

Cite this: DOI: 00.0000/xxxxxxxxxx

## Supplementary Information for *Pervaporation-driven electrokinetic energy harvesting using poly(dimethylsiloxane) microfluidic chips*

Hrishikesh Pingulkar,<sup>a</sup> Cédric Ayela,<sup>b</sup> and Jean-Baptiste Salmon<sup>a</sup>

### 1 Mask of the channel network

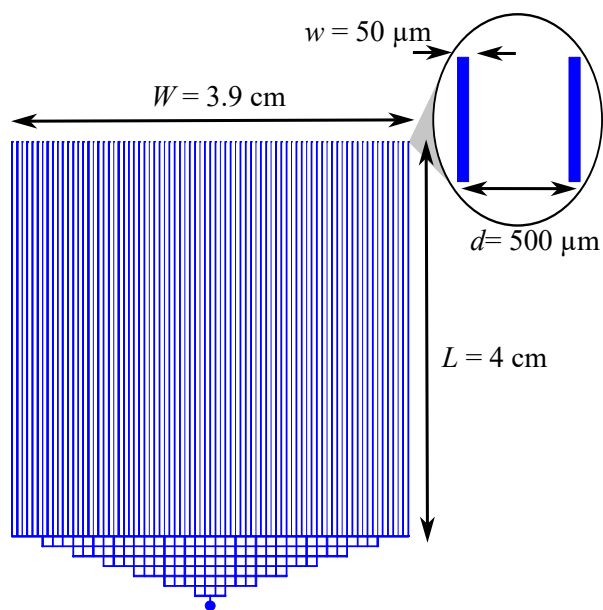


Fig. S1 Mask used to make the leaf channel network.  $N = 79$  dead-end microchannels of width  $w = 50 \mu\text{m}$  and length  $L = 4 \text{ cm}$  are connected to a single inlet. The centre-to-centre distance between adjacent channels is  $d = 500 \mu\text{m}$  resulting in a total leaf width of  $W = 3.9 \text{ cm}$ .

### 2 Approximations for the pervaporation-driven flow rate of a single channel

The relation:

$$F \simeq \frac{\pi}{\log(16H/(\pi w))}, \quad (\text{S1})$$

derived in another context<sup>1</sup> and only valid for  $H \gg w \gg h$ , provides nevertheless a rough approximation of the analytical solution given by Dollet *et al.*<sup>2</sup> for  $H \gg 1 \text{ mm}$ , see Fig. 4. Eqn S1 shows the weak logarithmic dependence of the pervaporation-driven flow rate with the transverse dimensions of the channel as

early recognised for thick chips<sup>3,4</sup>. For thinner chips, Dollet *et al.* provided the following approximation<sup>2</sup>:

$$F \simeq \frac{w}{\delta} + \frac{2}{\pi} \left[ \ln \frac{(H + \delta)h}{\delta^2} + \frac{H}{\delta} \ln \frac{H + \delta}{h} \right], \quad (\text{S2})$$

with  $\delta = H - h$ , valid for  $\delta \leq w$  and when  $h$  is not too small compared to  $w$ . As shown in Fig. 4, eqn S2 correctly approximates the analytical solution in our configuration even for  $H \leq 200 \mu\text{m}$ .

### 3 Numerical estimate of the pervaporation rate

To estimate the pervaporation rate  $Q$  for the channel network shown in Fig. S1, we performed numerical resolutions to calculate the concentration field  $C$  ( $\text{kg}/\text{m}^3$ ) of water within the PDMS leaf and the corresponding water mass flux  $\nabla C$ , see Refs.<sup>5,6</sup> for similar calculations. Fig. S2(a) shows the cross-section of the leaf which comprises  $N$  identical channels of rectangular cross-section  $h \times w$ . The problem is nearly invariant along the channels because  $L \gg H$ , thus justifying a 2D description. Because of the symmetries, we only solve the steady diffusion equation for  $C$  inside the dotted rectangle shown in Fig. S2(a). We then assume that the water concentration  $C$  in PDMS follows Henry's law and that the water diffusion coefficient  $D_w$  ( $\text{m}^2 \text{s}^{-1}$ ) in the matrix is constant (reasonable approximations according to Refs.<sup>2,7</sup>). With these assumptions, one can solve the dimensionless 2D diffusion equation  $\Delta \tilde{c} = 0$ , with  $\tilde{c} = (C/C_{\text{sat}} - \text{RH})/(1 - \text{RH})$ ,  $C_{\text{sat}}$  ( $\text{kg m}^{-3}$ ) being the concentration of water at saturation in PDMS. The parameter  $\tilde{q}$  ( $\text{m}^2 \text{s}^{-1}$ ) given in the main text is then  $\tilde{q} = D_w C_{\text{sat}}/\rho_w$ , with  $\rho_w$  ( $\text{kg m}^{-3}$ ) the water density<sup>8</sup>. With this definition, boundary conditions are  $\tilde{c} = 1$  at the channel walls and  $\tilde{c} = 0$  at the air/PDMS interface, and no-flux on the other boundaries for reasons of symmetry and because glass is impermeable to water.

Fig. S2(b) shows the numerical resolution of the concentration field  $\tilde{c}$  for the case studied in the present work:  $h = 30$ ,  $w = 50$ ,  $H = 200$ , and  $d = 500 \mu\text{m}$  (Matlab, pde toolbox). The water flux normal to the air/PDMS interface is numerically estimated from such concentration maps, and is used to finally estimate the overall pervaporation rate  $Q$  induced by the leaf by summing the  $N$  channels of length  $L$ . Fig. S3 shows the pervaporation-driven flow rate  $Q$  calculated using these numerical resolutions for a PDMS leaf of thickness  $H = 200 \mu\text{m}$  and width  $W = 3.9 \text{ cm}$  as a function of the number of channels  $N$  it contains, and thus

<sup>a</sup> CNRS, Solvay, LOF, UMR 5258, Université de Bordeaux, 178 av. Schweitzer, 33600 Pessac, France.

<sup>b</sup> Univ. Bordeaux, IMS, CNRS, Bordeaux INP, UMR 5218, 33607 Pessac, France.

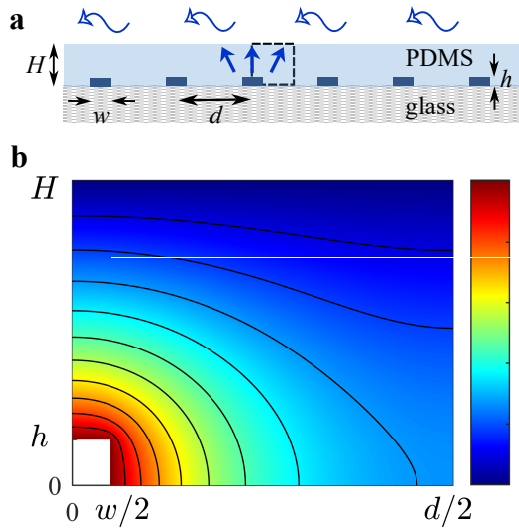


Fig. S2 (a) Cross-section view of the PDMS leaf. The dotted rectangle shows the calculation domain of the diffusion equation governing the concentration of water in PDMS. Concentration field  $\tilde{c}$  estimated numerically for  $h = 30$ ,  $w = 50$ ,  $H = 200$ , and  $d = 500$   $\mu\text{m}$  (the thin dark lines are isoconcentration lines).

for varying center-to-center distance  $d$  between adjacent channels ( $h = 30$  and  $w = 50$   $\mu\text{m}$ ).  $Q$  is normalized by the limiting pervaporation-driven flow rate  $Q_{\text{lim}}$  corresponding to the high channel density regime  $1/d \gg 1/H$  (strong coupling between the adjacent channels, see eqn 2). For  $N \ll 100$ ,  $Q$  increases linearly with  $N$ , and saturates at  $Q_{\text{lim}}$  for  $N \gg 100$ . The experimental case studied in the present work ( $N = 79$ ) is in between these two asymptotic regimes, and the numerical resolution gives in that case  $Q = \alpha Q_{\text{lim}}$ , with  $\alpha \simeq 0.5$ . We refer the reader to Ref.<sup>5</sup> for a full description and in-depth discussion of this problem.

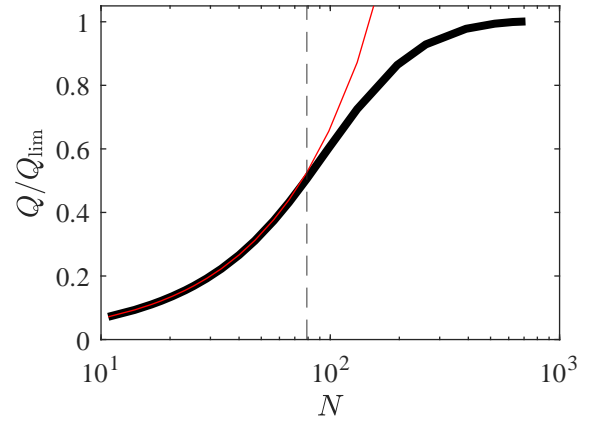


Fig. S3 Pervaporation-driven flow rate  $Q$  normalized by  $Q_{\text{lim}}$  (eqn 2) for a leaf of thickness  $H = 200$   $\mu\text{m}$  and width  $W = 3.9$  cm as a function of the number  $N$  of channels it contains. The red line is  $Q = NQ_i$  corresponding to the low density regime ( $1/d \ll 1/H$ ). The vertical dotted line indicates the experimental configuration studied experimentally for which  $Q \simeq 0.5Q_{\text{lim}}$ .

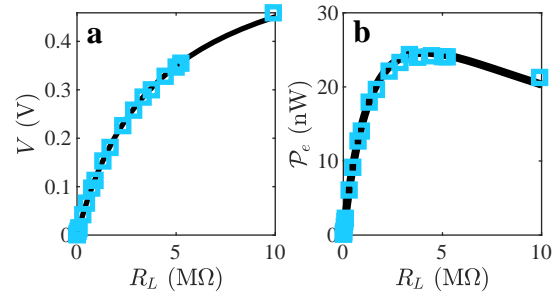


Fig. S4 (a) Streaming potential  $V$  and (b) electrical power  $\mathcal{P}_e = V^2/R_L$  as a function of the load resistance  $R_L$  measured for a pressure drop  $\Delta P = 1$  bar across a colloid plug of length  $L_p \simeq 3$  mm in a tube with inner radius  $R_t = 0.5$  mm (hydraulic resistance  $R_h \simeq 0.11$  bar min  $\mu\text{L}^{-1}$ ). The continuous lines are fits by eqn 4 with  $R_C = 4.1$  M $\Omega$  and  $S_{\text{str}} = 155$  nA bar $^{-1}$ .

## Notes and references

- 1 C. Loussert, F. Doumenc, J.-B. Salmon, V. S. Nikolayev and B. Guerrier, *Langmuir*, 2023, **39**, 11147.
- 2 B. Dollet, J.-F. Louf, M. Alonzo, K. Jensen and P. Marmottant, *J. R. Soc. Interface*, 2019, **16**, 20180690.
- 3 E. Verneuil, A. Buguin and P. Silberzan, *Europhys. Lett.*, 2004, **68**, 412.
- 4 G. C. Randall and P. S. Doyle, *Proc. Natl. Acad. Sci. USA*, 2005, **102**, 10813.
- 5 X. Noblin, L. Mahadevan, I. A. Coomaraswamy, D. A. Weitz, N. M. Holbrook and M. A. Zwieniecki, *Proc. Natl. Acad. Sci. USA*, 2008, **105**, 9140.
- 6 N. Ziane, M. Guirardel, J. Leng and J.-B. Salmon, *Soft Matter*, 2015, **11**, 3637.
- 7 S. J. Harley, E. A. Glascoe and R. S. Maxwell, *J. Phys. Chem. B*, 2012, **116**, 14183.
- 8 P. Bacchin, J. Leng and J. B. Salmon, *Chem. Rev.*, 2022, **122**, 6938.