

Supplementary material for the paper

Title: The influence of surface chemistry of activated carbons on adsorption and freezing/melting processes

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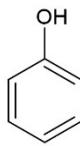
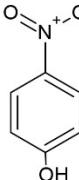
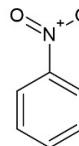
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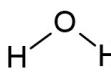
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Table S1. Physicochemical properties of adsorbates.

Compound name	Phenol (P)	4-Nirophenol (4-NP)	Nitrobenzene (NB)
Molecular formula	C ₆ H ₆ O	C ₆ H ₅ NO ₃	C ₆ H ₅ NO ₂
Chemical formula*			
Molecular weight (g/mol)	94.11	139.11	123.11
Solubility in water (g/100 mL at 20 °C)	8.3	1.6	0.19
Solubility in cyclohexane (g/100 mL at 20°C)	1.5	<0.01	15
Ionization constant (pKa)	9.99	7.15	-
Melting point (°C)	40.5	113.0	5.7
Boiling point (°C)	181.7	210.9	279.0

*The molecule structures of adsorbate drawn up in ChemSketch/ACDLabs software (Toronto, Canada, USA)

Table S2. Physicochemical characteristics of diluents.

Compound name	Water (W)	Cyclohexane (CH)
Molecular formula	H ₂ O	C ₆ H ₆
Molecular weight (g/mol)	18.02	84.16
Density (g/mL at 20 °C)	0.9982	0.7785
Polarity	Polar	Unpolar
Dielectric constant (20 °C)	80.1	2.02
Dipole moment (D)	1.84	0.00
Melting point (°C)	0	6.5
Boiling point (°C)	100	80.7
Chemical formula*		

*The molecule structures of diluents drawn up in ChemSketch/ACDLabs software (Toronto, Canada, USA)

Equations:

First-Order Equation and Pseudo-First-Order Equation (FOE and PFOE)

$$\ln(c_{eq} - c) = \ln(c_{eq} - c_o) - k_1 t \quad \text{or} \quad \ln(a_{eq} - a) = \ln a_{eq} - k_1 t \quad (\text{S1})$$

where c is the temporary concentration, a is the actual adsorbed amount, the o and eq subscripts are connected to the initial and equilibrium states, k_1 is the adsorption rate coefficient

Second-Order Equation and Pseudo-Second-Order Equation (SOE and PSOE)

$$a = a_{eq} [k_2 t / (1 + k_2 t)] \quad (\text{S2})$$

or $t/a = (1/a_{eq})(1/k_2 + t)$ and $a = a_{eq} [k_2 t / (1 + k_2 t)]$

where $k_2 = k_{2a} \cdot a_{eq}$ and k_{2a} are the rate coefficients for pseudo-second-order kinetics^{17,18}

1,2-Mixed-Order Equation (MOE)

$$F = a/a_{eq} = \frac{1 - \exp(-k_1 t)}{1 - f_2 \exp(-k_1 t)} \quad \text{or} \quad \ln\left(\frac{1 - F}{1 - f_2 F}\right) = -k_1 t \quad (\text{S3})$$

where F is the relative adsorption progress in time, $f_2 < 1$ is the normalized share of the second-order process in the kinetics. In special cases, the MOE equation may be degraded to the simple kinetic equations of the first ($f_2=0$) and the second-order ($f_2=1$) type

Fractal-Like MOE Equation (f-MOE)

$$F = \frac{1 - \exp(-k_1 t)^p}{1 - f_2 \exp(-k_1 t)^p} \quad (\text{S4})$$

Multi-Exponential Equation (m-exp)

$$c = (c_o - c_{eq}) \sum_{i=1}^n f_i \exp(-k_i t) + c_{eq} \quad \text{or} \quad c = c_0 - c_o u_{eq} \sum_{i=1}^n f_i [1 - \exp(-k_i t)] \quad (\text{S5})$$

where i is the term of the m-exp equation, k_i is the rate coefficient and $u_{eq}=1-c_{eq}/c_o$ is the relative loss of adsorbate from the solution

Intraparticle Diffusion Model (IDM, Crank)

$$F = 1 - \frac{6}{\pi^2} \sum_{n=1}^{\infty} \frac{1}{n^2} \exp\left(\frac{-\pi^2 \cdot n^2 \cdot D_a \cdot t}{r^2}\right) \quad (\text{S6})$$

where r is the radius of the adsorbent particle, D_a is the effective diffusion coefficient:

$$D_a = \frac{D}{\tau_p \cdot (1 + \rho \cdot K_H \cdot \varepsilon_p)} \quad (\text{S7})$$

where D is the molecular diffusion coefficient, τ_p – the dimensionless pore tortuosity factor, ρ is the particle density, ε_p is the particle porosity, K_H – the Henry adsorption constant

Pore Diffusion Model (PDM, McKay)

$$\frac{dF}{d\tau_s} = \frac{\frac{1}{3} (1 - u_{eq} \cdot F) \cdot (1 - F)^{\frac{1}{3}}}{\frac{1}{1 - B \cdot (1 - F)^{\frac{1}{3}}}} \quad (\text{S8})$$

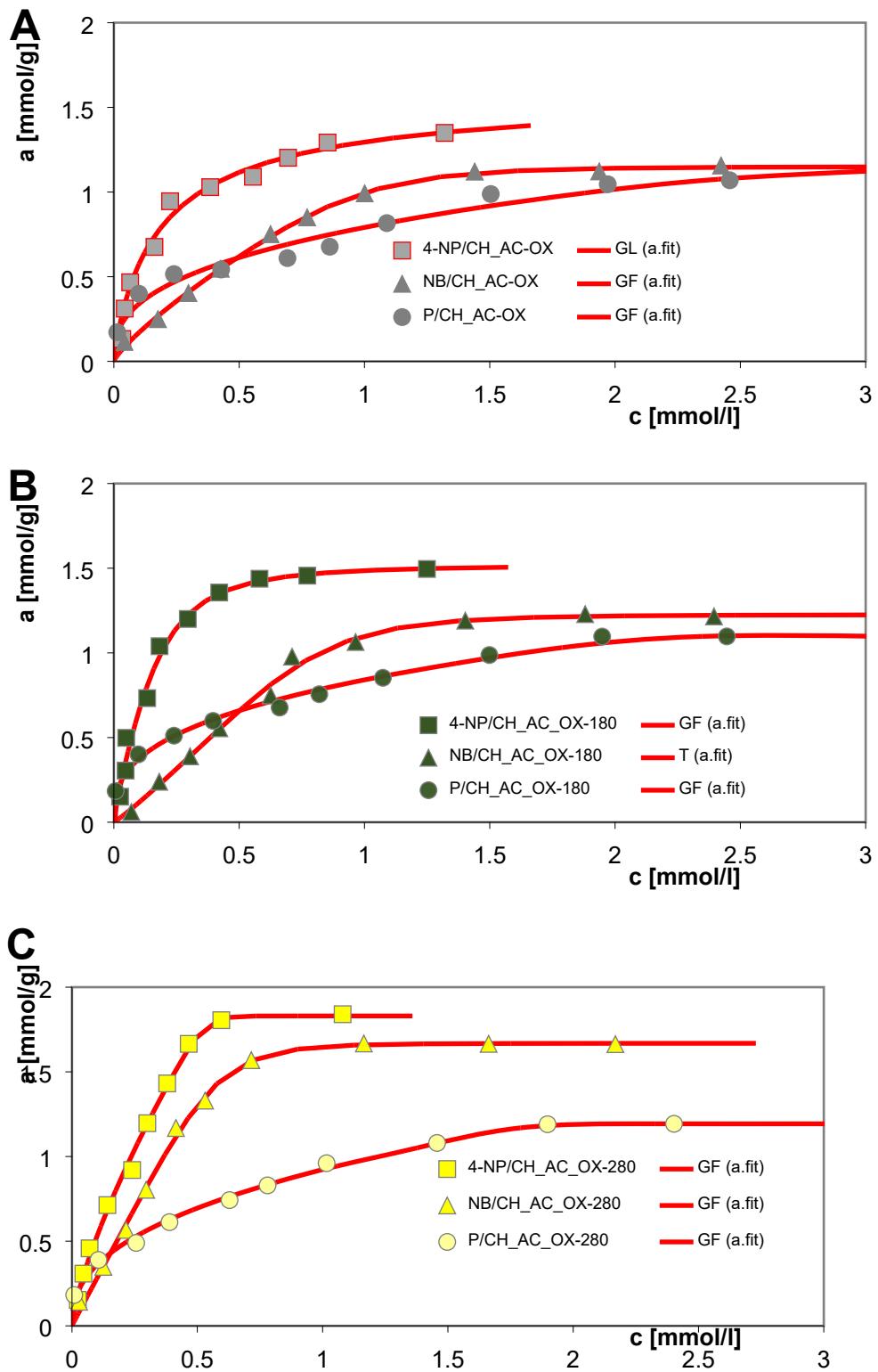
where u_{eq} is the relative adsorbate loss, the parameter $B = 1 - 1/B_i$, where $B_i = K_f/D_p$ is the Biot number, D_p is the pore diffusion coefficient, K_f is the external mass transfer coefficient, τ_s is the undersized model time:

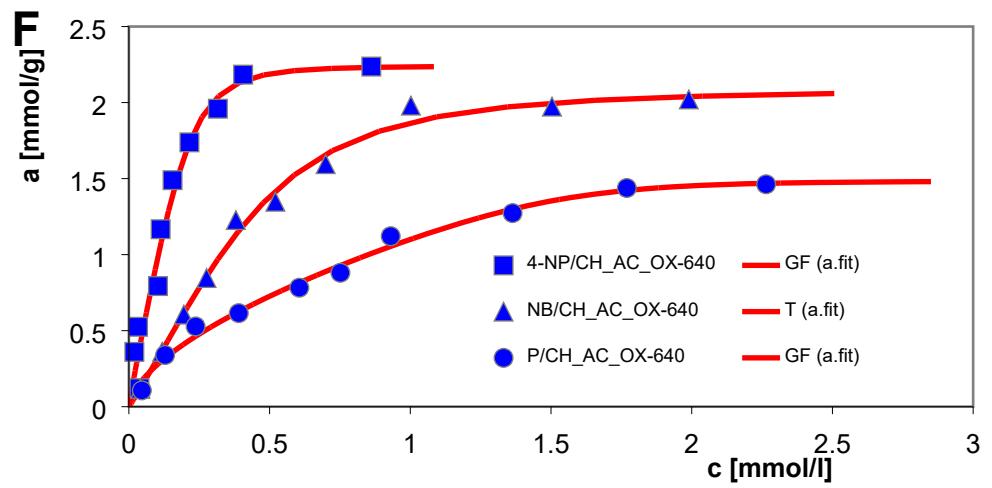
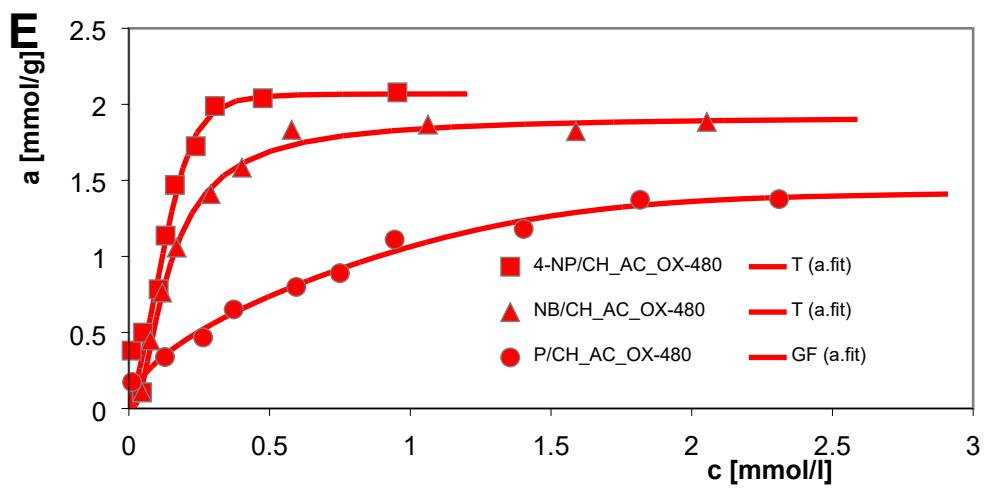
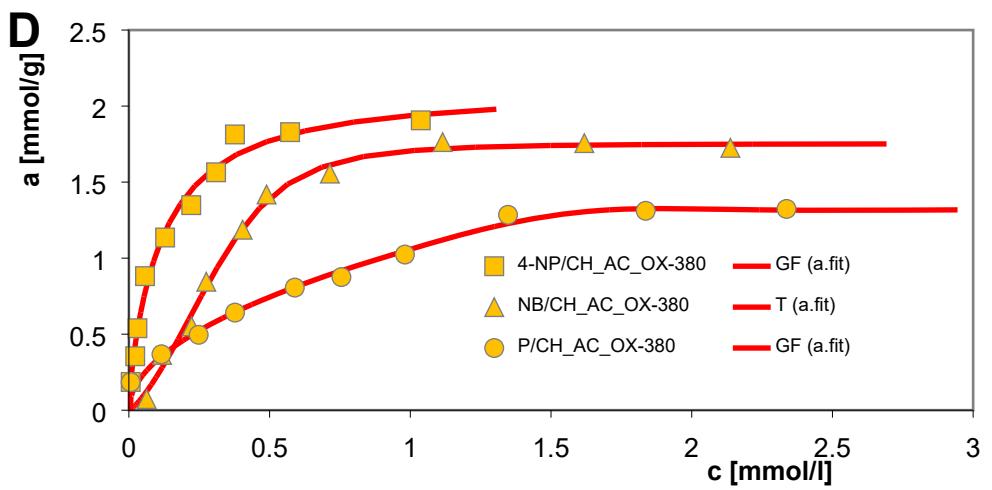
$$\tau_s = \frac{1}{6 \cdot u_{eq}} \left\{ \left(2B - \frac{1}{b} \right) \cdot \ln \left[\left| \frac{x^3 + X^3}{1 + X^3} \right| \right] + \frac{3}{a} \ln \left[\left| \frac{x + X}{1 + X} \right| \right] \right\} + \left\{ \arctan \left(\frac{2 - X}{X \cdot \sqrt{3}} \right) \right\} - \arctan \left(\frac{2 \cdot x - X}{X \cdot \sqrt{3}} \right) \quad (\text{S9})$$

(S10)

$$x = (1 - F)^{\frac{1}{3}}, b = \left(\frac{1}{1 - u_{eq}} \right)^{\frac{1}{3}}$$

where





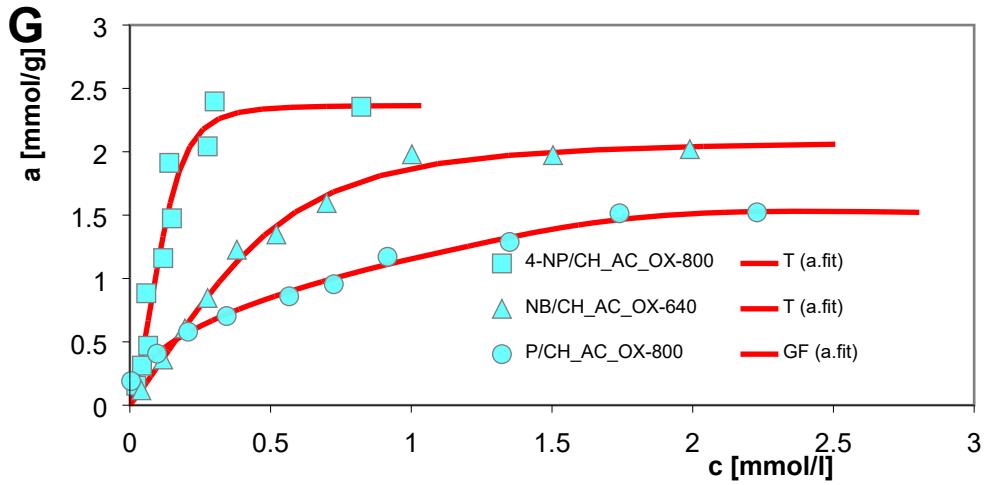


Figure S1. The isotherms of 4-NP, NB, and P adsorption from cyclohexane solutions on AC-OX (A), AC-OX-180 (B), AC-OX-280 (C), AC-OX-380 (D), AC-OX-480 (E), AC-OX-640 (F), and AC-OX-800 (G).

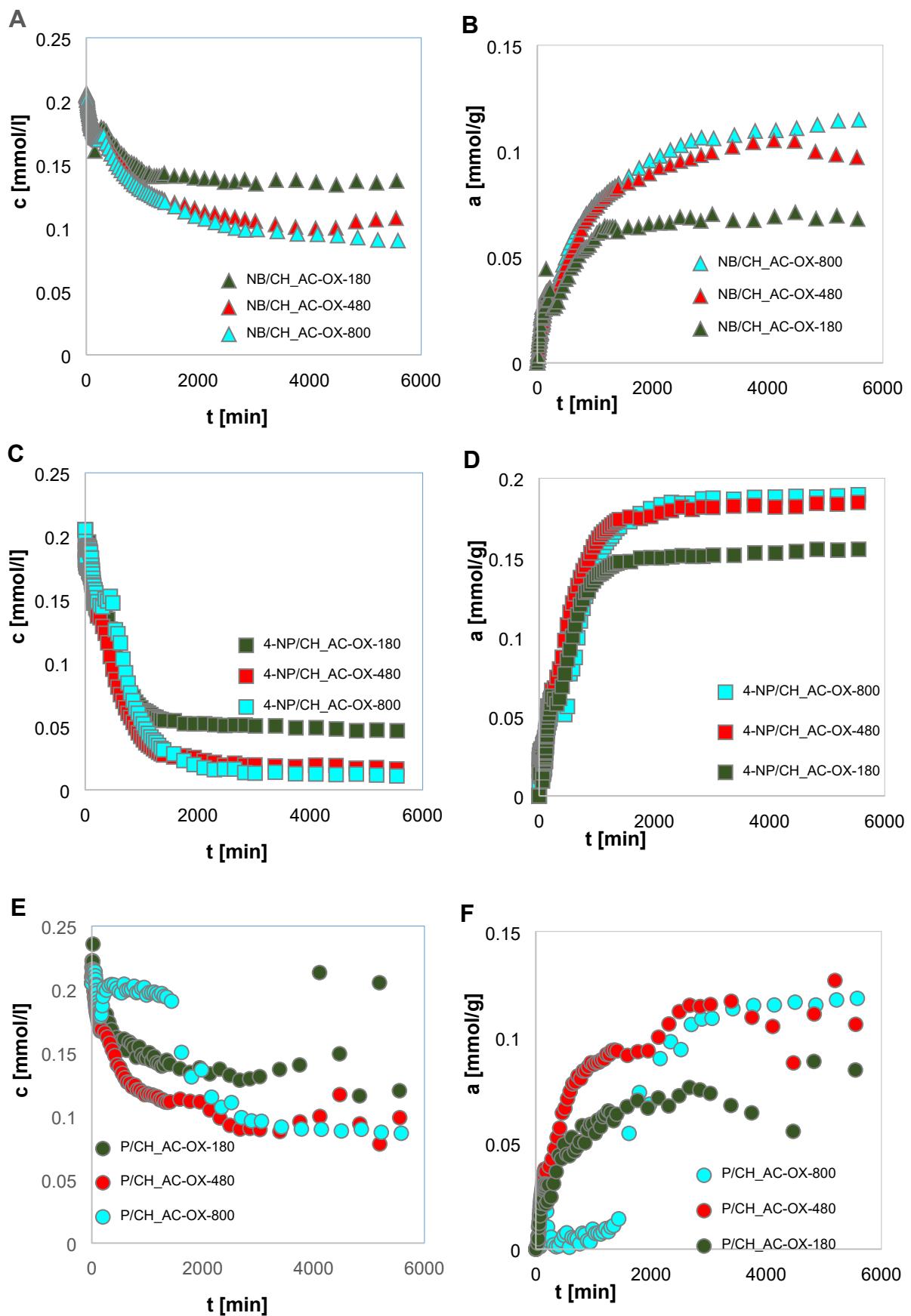


Figure S2. Adsorption kinetics for NB (A-B), 4-NP (C-D), and P (E-F) on AC-OX-180, AC-OX-480, and AC-OX-800 presented as changes in concentration over time (A, C, E) and changes in adsorption over time (B, D, F).

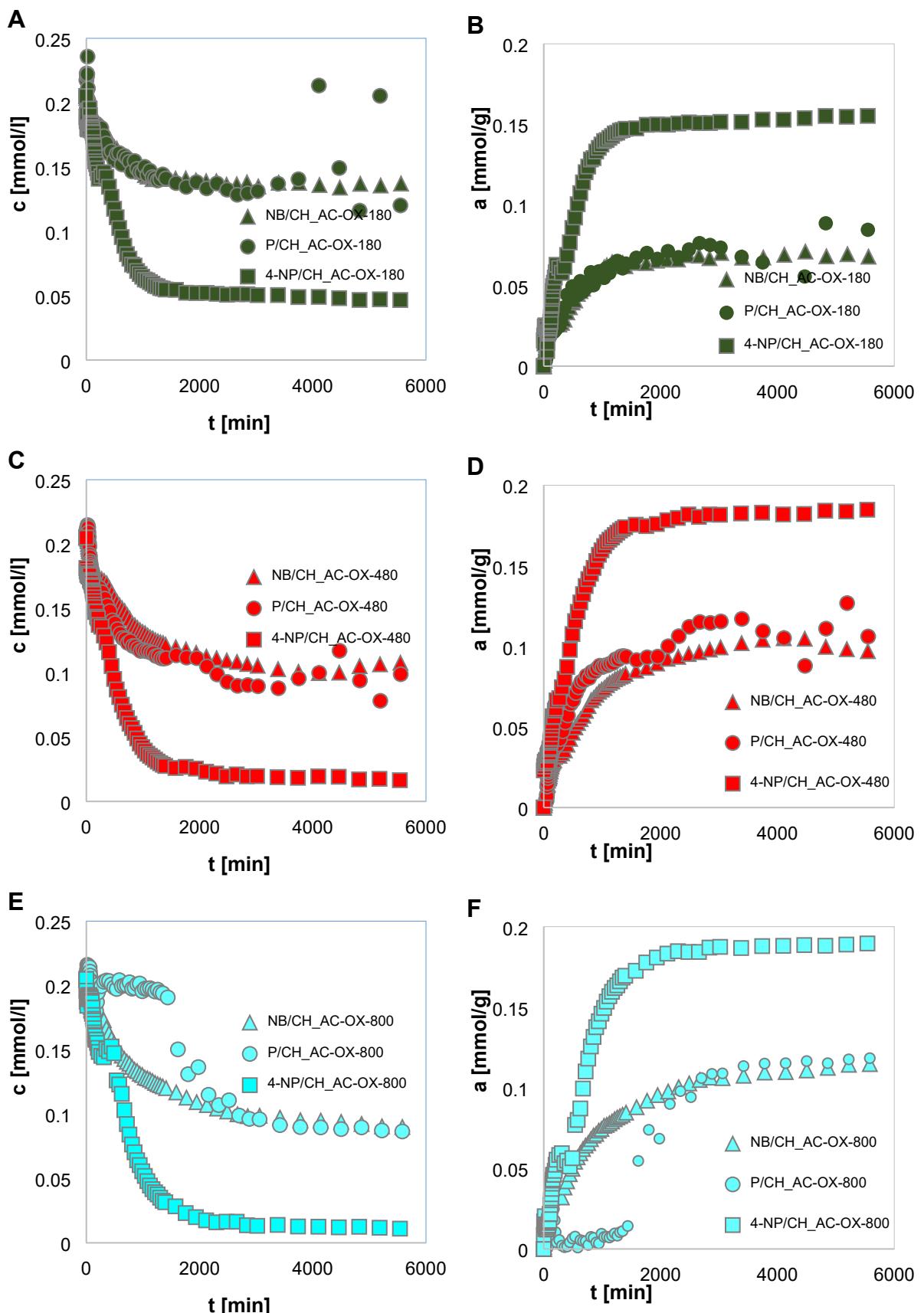


Figure S3. Adsorption kinetics for NB, 4-NP and P on AC-OX-180 (A-B), AC-OX-480 (C-D) and AC-OX-800 (E-F) presented as changes in concentration over time (A, C, E) and changes in adsorption over time (B, D, F).

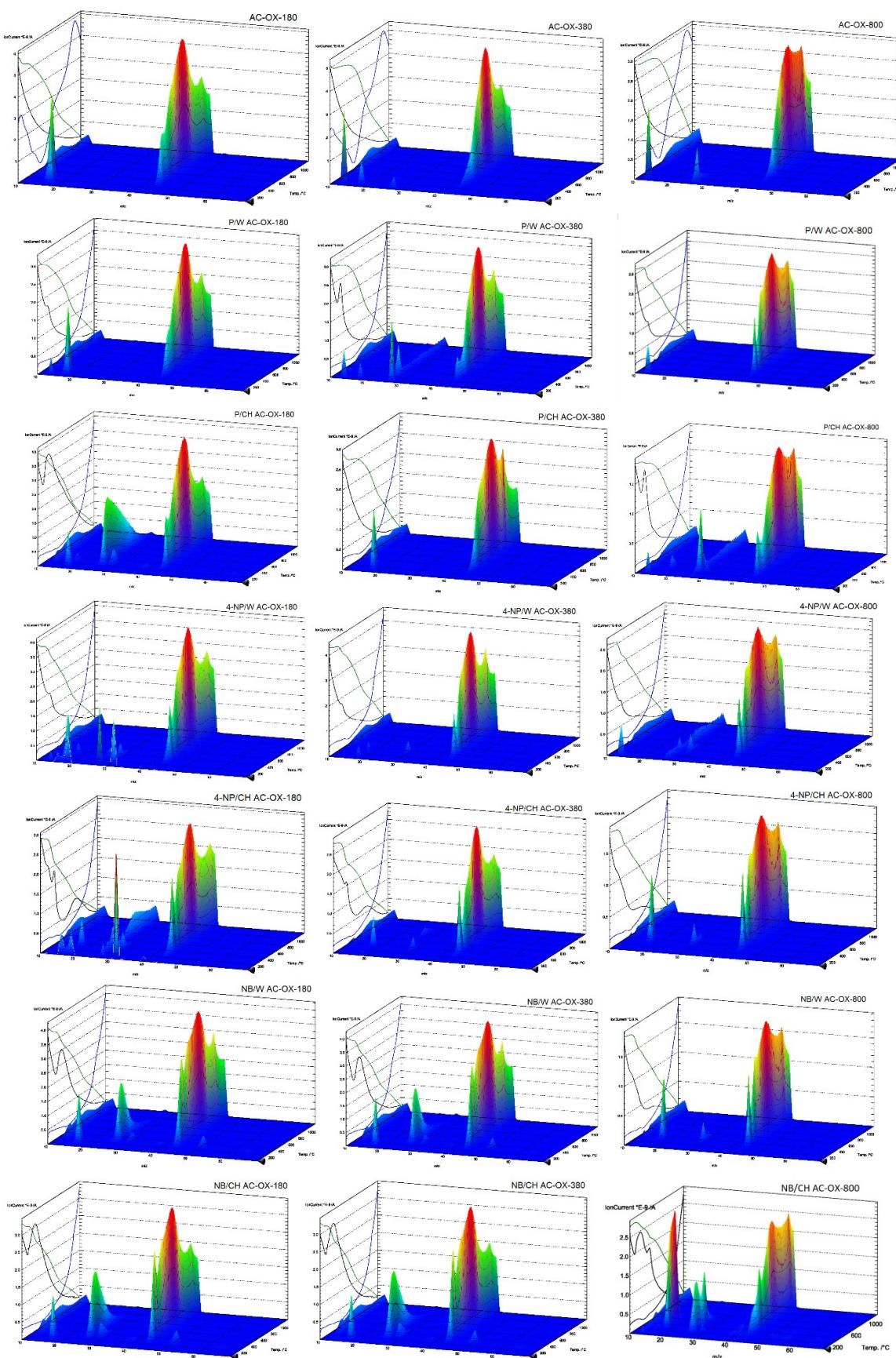
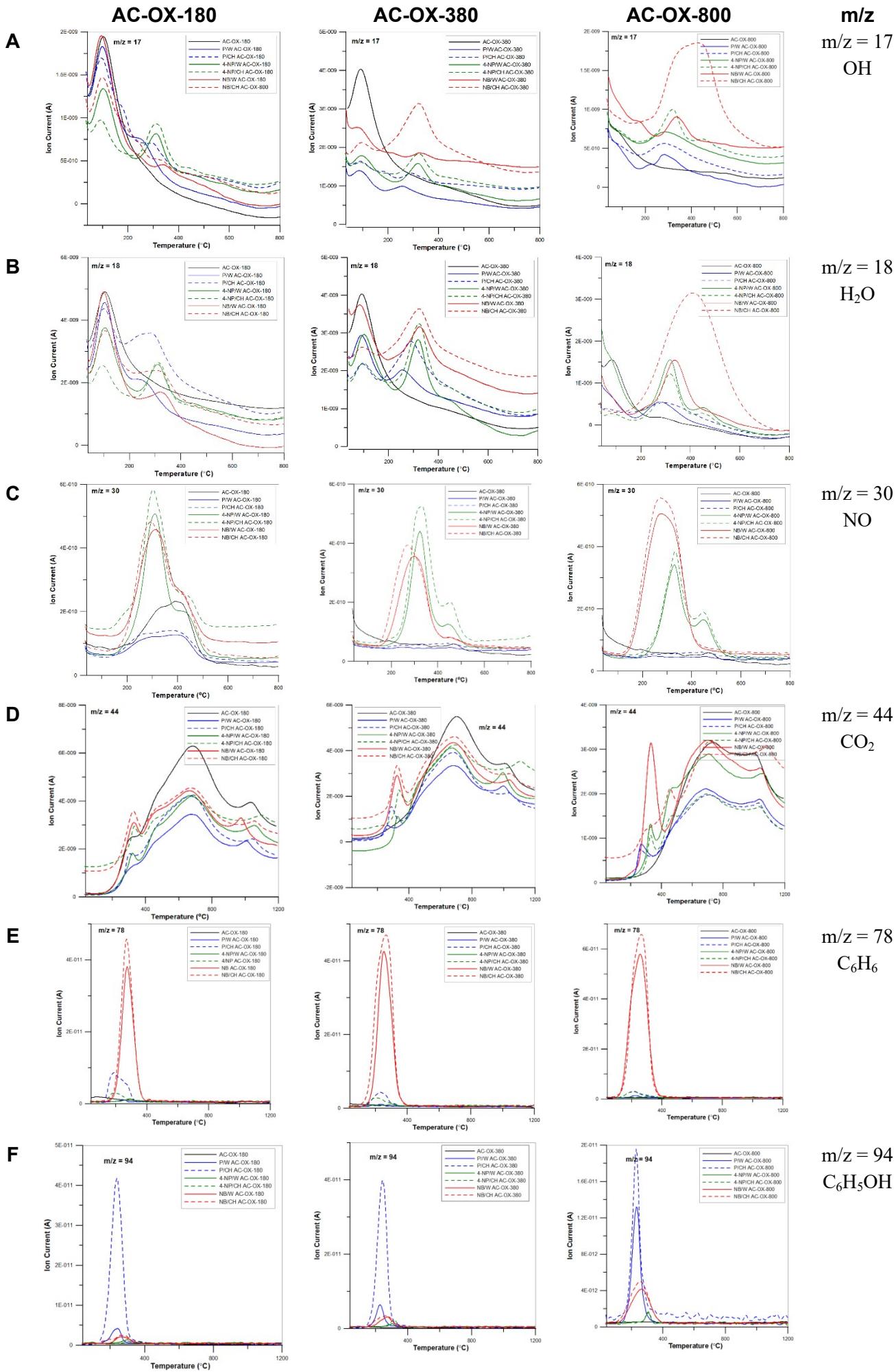


Figure S4. 3D MS profiles of decomposition of AC-OX-180, AC-OX-380 and AC-OX-800 samples.



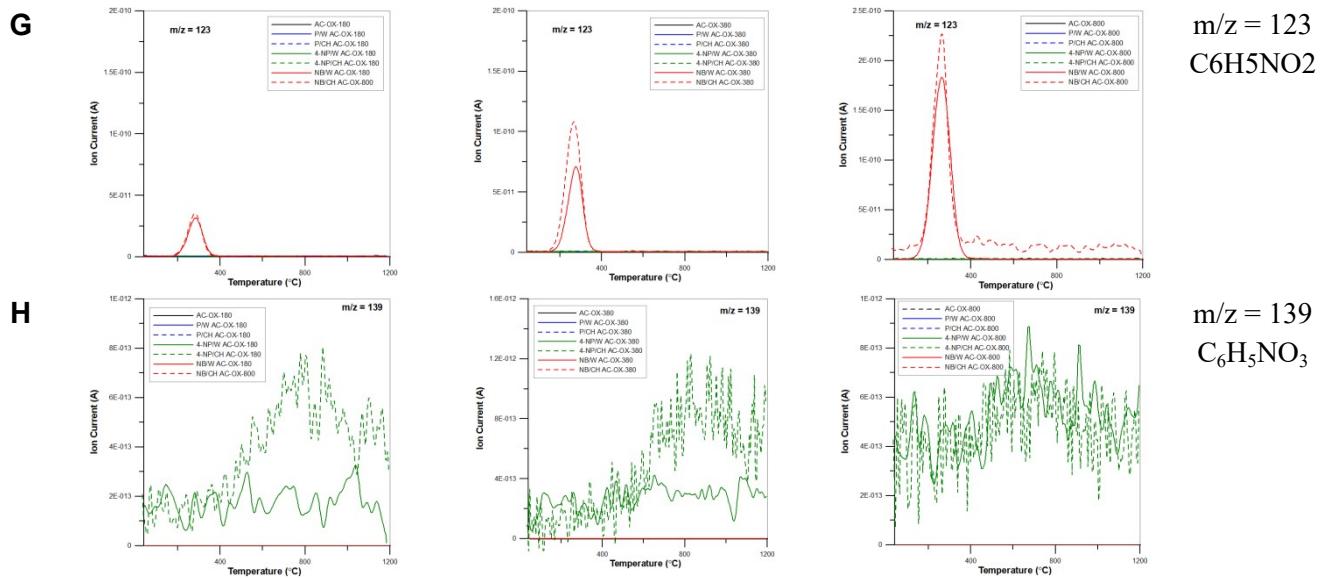


Figure S5. MS gaseous profiles registered during the thermal decomposition of AC-OX-180, AC-OX-380, and AC-OX-800 ($m/z = 17$ (A), $m/z = 18$ (B), $m/z = 30$ (C), $m/z = 44$ (D), $m/z = 78$ (E), $m/z = 94$ (F), $m/z = 123$ (G), $m/z = 139$ (H)) loaded with P/W and P/CH, 4-NP/W and 4-NP/CH, and NB/W and NB/CH, and modified ACs without solutes as a reference.