# Supplemental Information

# Amphiphilic Engineering of MoS<sub>2</sub>-g-C<sub>3</sub>N<sub>4</sub> Nanocomposites into a Mangrove-Inspired Cascade System for Sustainable Drinking Water Production

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### **1.** Experimental Section

#### **1.1 Materials characterizations**

SEM images were acquired using an S-4800 field-emission scanning electron microscope (Hitachi, Japan) at magnifications ranging from 2500 to 100,000. The morphology and structure of the specimen were examined using a JEM-2100 transmission electron microscope (TEM) operating at an acceleration voltage of 200 kV. Analysis of surface elements and functional groups on the adsorbent was conducted using X-ray photoelectron spectroscopy (XPS, ESCALAB 250Xi) with resolutions of 0.48 eV (Ag 3d5/2) and 0.68 eV (C 1s), respectively. UV-visible absorption spectra were recorded using the Beijing Puxi T6 New Century UV-visible spectrophotometer. AFS-933 atomic fluorescence photometer and ICP-OES were used to measure the Hg<sup>2+</sup>, Cu<sup>2+</sup>, Pb<sup>2+</sup>, Cd<sup>2+</sup>concentration in the solution.

#### **1.2 Adsorption experiments**

The static adsorption capacity of MoG composite was evaluated by analyzing the reduction of cationic dye Rhodamine B, anionic dye Congo Red and Hg<sup>2+</sup> in aqueous solution. In the context of static adsorption investigations, a quantity of 10 mg of the adsorbent was introduced into 10 mL of distinct contaminant solutions characterized by initial concentrations ranging from 10 to 500 mg L<sup>-1</sup>, and the system was allowed to equilibrate for a duration of 2 hours. Subsequently, the remaining dye content within the solution was quantified using ultraviolet spectroscopy, while the concentration of Hg<sup>2+</sup> was ascertained through atomic fluorescence spectroscopy. Furthermore, the impact of varying contact durations (0-120 min) as well as temperatures (25-65 °C)

were methodically explored, while maintaining a constant dye concentration of 500 mg  $L^{-1}$ . The adsorption capacity  $q_t$  (mg/g) and removal rate (%) were calculated according to the following equation.

$$Q_t = \frac{(c_0 - c_t)}{m} \times V$$
 (1)

$$\eta = \frac{C_0 - C_t}{C_0} \times 100\%$$
 (2)

Where  $C_0$  is the initial solution concentration (mg g<sup>-1</sup>), and *Ct* is the solution concentration at time t, *V* is the volume of solution (L) and *m* is the weight of MoG (g).

#### 1.3 Evaporation rate measurement via solar simulator

In order to quantify the real-time weight variation of water throughout the solar-driven evaporation process, a beaker containing water was positioned atop a precision balance accurate to four decimal places. This setup allowed for the assessment of both the evaporation rate and solar-thermal conversion efficiency. A segment of aerogel was positioned on the water's surface. Utilizing a 300 W xenon lamp coupled with an AM 1.5 G filter as the solar illumination source, the light intensity was measured employing a robust light photometer. The simulated solar irradiance (1000 W m<sup>-2</sup>) was directed perpendicularly onto the floating aerogel. The steam generation efficiency ( $\eta$ ) was also employed as a metric to gauge the desalination efficacy of the MoG aerogel, and it can be evaluated using the subsequent formula.<sup>1</sup>

$$\eta = \frac{kh_{LV}}{C_{opt} \times q_i}$$
(3)

where k is the evaporation rate,  $h_{LV}$  is the enthalpy of water evaporation (2444 J/g),  $C_{opt}$  is the optical concentration and  $q_i$  is the normal solar irradiation (100 mW cm<sup>-2</sup>).<sup>2</sup>

#### **1.4 Energy calculation**

In an effort to explain the extremely efficient utilization of the solar energy by the MoG evaporator, we conducted an in-depth analysis of energy losses using the following equation<sup>7</sup>:

$$Q_{sun} = Q_{eavp} + Q_{loss} = S_{eavp} D_a h_{fg} \left( C_{sat}(T_s) - \oint_{\infty} C_{sat}(T_{\infty}) \right) + A h_{loss} \Delta T$$
(4)

$$A\partial q_{solar}^{"} = S_{eavp} D_a h_{fg} \Delta c + A\varepsilon \sigma \left(T_s^{4} - T_{\infty}^{4}\right) + Ah_{conv} + \Delta T + \frac{\Delta T}{\frac{1}{S_{cond}K_1} + \frac{t_s}{AK_{wick}}}$$
(5)

In the equation (4), where  $S_{evap}$ , Da, and A are the evaporative shape factor, vapor mass diffusivity in air, area of the evaporator, respectively.  $C_{sat}(T_s)$  and  $C_{sat}(T_{\infty})$  are vapor saturation concentrations at Ts and  $T_{\infty}$ , respectively.  $\oint_{\infty}$  is the far-field relative humidity.

In the equation (5), where  $\partial$ ,  $\varepsilon$ ,  $\sigma$ ,  $h_{conv}$ ,  $K_1$ , and  $K_{wick}$  are the evaporator solar absorptance, evaporator infrared emissivity, Stefan–Boltzmann constant, convective heat loss coefficient, water thermal conductivity, and effective thermal conductivity of the capillary wick, respectively.  $S_{cond} = 2D$  is the conductive shape factor for a circular-disk evaporator.  $h_{conv} = 1/(1/h_a + 1/h_c)$  includes the contributions of both the heat transfer coefficient of air ambient (h<sub>a</sub>) and convection cover (h<sub>c</sub>).

For the MoG evaporator,  $A_{top}$  is 4 cm<sup>2</sup>,  $T_{top}$  is 35.8 °C,  $A_{side}$  is 4 cm<sup>2</sup>, and  $T_{side}$  is 30.5 °C, T<sub>environment</sub> is the ambient temperature (25 °C),  $\varepsilon$  is emissivity of the absorbing surface (~0.98),  $\sigma$  is the Stefan-Boltzmann constant (5.67× 10<sup>-8</sup> W m<sup>-2</sup> K<sup>-4</sup>), h is convection heat transfer coefficient (assumed to be 5 W m<sup>-2</sup> K<sup>-1</sup>), Since the side evaporation surface has a lower temperature than the environment temperature, it could gain energy from the environment. According to the above equation, for the MoG evaporator, the radiation loss from the top evaporation surface was estimated to be 0.0254 W, the radiation energy loss of the side evaporation surface was 0.0211 W, while radiation energy gain of the cotton side evaporation surface from surrounding environment was 0.0235 W; Convection loss from the top evaporation surface was estimated to be 0.0198 W, convection loss from the side evaporation surface was estimated to be 0.0176 W and convection energy gain of the MoG-based aerogel side evaporation surface from surrounding environment was estimated to be 0.0873 W.

Therefore, the evaporator has a net energy gain of 0.0269 W from the environment."

#### 1.5 Photothermal antibacterial tests

Bacteria Escherichia coli (E. coli) was cultured in Luria-Bertani (LB) liquid medium at 37 °C for 6 hours. Subsequently, the culture was dispersed using glass beads and diluted by a factor of  $10^5$  with LB medium. Then, 100 microliters of the diluted E. coli solution were applied to coat a Petri dish. The dish was placed under 1 sunlight for 60 minutes, thereafter, the LB solid medium, following the experimental procedure, was cultured at 37 °C for 14 hours. Finally, the size of the antibacterial zone was measured.

#### **1.6 Evaluation of nanofiltration performance**

MoG colloidal solutions were deposited onto nylon substrates using a straightforward vacuum filtration technique. During the vacuum filtration process, the nylon membrane was initially wetted with water and then affixed to the sand core of the suction filtration apparatus using a large holder. Subsequently, a highly dispersed MoG solution was gently poured onto the surface of the nylon membrane, achieving a loading mass of 7.64 mg cm<sup>-2</sup>. The volume of the colloidal solutions (3 mg/ml) was precisely controlled at 50 ml. Simultaneously, a vacuum pump was engaged to facilitate the permeation of the liquid through the porous nylon membrane until no visible liquid remained on the membrane's surface. Each membrane underwent triplicate analyses under identical conditions. The nanofiltration efficacy was evaluated through dead-end filtration experiments involving diverse dyes and Hg<sup>2+</sup> solutions (50 ppm). The concentrations of the feed and permeate were determined using ultraviolet-visible (UV-Vis) spectroscopy, with measurements taken at the respective maximal absorption wavelengths of the six organic dyes.

Filtration characteristics, including water permeability (J, L m<sup>-2</sup> h <sup>-1</sup> bar<sup>-1</sup>) and dye rejection (R, %), were calculated by the following equations:

$$J = \frac{J_W}{\triangle P} = \frac{V}{A \times t \times \triangle P}$$
(6)

Where V is the volume of permeate (L), A is effective membrane area  $(4 \times 10^{-4} \text{ m}^2)$ , t is the permeation time (h), and  $\Delta P$  is the transmembrane pressure (0.8 bar).

$$R_{\%} = \frac{C_f - C_p}{C_f} \times 100 \tag{7}$$

Where  $C_f$  and  $C_p$  are the concentrations of markers in the permeate and retentate solutions.

A synthetic sewage was prepared to mimic a real application scenario to determine the purification ability of the system:<sup>3</sup> a suitable amount of biological and chemical medium, consisting of 80 mg of peptone, 55 mg of meat extract, 15 mg of urea, 14 mg of K<sub>2</sub>HPO<sub>4</sub>, 4 mg of NaCl, 2 mg of CaCl<sub>2</sub>·2H<sub>2</sub>O, and 1 mg of Mg<sub>2</sub>SO<sub>4</sub>·7H<sub>2</sub>O, were dissolved in 500 mL of tap water.

#### 1.7 Cascade system and traditional wastewater treatment process inventory

Cascade system: It is mentioned in the text that the average water evaporation of our cascade system is  $1.32 \text{ kg m}^{-2} \text{ h}^{-1}$ , and the area of the gel evaporator required when the water yield is 5000 L/h is calculated according to equation S6:

Aerogel area(Aa, m<sup>2</sup>)=
$$\frac{Q_e}{Q_a}$$
 (8)

The volume of the gel evaporator is given by equation S7, where the aerogel thickness is assumed to be 1 cm.

Aerogel volume(Av, 
$$m^3$$
)=0.01×Aerogel are (9)

In addition, the average density of MoG loaded on the aerogel is  $200 \text{ kg/m}^3$ , so equation S8 can be used to calculate the total amount of MoG required for a gel evaporator with a water volume of 5000 L/h.

$$MoS_2$$
-g- $C_3N_4$  mass(MoG m, kg)=200×Aerogel volume (10)

The average density of MoG loaded on the membrane is 9.43 kg/m<sup>2</sup>, and the water flux of the membrane is 966 L m<sup>-2</sup> h<sup>-1</sup> bar<sup>-1</sup>, so equation S9 can be used to calculate the total amount of MoG required by the filter membrane when the water volume is 5000 L/h.

MoS<sub>2</sub>-g-C<sub>3</sub>N<sub>4</sub> mass(MoG m, kg)=
$$\frac{Q_e}{L_m} \times 9.43$$
 (11)

By modeling the MoG synthesis process using the ecoinvent v3.5 database, the  $CO_{2e}$  for the production of 1 kg of MoG was calculated.

#### **1.8 Traditional wastewater treatment process**

The traditional process includes pretreatment, conditioning and oxidation, Adsorption, coagulation and filtration. Each step of the process requires the addition of chemical

agents. The environmental benefits of traditional processes are determined by calculating the amount of carbon dioxide generated during the production of the chemical agents. Including FeCl<sub>3</sub>, PAM (polyacrylamide), lime, activated carbon, manganese sand, KDF copper-zinc alloy filter media. The dosage of each chemical agent for each step of the process is known from the literature.

#### **1.9 Janus graphene oxide evaporator inventory:**

Evaporation rate: The reported E.R. was extracted from Fig. 8e from Lin et al. and estimated at a value of 0.74 kg m<sup>-2</sup> h<sup>-1</sup>. This can be used as the true evaporation rate under real sunlight.

In order to achieve a better comparison, we specify that the required area is calculated based on the 1 L/h water discharge rate, which can be calculated according to equation S10.

Janus evaporator area(JEa, m<sup>2</sup>)=
$$\frac{Q_e}{Q_a}$$
 (11)

The volume of the Janus GO evaporator is given by equation S11, where the thickness of the evaporator is assumed to be 1 cm.

Janus evaporator volume(JEv,  $m^3$ )=0.01×Janus evaporator area (12)

In addition, the average density of the Janus GO evaporator is  $280 \text{ kg/m}^3$ , so Equation S7 can be used to calculate the total mass of the gel evaporator at 1 L/h of water.

By modeling the Janus GO evaporator synthesis process using the Ecoinvent v3.5 database, the  $CO_{2e}$  for the production of 1 kg of Janus GO evaporator was calculated.

Similarly, the total mass of other evaporators can also be calculated according to the above method, and the specific parameters are detailed in Table S6.

# Supporting Figures



Figure S1 Schematic diagram for the preparation of MoG using a hydrothermal method.



Figure S2 Size distribution of MoG mesoporous structure (inset is  $N_2$  adsorption-desorption isotherm).



Figure S3 XPS spectra of (a) C 1s, (b) N 1s, (c) Mo 3d and (d) S 2p.

The C 1s XPS spectrum exhibited distinct peaks at ~284.8 eV, corresponding to the graphitic adventitious C-C bond within g-C<sub>3</sub>N<sub>4</sub>. In the N 1s spectrum, three peaks emerged at ~400.6, ~399.6, and ~398.2 eV, attributed to C-NH<sub>x</sub>, N-(C)<sub>3</sub>, and C=N-C functionalities, respectively. Within the S 2p spectrum, the prominent peaks at ~163.08 eV (S  $2p_{1/2}$ ) and ~161.87 eV (S  $2p_{1/2}$ ) signify the presence of the 1 T phase. Two smaller peaks at around 163.68 and 162.5 eV are assigned to the S  $2p_{1/2}$  and S  $2p_{3/2}$  orbitals of the 2 H phase, respectively <sup>4</sup>. To validate the existence of the 1 T phase MoS<sub>2</sub>, the Mo 3d and S 2p XPS spectra were subjected to analysis. Notably, two principal peaks at ~232.3 and ~228.9 eV correspond to Mo<sup>4+</sup> 3d<sub>3/2</sub> and Mo<sup>4+</sup> 3d<sub>5/2</sub> orbitals within the 1 T phase, respectively. Simultaneously, the minor peaks at around 232.6 and 229.5 eV are

indicative of the Mo<sup>4+</sup>  $3d_{3/2}$  and Mo<sup>4+</sup>  $3d_{5/2}$  orbitals within the 2H phase, respectively. Furthermore, an additional peak at ~235.7 eV is attributed to Mo<sup>6+</sup> within MoO<sub>3</sub>, stemming from coordination-induced slight oxidation. The S 2s peak is positioned at ~226.3 eV. It is of significance to highlight that within the S 2p spectrum of MoG, a distinct peak at 164.1 eV signifies the presence of S-C bonds, consistent with existing literature.<sup>5-7</sup> This peak was attributed to the reaction of S atoms with the functional groups and with the edges of g-C<sub>3</sub>N<sub>4</sub>, resulting in a bridge between g-C<sub>3</sub>N<sub>4</sub> and the MoS<sub>2</sub> nano spheres.



**Figure S4** Molecular dynamic simulation of the interaction  $g-C_3N_4$  and rhodamine B. Histograms and estimated densities of the distance between the atoms of rhodamine B and the surface of  $g-C_3N_4$  at 0 (blue), 10 (yellow), and 20 (green) ns respectively.



Figure S5 Molecular dynamic simulation of the interaction  $MoS_2$  and rhodamine B. Histograms and estimated densities of the distance between the atoms of rhodamine B and the surface of  $MoS_2$  at 0 (blue), 10 (yellow), and 20 (green) ns respectively.



Figure S6 (a) Fluorescence spectra of RhB titrated with MoG; (b) Fluorescence spectra of RhB titrated with MoS<sub>2</sub>.



Figure S7 Comparison of adsorption efficiency for different dyes at different concentrations.



Figure S8 Adsorption isotherms of RhB by MoG at different temperatures.

We first investigated the effect of temperature on the adsorption of RhB by MoG, experimental studies were carried out at 298 K, 318 K, 338 K respectively. From the correlation coefficients (R<sup>2</sup>) and fitting curves (Table S1), it was found that the Langmuir model is more suitable to simulate RhB adsorption than the Freundlich model, indicating a monolayer coverage of adsorbents.<sup>8</sup>



**Figure S9** Pseudo-secondary kinetic model for RhB adsorption; ( $C_0 = 500$  ppm; T = 298 K; m adsorbent = 10 mg; V = 10 mL).





The fitting results and kinetic parameters are shown in Table S2. The results from Table S2 show that the linear pseudo-second-order kinetic model, with the highest  $R^2$  (0.9998), is more consistent with the experimental data than the other models.



Figure S11 Adsorption isotherms of  $Hg^{2+}$  by MoG at different temperatures.

To further explore the influence of temperature on mercury ion adsorption by MoG, experimental studies were carried out at 298 K, 318 K, 338 K respectively. The Langmuir and Freundlich adsorption isotherm models are used to fit the experimental data. The values of  $q_m$ ,  $K_L$ ,  $K_F$  and n displayed in Table S3. According to the fitting curve and correlation coefficient ( $R^2$ ), the former  $R^2$  was larger than the latter  $R^2$ , indicating that Langmuir model was more suitable for simulating  $Hg^{2+}$  adsorption than Freundlich model.



Figure S12 Fitting results for pseudo-first-order.



Fig. S13 Fitting results for pseudo-second-order.

Identically, the fitting results and kinetic parameters of kinetic models are shown in Table S4. Obviously, the linear correlation coefficient ( $R^2 = 0.9998$ ) for the pseudosecond-order model is higher than the linear correlation coefficient ( $R^2 = 0.16731$ ) for the pseudo-first-order one. This result indicates that chemisorption is the dominant adsorption process of Hg<sup>2+</sup>.



Figure S14 (a-d) Simultaneous adsorption of  $Hg^{2+}/RhB$  and  $Hg^{2+}/Congo$  red (CR ) by MoG.



**Figure S15** Simultaneous adsorption capacity of RhB, CR, Hg<sup>2+</sup> by MoG at different initial concentrations.

In the context of the RhB-Hg<sup>2+</sup> cationic system, the  $R_{q,RhB}$  values (Fig. S14a) closely approached 1, indicating minimal influence of coexisting Hg<sup>2+</sup> on RhB adsorption. Conversely, the  $R_{q,Hg}^{2+} < 1$  (Fig. S14b), signifying varying degrees of inhibition in Hg<sup>2+</sup> adsorption by RhB. This is because RhB carries a positive charge when dissolved in water, allowing for electrostatic attraction with the negatively charged MoS<sub>2</sub>.<sup>9</sup> Additionally, MoS<sub>2</sub> possesses inherent polarization at its edge active

sites, enabling interactions with specific polar molecules such as RhB. This implies that the binding force between the adsorbent and RhB is greater than that between  $Hg^{2+}$ , resulting in this phenomenon.<sup>10-12</sup>

In the context of the CR-Hg<sup>2+</sup> anionic system, the  $R_{q,CR} \ge 1$  (Fig. S14c) means that the presence of Hg<sup>2+</sup> substantially augmented the CR removal process. Conversely, Hg<sup>2+</sup> adsorption experienced varying degrees of inhibition by CR (Fig. S14d). This phenomenon can be rationalized as follows: CR, a negatively charged anionic dye in aqueous solution, may achieve enhanced adsorption by the formation of a VI-Hg-CR configuration facilitated through Hg<sup>2+</sup> bridgin g.<sup>13</sup> In ternary systems, the adsorption capacity exhibited the sequence of  $RhB > Hg^{2+} > CR$  (Fig. S15a), a trend congruent with outcomes from single-species adsorption investigations. It was worth noting, CR adsorption achieved peak levels before diminishing at higher concentrations, potentially attributable to a reduction in accessible adsorption sites within the ternary milieu. Notably, relative to their respective single adsorption systems, MoG displayed diminished adsorption capacity for these metallic ions. Within the ternary systems, escalating concentrations of metal ions engendered competitive adsorption onto MoG, consequently inducing a decline in removal efficiency. On the basis of the above experimental phenomena, we suspect that the high efficiency of the MoG upon pollutant elimination is due to the synergistic effect of physical adsorption and chemical adsorption. Considering the molecular architectures of RhB and MoG, an electrostatic interaction between RhB and MoG arises. This stems from the cationic nature of RhB and the negative charge carried by MoG within the solution. Furthermore, both RhB and MoG encompass aromatic rings, thus potentially engendering heightened  $\pi$ - $\pi$  interactions. Moreover, the presence of nitrogen atoms in both g-C<sub>3</sub>N<sub>4</sub> and RhB opens the possibility for hydrogen bonding between these constituents. The adsorption of CR by the MoG could be attributed to the open hierarchical structure of the composite.<sup>14</sup> Meanwhile, the adsorption mechanisms of the Hg<sup>2+</sup> on MoG were mainly the chelation between S and Hg on the adsorbent-adsorbate interface as well as precipitation and crystal growth on the surface of the adsorbent.<sup>15</sup>



Figure S16 Example of a large-area MoG/nylon membrane fabricated by vacuum filtration.



**Figure S17** Removal efficiency and water flux of MoG membrane for RhB at different loading levels.



**Figure S18** Separation performance of MoG for mixed dye molecules of Rhodamine B/Congo red (RhB/CR).



**Figure S19** Removal efficiency and water flux of MoG membrane for  $Hg^{2+}$  at different loading levels.



Figure S20 Concentration of heavy metal ions in water after evaporation.



Figure S21 Schematic diagram of the two-stage interconnected system for clean water production.



Figure S22 The UV absorption spectra of dyes in simulated wastewater before and after solar evaporation.

|      | Langmuir              |             |                | Freundlich       |        |                |
|------|-----------------------|-------------|----------------|------------------|--------|----------------|
| Т, К | q <sub>m</sub> , mg/g | $K_L, L/mg$ | R <sup>2</sup> | $K_{\mathrm{f}}$ | n      | $\mathbb{R}^2$ |
| 298  | 777.6347              | 0.03895     | 0.996          | 73.2208          | 2.1487 | 0.958          |
| 318  | 802.170               | 0.05945     | 0.987          | 100.0000         | 2.2321 | 0.951          |
| 338  | 775.789               | 0.09129     | 0.985          | 115.718          | 2.3460 | 0.927          |

Table S1. Parameters for isotherm models for the sorption of RhB on MoG.

 Table S2. Adsorption parameters of RhB.

| C <sub>0</sub> , mg/L | q <sub>m</sub> , mg/g | pseudo-first-order        |                       |         | pseudo-second-order                                   |          |           |
|-----------------------|-----------------------|---------------------------|-----------------------|---------|---|----------|-----------|
|                       |                       | $K_1$ , min <sup>-1</sup> | q <sub>e</sub> , mg/g | $R_1^2$ | K <sub>2</sub> , mg g <sup>-1</sup> min <sup>-1</sup> | qe, mg/g | $R_2^2$   |
| 50                    | 49.8                  | 0.0253                    | 1.2016                | 0.6362  | 0.2580  | 49.5295  | 1.00<br>0 |

**Table S3**. Parameters for isotherms models for the sorption of  $Hg^{2+}$  on MoG.

|      | Langmuir              |                       |                | Freundlich       |        |                |  |
|------|-----------------------|-----------------------|----------------|------------------|--------|----------------|--|
| Τ, Κ | q <sub>m</sub> , mg/g | K <sub>L</sub> , L/mg | R <sup>2</sup> | $K_{\mathrm{f}}$ | n      | $\mathbb{R}^2$ |  |
| 298  | 768.116               | 0.02429               | 0.987          | 39.3228          | 1.9209 | 0.850          |  |
| 318  | 781.476               | 0.00654               | 0.995          | 16.6213          | 1.6349 | 0.971          |  |
| 338  | 923.012               | 0.00365               | 0.996          | 9.9986           | 1.4646 | 0.986          |  |

**Table S4.** Adsorption parameters of  $Hg^{2+}$  ions.

| C <sub>0</sub> , mg/L | q <sub>m</sub> , mg/g | pseudo-first-order        |                       |         | pseudo-second-order                                   |                       |         |
|-----------------------|-----------------------|---------------------------|-----------------------|---------|---|-----------------------|---------|
|                       |                       | $K_1$ , min <sup>-1</sup> | q <sub>e</sub> , mg/g | $R_1^2$ | K <sub>2</sub> , mg g <sup>-1</sup> min <sup>-1</sup> | q <sub>e</sub> , mg/g | $R_2^2$ |
| 100                   | 99.8                  | 0.0253                    | 10.7145               | 0.6362  | 0.0169  | 100                   | 0.999   |

|                         | Molecular<br>weight<br>(g mol <sup>-1</sup> ) | Solute<br>Charge | Chemical structure |
|-------------------------|---|------------------|--------------------|
| Methyl<br>orange (MO)   | 327.33  | -                |                    |
| Malachite<br>green (MG) | 364.91  | +                | • *****            |
| Methyl violet<br>(MV)   | 408.03  | +                |                    |
| Rhodamine B<br>(RhB)    | 479.01  | +                |                    |



# Table S6. Evaporator parameters.

|            | Evaporation rate<br>(kg m <sup>-2</sup> h <sup>-1</sup> ) | Thickness<br>(m) | Mass density<br>(kg/m <sup>3</sup> ) | References |
|------------|---|------------------|--------------------------------------|------------|
| J-PPy      | 0.6175  | 0.01             | 254.7                                | 16         |
| PSHs       | 2.1   | 0.01             | 86.7                                 | 17         |
| COF/GO     | 3.69  | 0.01             | 13.46                                | 18         |
| PDMX/HPP   | 1.08  | 0.016            | 178                                  | 19         |
| PPy-PI NAG | 1.42  | 0.01             | 35.7                                 | 19         |
| MTBs       | 0.68  | 0.01             | 217                                  | 20         |

Table S7. WHO standard for drinking water.

| Heavy mental                              | Mercury | Cadmium | Lead | Copper | Turbidity |
|---|---------|---------|------|--------|-----------|
| WHO Guideline value (mg L <sup>-1</sup> ) | 0.001   | 0.005   | 0.01 | 2      | 5NTU      |

 Table S8. Estimation of materials cost for cascade system.

| Chemicals                          | Vendor           | Price            |         | Materials/<br>device | Price/<br>device |
|------------------------------------|------------------|------------------|---------|----------------------|------------------|
| Thioacetamide                      | Kermel           | 500 g            | \$ 40.3 | 0.135 g              | \$ 0.01          |
| Ammonium molybdate<br>tetrahydrate | Kermel           | 500 g            | \$ 22.8 | 0.175 g              | \$ 0.0008        |
| Melamine                           | Macklin          | 500 g            | \$ 12.8 | 0.0175 g             | \$ 0.0004        |
| Chitosan                           | TCL              | 500 g            | \$ 67.1 | 0.2 g                | \$ 0.03          |
| Nylon membrane                     | Zhejiang<br>Yibo | 1 m <sup>2</sup> | \$ 96   | 0.002 m <sup>2</sup> | \$ 0.192         |
| Acetic acid                        | Kermel           | 500 mL           | \$ 5.8  | 0.2mL                | \$ 0.002         |
| Glutaraldehyde (25%)               | Kermel           | 500 mL           | \$9     | 1 mL                 | \$ 0.018         |
| Operating cost                     |                  | 1 kW h           | \$ 0.05 | 96.08 kW h           | \$ 4.804         |
| Cost of cascade system             |                  |                  |         |                      | \$ 5.22          |

#### Reference

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