## Supplementary material

## Studying the degradation of bulk PTFE into microparticles via SP ICP-MS: A systematically developed method for the detection of F-containing particles

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|      | Matrix Code – |            | Experimental Conditions |   |                     |                       |  |  |
|------|---------------|------------|-------------------------|---|---------------------|-----------------------|--|--|
| Exp. |               |            | (A) Pla                 | asma                                      | (B) Bandpass        |                       |  |  |
|      | Variable 1    | Variable 2 | Sample Depth<br>(mm)    | Nebulizer Flow<br>(mL min <sup>-1</sup> ) | Q1 Mass Gain<br>(V) | Q1 Mass Offset<br>(V) |  |  |
| 1    | 0             | 0          | 4.5                     | 1.40                                      | 10                  | 130                   |  |  |
| 2    | 0             | 1          | 4.5                     | 1.50                                      | 10                  | 150                   |  |  |
| 3    | 0.866         | 0.5        | 6.0                     | 1.45                                      | 20                  | 140                   |  |  |
| 4    | 0             | -1         | 4.5                     | 1.30                                      | 10                  | 110                   |  |  |
| 5    | -0.866        | -0.5       | 3.0                     | 1.35                                      | 0                   | 120                   |  |  |
| 6    | -0.866        | 0.5        | 3.0                     | 1.45                                      | 0                   | 140                   |  |  |
| 7    | 0.866         | -0.5       | 6.0                     | 1.35                                      | 20                  | 120                   |  |  |
| CP   | 0             | 0          | 4.5                     | 1.40                                      | 10                  | 130                   |  |  |
| CP   | 0             | 0          | 4.5                     | 1.40                                      | 10                  | 130                   |  |  |
| CP   | 0             | 0          | 4.5                     | 1.40                                      | 10                  | 130                   |  |  |

Table S1: Doehlert experimental design for optimisation of the (A) plasma, and (B) bandpass

| Evn     | Matrix     | Code       | Experimental Conditions |             |  |  |
|---------|------------|------------|-------------------------|-------------|--|--|
| Exp.    | Variable 1 | Variable 2 | Extract 2 (V)           | Deflect (V) |  |  |
| 1       | -1         | -1         | -5                      | -5          |  |  |
| 2       | -1         | 1          | -5                      | 5           |  |  |
| 3       | 1          | -1         | 5                       | -5          |  |  |
| 4       | 1          | 1          | 5                       | 5           |  |  |
| 5       | -1.41421   | 0          | -7                      | 0           |  |  |
| 6       | 1.41421    | 0          | 7                       | 0           |  |  |
| 7       | 0          | -1.41421   | 0                       | -7          |  |  |
| 8       | 0          | 1.41421    | 0                       | 7           |  |  |
| 9 (CP)  | 0          | 0          | 0                       | 0           |  |  |
| 10 (CP) | 0          | 0          | 0                       | 0           |  |  |

**Table S2**: Central Composite experimental design for optimization of extract 2 and deflect of ion optics.

**Figure S1**: Colorimetric map obtained from the Central Composite experimental design (2 factors: 10 exp) for ion optics optmisation. Selected conditions are marked as a white circle.





**Table S3**: Factorial design 2<sup>5</sup> executed to discriminate between significant and non-significantfactors that can affect the CRC performance

|      |       | Ма    | atrix Co | de    |       | Experimental Conditions |                          |            |                        |                        |
|------|-------|-------|----------|-------|-------|-------------------------|--------------------------|------------|------------------------|------------------------|
| Exp. | Var 1 | Var 2 | Var 3    | Var 4 | Var 5 | Oct<br>Bias             | Energy<br>Discrimination | He<br>Flow | H <sub>2</sub><br>Flow | O <sub>2</sub><br>Flow |
| 1    | -1    | -1    | -1       | -1    | -1    | -8                      | -5                       | 0          | 0                      | 5                      |
| 2    | 1     | -1    | -1       | -1    | -1    | -2                      | -5                       | 0          | 0                      | 5                      |
| 3    | -1    | 1     | -1       | -1    | -1    | -8                      | 2                        | 0          | 0                      | 5                      |
| 4    | 1     | 1     | -1       | -1    | -1    | -2                      | 2                        | 0          | 0                      | 5                      |
| 5    | -1    | -1    | 1        | -1    | -1    | -8                      | -5                       | 2          | 0                      | 5                      |
| 6    | 1     | -1    | 1        | -1    | -1    | -2                      | -5                       | 2          | 0                      | 5                      |
| 7    | -1    | 1     | 1        | -1    | -1    | -8                      | 2                        | 2          | 0                      | 5                      |
| 8    | 1     | 1     | 1        | -1    | -1    | -2                      | 2                        | 2          | 0                      | 5                      |
| 9    | -1    | -1    | -1       | 1     | -1    | -8                      | -5                       | 0          | 2                      | 5                      |
| 10   | 1     | -1    | -1       | 1     | -1    | -2                      | -5                       | 0          | 2                      | 5                      |
| 11   | -1    | 1     | -1       | 1     | -1    | -8                      | 2                        | 0          | 2                      | 5                      |
| 12   | 1     | 1     | -1       | 1     | 24    | -2                      | 2                        | 0          | 2                      | 5                      |
| 13   | -1    | -1    | 1        | 1     | -1    | -8                      | -5                       | 2          | 2                      | 5                      |
| 14   | 1     | -1    | 1        | 1     | -1    | -2                      | -5                       | 2          | 2                      | 5                      |
| 15   | -1    | 1     | 1        | 1     | -1    | -8                      | 2                        | 2          | 2                      | 5                      |
| 16   | 1     | 1     | 1        | 1     | -1    | -2                      | 2                        | 2          | 2                      | 5                      |
| 17   | -1    | -1    | -1       | -1    | 1     | -8                      | -5                       | 0          | 0                      | 30                     |
| 18   | 1     | -1    | -1       | -1    | 1     | -2                      | -5                       | 0          | 0                      | 30                     |
| 19   | -1    | 1     | -1       | -1    | 1     | -8                      | 2                        | 0          | 0                      | 30                     |
| 20   | 1     | 1     | -1       | -1    | 1     | -2                      | 2                        | 0          | 0                      | 30                     |
| 21   | -1    | -1    | 1        | -1    | 1     | -8                      | -5                       | 2          | 0                      | 30                     |
| 22   | 1     | -1    | 1        | -1    | 1     | -2                      | -5                       | 2          | 0                      | 30                     |
| 23   | -1    | 1     | 1        | -1    | 1     | -8                      | 2                        | 2          | 0                      | 30                     |
| 24   | 1     | 1     | 1        | -1    | 1     | -2                      | 2                        | 2          | 0                      | 30                     |
| 25   | -1    | -1    | -1       | 1     | 1     | -8                      | -5                       | 0          | 2                      | 30                     |
| 26   | 1     | -1    | -1       | 1     | 1     | -2                      | -5                       | 0          | 2                      | 30                     |
| 27   | -1    | 1     | -1       | 1     | 1     | -8                      | 2                        | 0          | 2                      | 30                     |
| 28   | 1     | 1     | -1       | 1     | 1     | -2                      | 2                        | 0          | 2                      | 30                     |
| 29   | -1    | -1    | 1        | 1     | 1     | -8                      | -5                       | 2          | 2                      | 30                     |
| 30   | 1     | -1    | 1        | 1     | 1     | -2                      | -5                       | 2          | 2                      | 30                     |
| 31   | -1    | 1     | 1        | 1     | 1     | -8                      | 2                        | 2          | 2                      | 30                     |
| 32   | 1     | 1     | 1        | 1     | 1     | -2                      | 2                        | 2          | 2                      | 30                     |

**Figure S2:** Pareto chart for the factorial design 2<sup>5</sup> showing the significant factors that affect the CRC performance.



Standardized Effect Estimate (Absolute Value)

|      |       | Matrix Co | ode   | Experimental Conditions |                        |                          |  |
|------|-------|-----------|-------|-------------------------|------------------------|--------------------------|--|
| Exp. | Var 1 | Var 2     | Var 3 | H <sub>2</sub><br>Flow  | O <sub>2</sub><br>Flow | Energy<br>Discrimination |  |
| 1    | -1    | -1        | 0     | 0                       | 5                      | -10                      |  |
| 2    | 1     | -1        | 0     | 1                       | 5                      | -10                      |  |
| 3    | -1    | 1         | 0     | 0                       | 15                     | -10                      |  |
| 4    | 1     | 1         | 0     | 1                       | 15                     | -10                      |  |
| 5    | -1    | 0         | -1    | 0                       | 10                     | -15                      |  |
| 6    | 1     | 0         | -1    | 1                       | 10                     | -15                      |  |
| 7    | -1    | 0         | 1     | 0                       | 10                     | -5                       |  |
| 8    | 1     | 0         | 1     | 1                       | 10                     | -5                       |  |
| 9    | 0     | -1        | -1    | 0.5                     | 5                      | -15                      |  |
| 10   | 0     | 1         | -1    | 0.5                     | 15                     | -15                      |  |
| 11   | 0     | -1        | 1     | 0.5                     | 5                      | -5                       |  |
| 12   | 0     | 1         | 1     | 0.5                     | 15                     | -5                       |  |
| 13   | 0     | 0         | 0     | 0.5                     | 10                     | -10                      |  |
| 14   | 0     | 0         | 0     | 0.5                     | 10                     | -10                      |  |
| 15   | 0     | 0         | 0     | 0.5                     | 10                     | -10                      |  |

**Table S4:** Box-Behnken experimental design for optimization of H<sub>2</sub> flow, O<sub>2</sub> flow, and energy discrimination of CRC.

**Figure S3**. Box-Behnken Designs (3 factors: 15 exp) for CRC optimisations: A)  $O_2$  flow vs  $H_2$  flow, B) Energy discrimination vs  $H_2$  flow and C) Energy discrimination vs  $O_2$  flow. Optimised values are shown at the bottom of the figures, respectively.

