

## Supporting Information

Strong yet tough bio-based biomimetic-multiphase composite polyesters  
with superior barrier and chemically closed-loop performance

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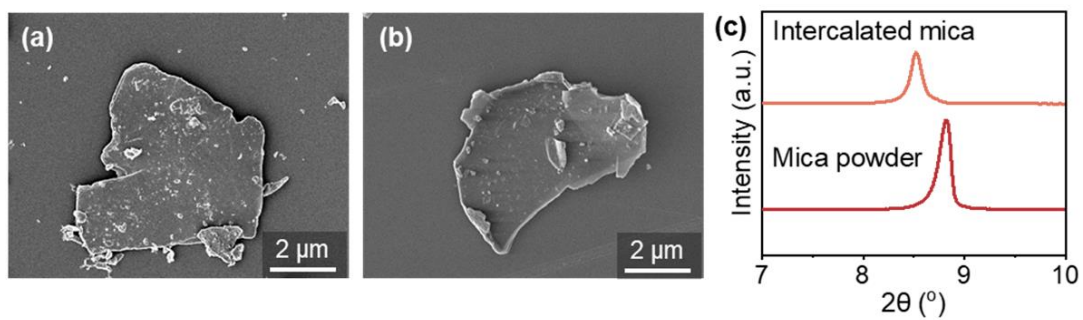
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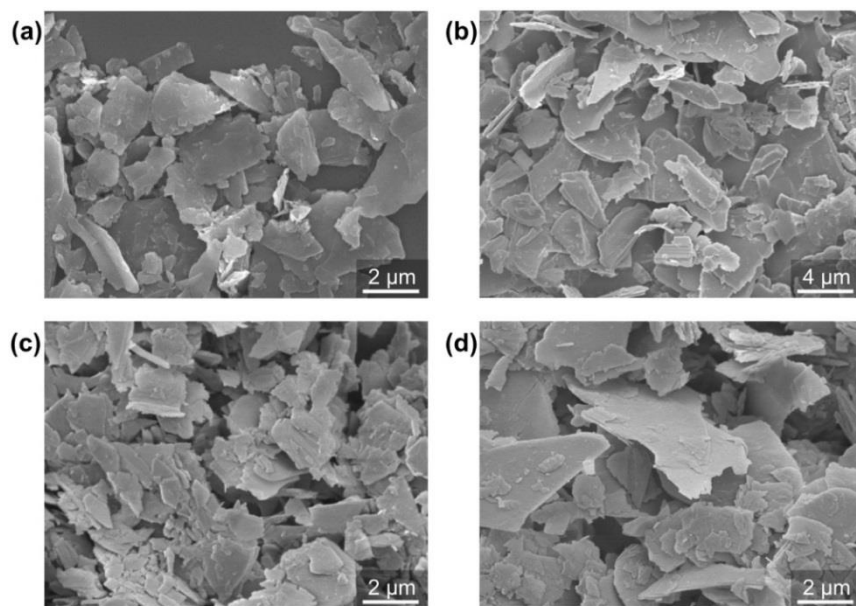
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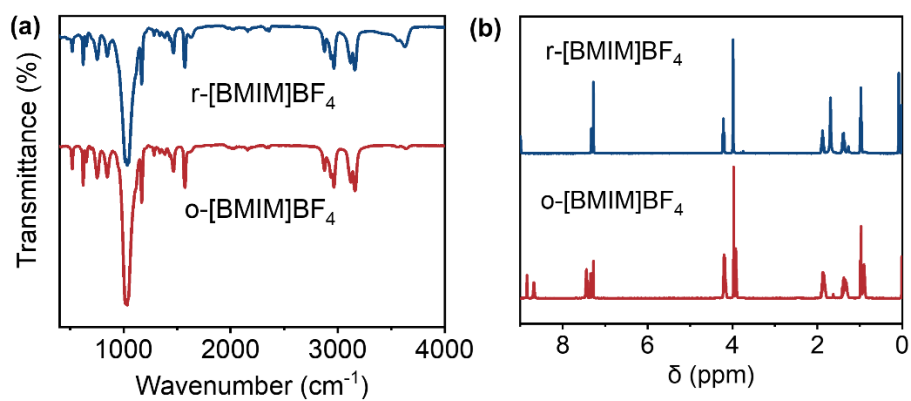
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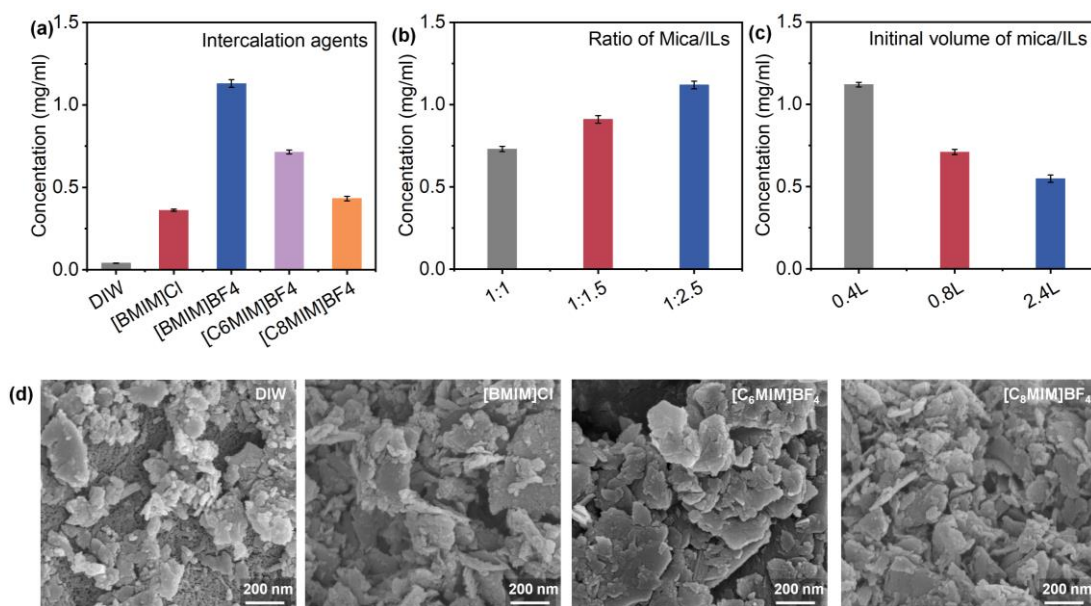
**Figure S1.** SEM images of bulk mica (a) and intercalated mica (b). XRD patterns of mica and intercalated mica (c). Typically, the bulk mica shows compact large block structure. After intercalation by ILs, the thickness of mica became thinner. It can be seen from the XRD results, after intercalation, the layer spacing of mica became larger.



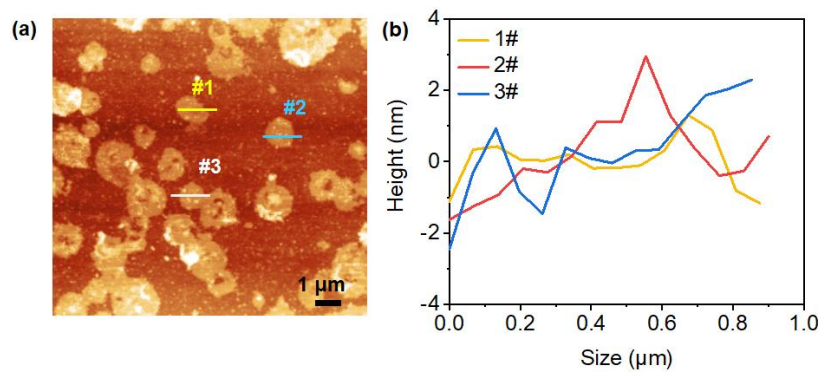
**Figure S2.** SEM images of MSSs through ILs assisted sonication exfoliation. Results demonstrate that the obtained MSSs have uniform size distribution and ultrathin feature.



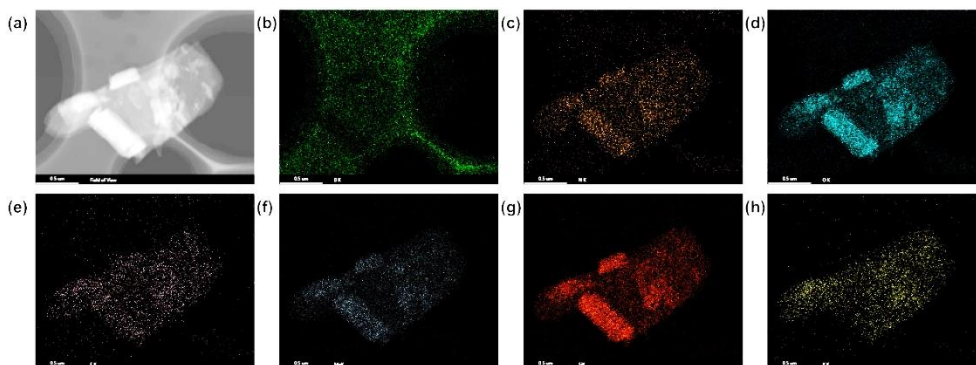
**Figure S3.** FTIR (a) and <sup>1</sup>H NMR (b) spectra of recycled ILs r-[BMIM]BF<sub>4</sub> and compared with the original ILs o-[BMIM]BF<sub>4</sub><sup>[1]</sup>. It can be observed that the chemical composition of r-[BMIM]BF<sub>4</sub> has not changed and it can continue to be utilized for mica exfoliation.



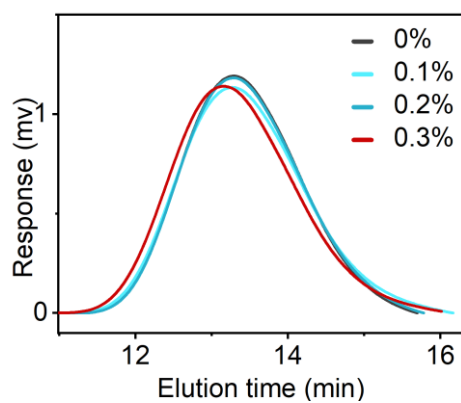
**Figure S4.** Different ILs (a), mass ratios (b), and liquid volumes (c) were used to exfoliate mica. The concentration of MSSs was calculated to screen for the optimal intercalation agent and stripping conditions. By comparing the concentration of MSSs and the SEM images (d) of MSSs, it was found that [BMIM]BF<sub>4</sub> is the optimal intercalation agent and the optimal exfoliation condition is when the ratio of ionic liquid to mica is 1:2.5.



**Figure S5.** AFM image (a) and the corresponding height profiles (b) of the exfoliated MSSs. AFM results reveal that the MSSs with a thickness of 1.5 nm, indicating their single-layer feature.

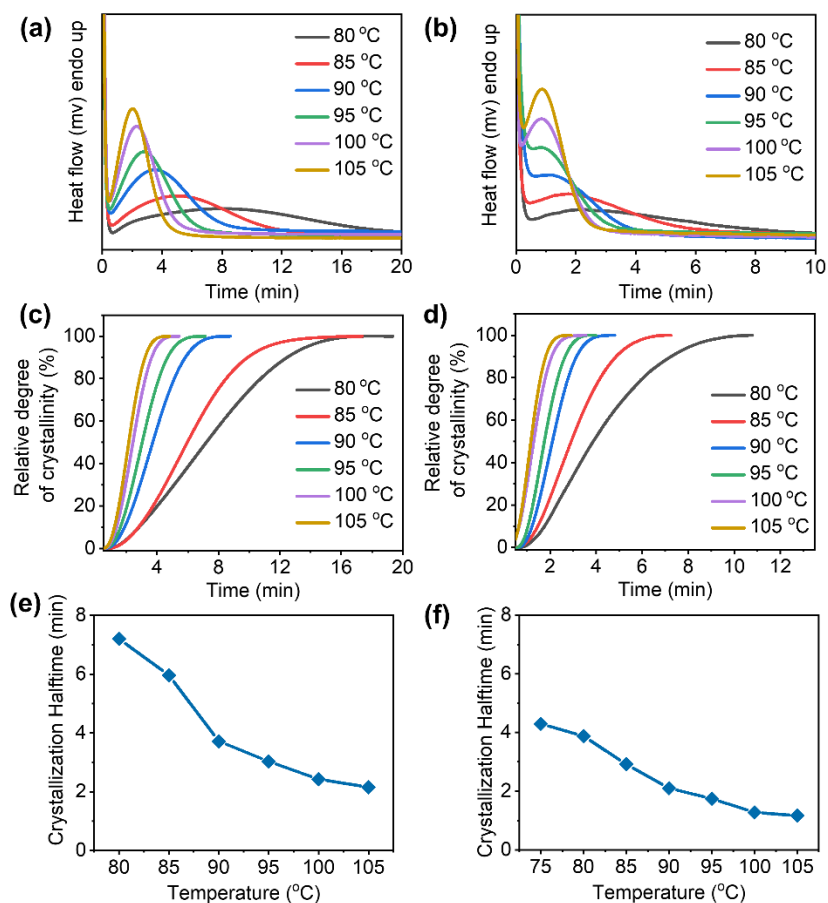


**Figure S6.** EDS images of MSSs through SEM testing (a). The element distribution mapping of (b) B atom, (c) N atom, (d) O atom, (e) F atom, (f) Mg atom, (g) Si atom, and (h) K atom. The elements are uniform distribution in the MSSs.

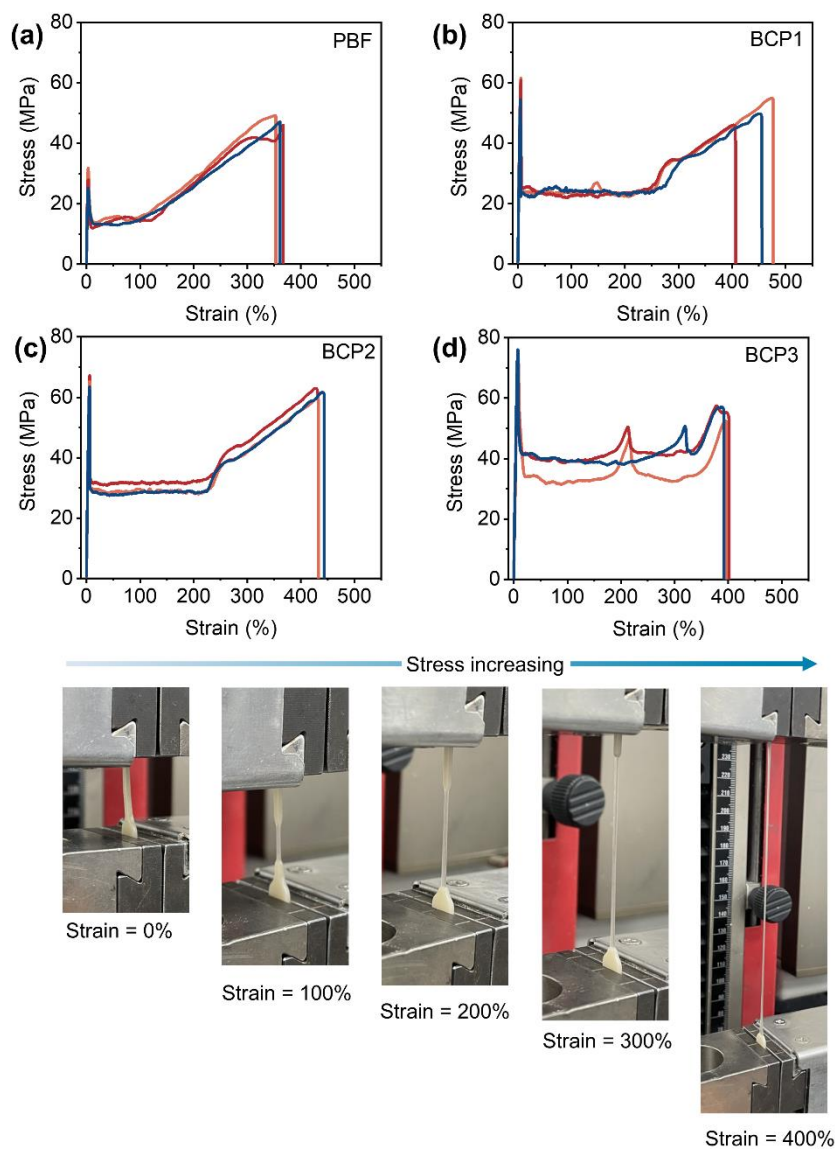


**Figure S7.** GPC chromatogram of PBF and BCP with different content of MSSs. The result shows that the addition of MSSs in PBF cannot change the molecular weight.

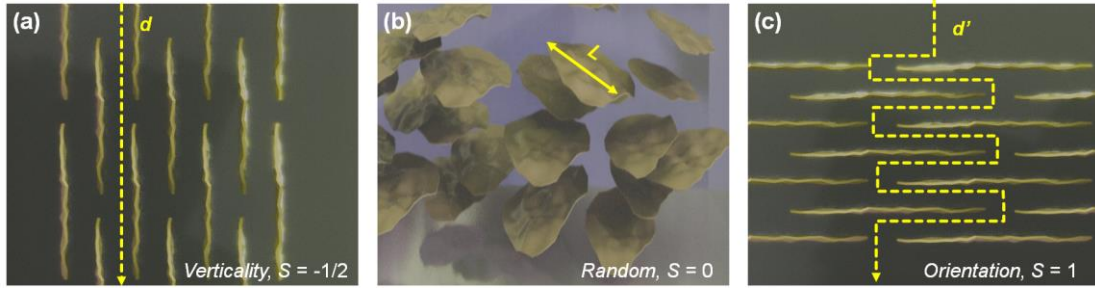




**Figure S8.** Isothermal crystallization peaks recorded at the indicated temperatures for PBF and BCP3 (a and b), Evolution of the relative degree of crystallinity with time for PBF and BCP3 (c and d). Halftime of crystallization versus the isothermal crystallization temperature for PBF and BCP3 (e and f) [2].



**Figure S9.** The stress-strain plots of PBF (a), BCP1 (b), BCP2 (c), and BCP3 (d) films. These BCP films exhibit largely enhanced mechanical properties, and the strengths and modulus of composites increased with the increasing of fillers. The digital photos of stress process for the BCP3 sample (e).



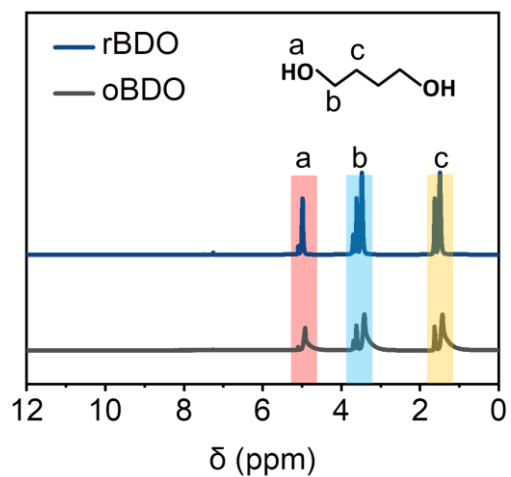
**Figure S10.** Schematic diagrams of the physical barrier mechanisms of MSSs composites. Tortuosity ( $\tau$ ) of the gas diffusion in the films was determined by *Nielsen* theory. The  $\tau$  is defined as the ratio of the factual distance  $d'$  to the shortest distance  $d$ . The gas cannot penetrate into the sheets, while they must bypass the MSSs, causing tortuous pathways. As a result, the degree of tortuosity is related to aspect ratio  $L/W$  ( $L$  and  $W$  represent the lateral size and thickness of MSSs, respectively), orientation  $S$ , and content  $\varphi$  of the fillers, which can be approximately given by following <sup>[3]</sup>.

$$\tau = \frac{d'}{d} = 1 + \frac{L}{2W} \times \varphi \times \frac{2}{3} \left( S + \frac{1}{2} \right) \quad (S1)$$

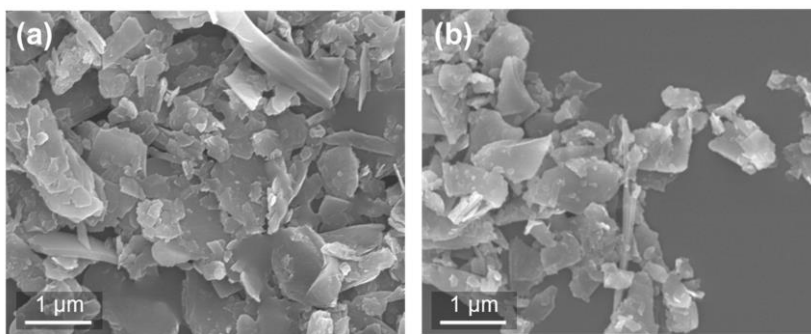
where the orientation degree  $S$  can be defined by equation

$$S = \frac{1}{2} (3\cos^2\theta - 1) \quad (S2)$$

where when the sheets are verticality distribution,  $\theta = 90^\circ$  ( $S = -1/2$ ); when the sheets are parallel arrangement,  $\theta = 0^\circ$  ( $S = 1$ ), while the sheets are random distribution,  $\theta = 54.74^\circ$  ( $S = 0$ ). The corresponding results can be found in Table S5.



**Figure S11.** <sup>1</sup>H NMR spectra of standard BDO (oBDO) and recycled BDO (rBDO). Result demonstrates that rBDO shows the same <sup>1</sup>H NMR spectrum with the oBDO.



**Figure S12.** SEM image of the recycled MSSs (rMSSs). Results demonstrate that the rMSSs remained their original sheet-like structure during the chemical recycled process.

**Table S1.** Molecular weight and intrinsic viscosity [ $\eta_{sp}$ ] of polyesters.

<b>Sample</b>	<b>MSSs (wt%)</b>	<b><math>[\eta]</math></b>	<b><math>M_n</math> (g/mol)</b>	<b><math>M_w</math> (g/mol)</b>	<b>PD</b>
PBF	0.0	0.94	$4.0 \times 10^4$	$6.9 \times 10^4$	1.7
BCP1	0.1	0.97	$3.7 \times 10^4$	$7.0 \times 10^4$	1.9
BCP2	0.2	0.97	$3.9 \times 10^4$	$6.9 \times 10^4$	1.8
BCP3	0.3	1.05	$4.1 \times 10^4$	$7.8 \times 10^4$	1.9

**Table S2.** Mechanical properties parameters of different polyester materials.

<b>Sample</b>	<b><math>\sigma_y^a</math> (MPa)</b>	<b><math>E^a</math> (GPa)</b>	<b><math>\varepsilon^a</math> (%)</b>	<b><math>\tau^a</math> (MJ/m<sup>3</sup>)</b>
PBF	47 ± 2	1.4 ± 0.05	360 ± 7	96 ± 2
BCP1	58 ± 4	1.5 ± 0.1	445 ± 20	137 ± 18
BCP2	65 ± 2	1.5 ± 0.1	436 ± 7	166 ± 5
BCP3	76 ± 1	1.5 ± 0.1	397 ± 4	161 ± 18

<sup>a</sup> $\sigma$ ,  $E$ ,  $\varepsilon$ , and  $\tau$  refer to tensile strength, Young's modulus, elongation at break, and toughness, respectively.

**Table S3.** Mechanical properties of BCP and previously reported FDCA-based polyesters materials.

<i>No.</i>	<b>Sample</b>	$\sigma_y$ (MPa)	$\sigma_b$ (MPa)	$\epsilon$ (%)	<b>Ref.</b>
1	PEF	-	82	4	[4]
2	Mica/PEF	67	-	4.7	[5]
3	PE <sub>91</sub> Pe <sub>9</sub> F	80	-	29	[4]
4	PE <sub>82</sub> Pe <sub>18</sub> F	83	-	115	[4]
5	PE <sub>66</sub> Pe <sub>34</sub> F	75	-	181	[4]
6	PE <sub>53</sub> Pe <sub>47</sub> F	72	-	265	[4]
7	PE <sub>37</sub> Pe <sub>63</sub> F	49	-	185	[4]
8	PE <sub>16</sub> Pe <sub>84</sub> F	33	-	286	[4]
9	PE <sub>4</sub> Pe <sub>96</sub> F	-	20	315	[4]
10	PE <sub>81</sub> H <sub>19</sub> F	-	66	3	[6]
11	PE <sub>72</sub> H <sub>28</sub> F	71	-	54	[6]
12	PE <sub>64</sub> H <sub>36</sub> F	65	-	159	[6]
13	PE <sub>48</sub> H <sub>52</sub> F	48	-	275	[6]
14	PE <sub>34</sub> H <sub>66</sub> F	-	34	315	[6]
15	PE <sub>12</sub> H <sub>88</sub> F	-	38	148	[6]
16	PPF	-	29	3	[7]
17	PBF	-	21	157	[7]
18	PHF	-	42	22	[7]
19	PPeF	-	9	1050	[8]
<b>20</b>	<b>BCP</b>	<b>76</b>	-	<b>397</b>	<b>This work</b>

$\sigma_y$ ,  $\sigma_b$ , and  $\epsilon$  refer to yield strength, break strength and elongation at break.



**Table S4.** Structural parameters of BCP at various strains calculated from 1D correlation function curves of the SAXS profile.

<b>Sample</b>	<b>Strain (%)</b>	<b><math>L</math> (nm)<sup>a</sup></b>	<b><math>I_a</math> (nm)<sup>b</sup></b>	<b><math>I_c</math> (nm)<sup>c</sup></b>	<b><math>\Phi^d</math></b>
BCP	0	10.7	7.1	3.6	0.33
	100	12	7.9	4.1	0.34
	200	11.2	7.4	3.9	0.34

<sup>a</sup>The long period length; <sup>b</sup>Amorphous thickness; <sup>c</sup> crystalline thickness; <sup>d</sup> linear crystallinity.

**Table S5.** Gas barrier properties of different polyester materials.

<b>Sample</b>	<b><math>\tau^a</math></b>	<b>O<sub>2</sub><sup>a</sup></b>	<b>BIFp</b>	<b>CO<sub>2</sub><sup>a</sup></b>	<b>BIFp</b>	<b>H<sub>2</sub>O<sup>b</sup></b>	<b>BIFp</b>
PBF	1.0	0.060	1.0	0.073	1.0	4.70	1.0
BCP1	1.4	0.0317	1.9	0.0435	1.7	2.15	2.2
BCP2	1.8	0.0245	2.5	0.0312	2.3	1.74	2.7
BCP3	2.2	0.0183	3.3	0.0244	3.0	1.49	3.2
PET	/	0.077	/	0.11	/	4.80	/

<sup>a</sup>The test was carried out at 0.1001 MPa, at 23 °C, 50% relative humidity. 1 barrer = 10<sup>-10</sup> cm<sup>3</sup> cm/cm<sup>2</sup>·s·cm Hg. <sup>b</sup>The test was carried out at 38 °C, 90% relative humidity, 10<sup>-14</sup> g cm/cm<sup>2</sup> s Pa.

**Table S6.** Gas permeability coefficients for BCP and other polyester materials

Sample	CO <sub>2</sub> (barrer)	BIFp	O <sub>2</sub> (barrer)	BIFp	H <sub>2</sub> O (g/(m <sup>2</sup> d))	H <sub>2</sub> O (g·cm/(cm <sup>2</sup> s Pa))	BIFp	Ref
PE	6.29	1.0	1.58	1.0	7.9	/	1.0	[9]
PP	3.82	1.6	2.75	0.6	2.2	/	3.6	[10]
PET	0.11	63.5	0.077	20.5	/	4.8×10 <sup>-14</sup>	1.8	[11]
PEF	0.04	161.2	0.02	105.3	/	1.64×10 <sup>-14</sup>	4.9	[12]
P <sub>14</sub> BTF	0.09	68.3	0.05	30.3	/	2.05×10 <sup>-14</sup>	3.9	[13]
PBCF <sub>40</sub>	0.7	9.0	0.1	15.8	/	1.3×10 <sup>-14</sup>	0.1	[14]
PBFGA <sub>20</sub>	0.05	125.8	0.02	75.2	/	2.65×10 <sup>-14</sup>	3.0	[15]
PBF	0.073	86.2	0.06	26.3	/	4.7×10 <sup>-14</sup>	1.8	This work
<b>BCP</b>	<b>0.024</b>	<b>262.1</b>	<b>0.018</b>	<b>87.8</b>	/	<b>1.48×10<sup>-14</sup></b>	<b>5.4</b>	<b>This work</b>

**Table S7.** Mechanical properties of physically recycled BCP.

<b>Sample</b>	<b><math>\sigma</math> (MPa)</b>	<b><math>E</math> (GPa)</b>	<b><math>\varepsilon</math> (%)</b>	<b><math>\tau</math> (MJ/m<sup>3</sup>)</b>
Original	76 $\pm$ 1	1.5 $\pm$ 0.1	397 $\pm$ 4	161 $\pm$ 18
1 <sup>st</sup>	76 $\pm$ 1	1.5 $\pm$ 0.1	382 $\pm$ 5	159 $\pm$ 15
3 <sup>th</sup>	73 $\pm$ 1	1.3 $\pm$ 0.1	409 $\pm$ 5	168 $\pm$ 16

**Table S8.** Mechanical properties of chemically recycled BCP.

<b>Sample</b>	<b><math>\sigma</math> (MPa)</b>	<b><math>E</math> (GPa)</b>	<b><math>\epsilon</math> (%)</b>	<b><math>\tau</math> (MJ/m<sup>3</sup>)</b>
o-BCP	76 $\pm$ 1	1.5 $\pm$ 0.1	397 $\pm$ 4	161 $\pm$ 18
r-BCP	77 $\pm$ 1	1.5 $\pm$ 0.1	378 $\pm$ 5	159 $\pm$ 15

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