficient  $k_{ij}$  defined as  $k_{ij}=d_{ij}/(\varepsilon_{ii}S_{jj})^{-1/2}$  is another important indicator of piezoelectric materials, which suggests their ability to convert electrical energy into mechanical quantities and vice versa and whether it is suitable for designing energy harvesting and sensing transducers<sup>10</sup>. GaPO<sub>4</sub> possesses more advantages compared with quartz, such as higher  $d_{11}$  and  $k_{11}$ , and higher critical temperature up to 1206 K, at which temperature an irreversible transformation into a cristobalite-like phase occurs. Therefore, it is an excellent material for use as a pressure transducer and other functional applications that involve harsh high-temperature environments.

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