

## Supporting Information

### **A Bio-inspired Approach to Engineering Water-Responsive, Mechanically-Adaptive Materials**

*Daseul Jang,<sup>a</sup> Yu-Tai Wong,<sup>b</sup> LaShanda T. J. Korley<sup>a, b\*</sup>*

<sup>a</sup>. Department of Materials Science and Engineering, University of Delaware, 127 The Green, 201 Dupont Hall, Newark, Delaware, USA, 19716.

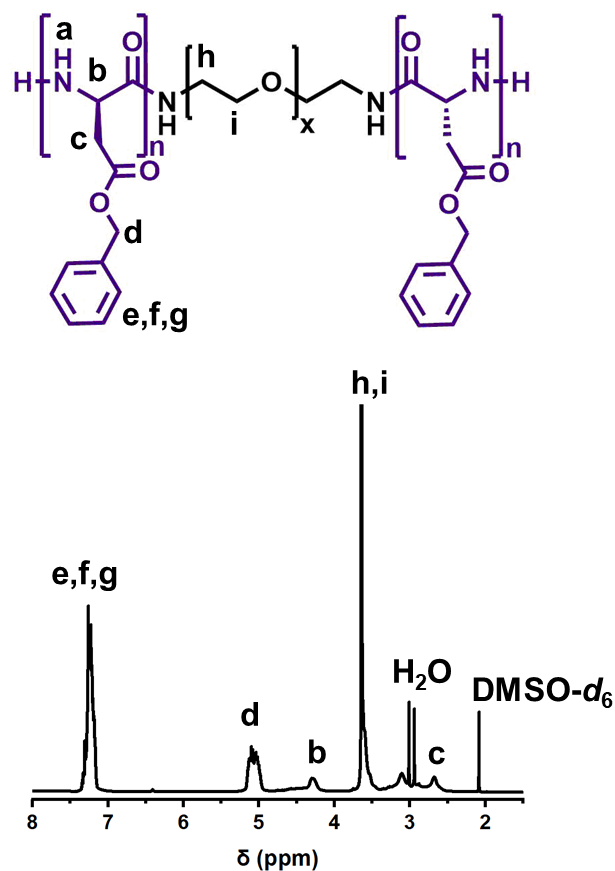
<sup>b</sup>. Department of Chemical and Biomolecular Engineering, University of Delaware, 150 Academy Street, Newark, Delaware, 19716.

\* Corresponding author: [lkorley@udel.edu](mailto:lkorley@udel.edu)

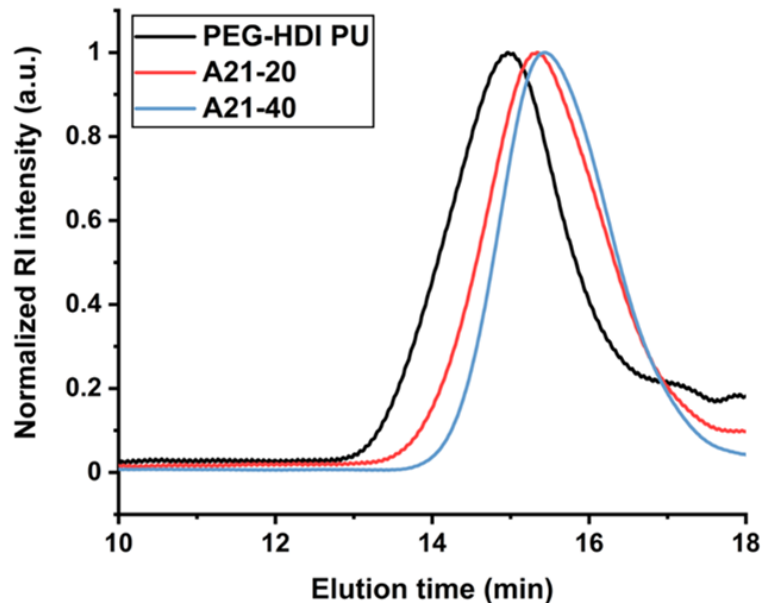
## Abbreviations and nomenclature

<sup>1</sup>H nuclear magnetic resonance (<sup>1</sup>H NMR)  
Poly( $\beta$ -benzyl-L-aspartate) (PBLA)  
 $\alpha,\omega$ -Bis(amine)poly(ethylene glycol) (PEG)  
Degree of polymerization (DP)  
1,6-hexamethylene diisocyanate (HDI)  
Polyurea (PU)  
Peptide-polyurea hybrids (PPUs)  
Cellulose nanocrystals (CNCs)  
Gel permeation chromatography (GPC)  
Atomic force microscopy (AFM)  
Poly(methyl methacrylate) (PMMA)  
Nanocellulose (NC)

The following nomenclature was utilized. An-X and An-X/CNCY were used for the PPUs and the PPU/CNC nanocomposites, respectively, where A indicates non-chain extended peptide-polyurea hybrids consisting of PBLA-*b*-PEG-*b*-PBLA as the soft segment, n is the peptide repeat length (21), X is the peptide weight fraction in the resultant sample (20 or 40 wt%), and Y is CNC content (wt%). The control film without PBLA was denoted by PEG-HDI PU.



**Figure S1.**  $^1\text{H}$  NMR spectrum of PBLA-*b*-PEG-*b*-PBLA triblock recorded in dimethyl sulfoxide (DMSO)- $d_6$ . The PBLA repeat length or the degree of polymerization of the PBLA block ( $n$ ) was determined from the integration ratio of resonance corresponding to PEG block at  $\delta$  3.9 ppm and PBLA block at  $\delta$  ~ 5.5 ppm. The peak at  $\delta$  3.9 ppm corresponding to the PEG backbone was used as a reference peak, with the integration value of this peak set to 188 ( $x=47$ ), as identified from end group analysis of the PEG homopolymer (~ 2,000 g/mol). The relative DP ratio of PEG( $x$ )/PBLA( $n$ ) is ~2, indicating that the PEG block has approximately double the repeat units compared to the PBLA block in the resulting triblock copolymer.

**(A)****(B)**

	PBLA <sup>a</sup> (wt%)	$M_n^b$ (kg mol <sup>-1</sup> )	$\mathcal{D}^b$
PEG-HDI PU	0	118.6	3.0
A21-20	20	57.0	2.9
A21-40	40	48.6	2.5

<sup>a</sup> Determined from Equation S1.

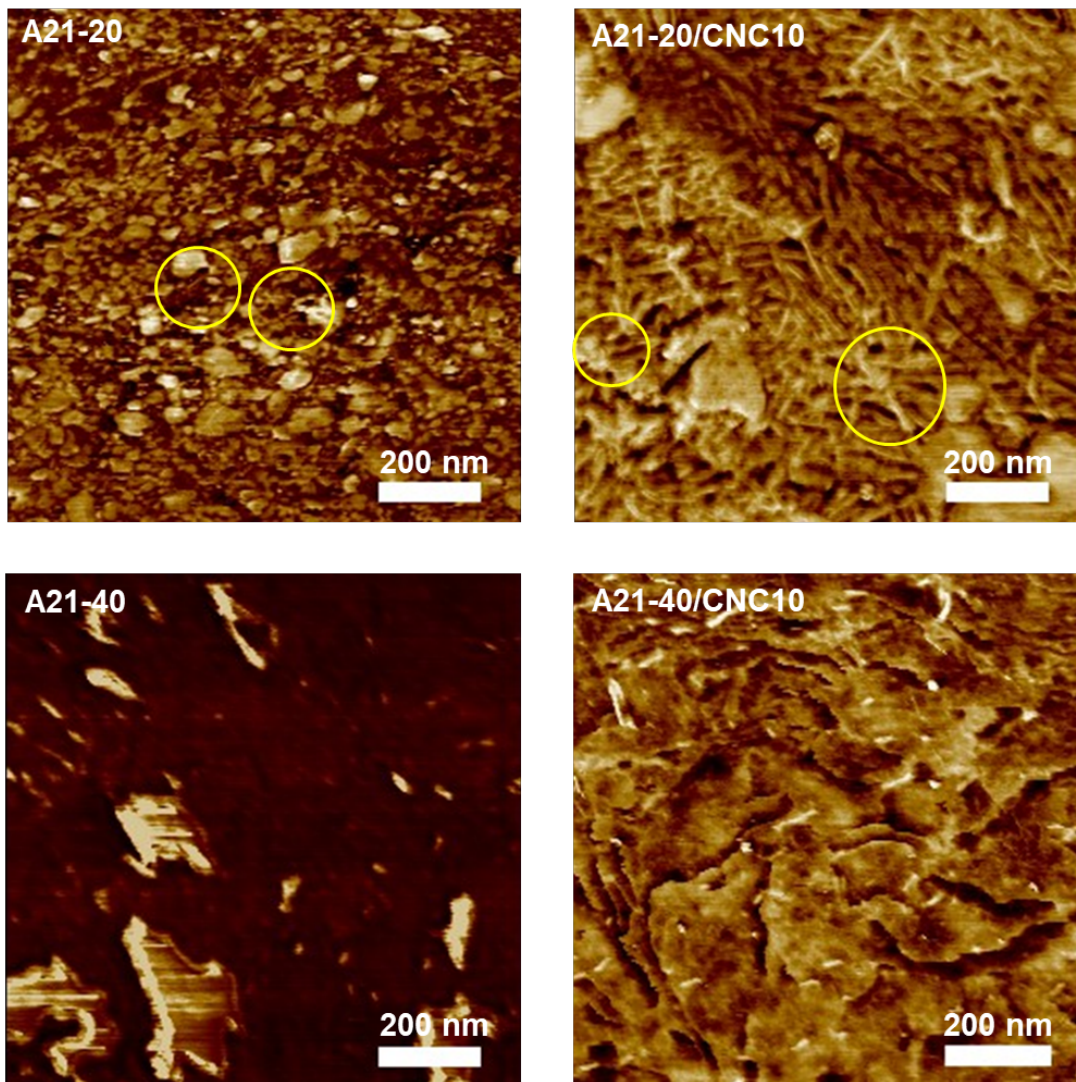
<sup>b</sup> Calculated from GPC using DMAc/0.5 wt% of LiBr as the eluent and PMMA as standards.

**Figure S2. (A)** GPC traces for the synthesized PEG-HDI PU (control) and PPU (A21-20 and A21-40) **(B)** Table summarizing the PBLA weight fraction, number-average molecular weight ( $M_n$ ) and dispersity ( $\mathcal{D}$ ) of the synthesized control and PPU.

**Equation S1.** PBLA content for PPU samples

$$\text{wt\% (PBLA)} = 100 \times \left( \frac{xM_{\text{PBLA}}}{xM_{\text{PBLA}} + yM_{\text{PEG}} + zM_{\text{HDI}}} \right)$$

where  $x$ ,  $y$  and  $z$  are the molar quantities of the PBLA, PEG, and HDI, respectively, and  $M_{\text{PBLA}}$ ,  $M_{\text{PEG}}$  and  $M_{\text{HDI}}$  are the molecular weights of PBLA, PEG and HDI, respectively.



**Figure S3.** Magnified AFM phase images of the surface of dried PPU and PPU/CNC nanocomposite films (1 x1  $\mu\text{m}$ ). Yellow circles indicate the interconnected rods.

## Mathematical model to predict Young's modulus

The **Halpin-Tsai Model**<sup>1</sup> is used to predict the mechanical properties of composites containing randomly oriented nanofibers. This model excludes filler-filler interactions, assuming that fillers are dispersed homogeneously in a polymer matrix *via* ideal filler-matrix interactions. The extent of reinforcement is determined by the following factors: 1) individual mechanical properties of the pristine matrix and the filler material, 2) the filler aspect ratio, 3) the degree of filler alignment, and 4) the filler volume fraction.

$$E_{c,L} = \frac{E_m(1 + 2\frac{L}{D}\eta_L\varphi_f)}{(1 - \eta_L\varphi_f)}, \quad \eta_L = \frac{E_f - E_m}{E_f + 2\frac{L}{D}E_m}$$

$$E_{c,T} = \frac{E_m(1 + 2\eta_T\varphi_f)}{(1 - \eta_T\varphi_f)}, \quad \eta_T = \frac{E_f - E_m}{E_f + 2E_m}$$

$$E_{c,R} = aE_{c,L} + (1 - a)E_{c,T}$$

$$a = 0.13 + 0.0815\varphi_f - 1.669\frac{E_m}{E_f}$$

Where  $E$  indicates Young's modulus:  $E_L$  is longitudinal modulus  $E_c$  transverse modulus, and  $E_R$  is the modulus of a randomly oriented composite. The subscripts m, f, and c are assigned to the matrix, filler, and composite, respectively.  $L/D$  is the filler aspect ratio (*i.e.*, the ratio of the longest dimension (length) to the shortest dimension (diameter)).  $a$  is defined as the weight fraction.  $\varphi_f$  is the volume fraction of the filler.

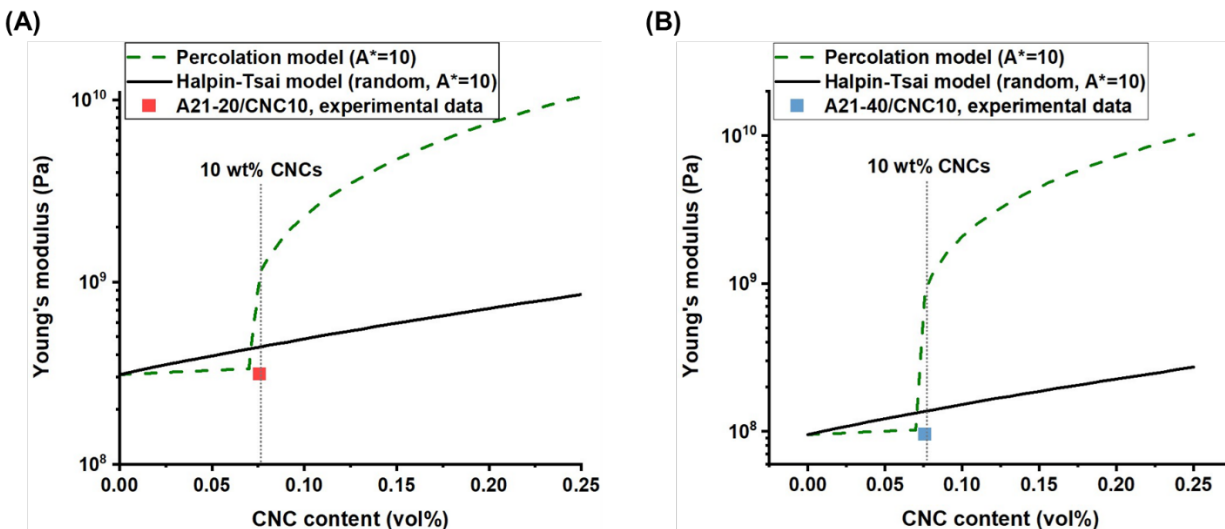
The **Percolation model**<sup>2-3</sup> describes systems exhibiting strong filler-filler interactions, yielding a rigid network above a critical filler fraction (*i.e.*, percolation threshold). Above the percolation threshold ( $\varphi_t$ ), the modulus of the composite ( $E_c$ ) is mostly determined by the rigidity of the filler network ( $E_f$ ).

$$E_c = \frac{(1 - 2\Psi + \Psi\varphi_f)E_mE_f + (1 - \varphi_f)\Psi E_f^2}{(1 - \varphi_f)E_f + (\varphi_f - \Psi)E_m}$$

$$f(x) = \begin{cases} 0 & , \quad \varphi_f \leq \varphi_t \\ \varphi_f \left( \frac{\varphi_f - \varphi_t}{1 - \varphi_t} \right)^{0.4} & , \quad \varphi_f > \varphi_t \end{cases}$$

For simplicity, it is assumed that the filler distribution is isotropic, and the aspect ratio is fixed to calculate  $\varphi_t$  using the equation below.

$$\varphi_t = \frac{\frac{2L}{D} + \frac{4}{3}}{\frac{32}{3} \left[ 1 + \frac{3}{2} \left( \frac{L}{D} \right) + \frac{3}{8} \left( \frac{L}{D} \right)^2 \right]}$$



**Figure S4.** Experimental Young's modulus of **(A)** A21-20/CNC10 and **(B)** A21-40/CNC10 nanocomposites compared with the percolation model (green dash curve) and the Halpin-Tsai model for randomly-oriented CNCs (black solid line). Based on the supplier's information on CNCs, the aspect ratio ( $A^*$ ) was set to 10 for model fitting.

**Table S1.** Swelling behavior of PPU as a function of PBLA and CNC content.

Sample	PBLA content (%)	CNC content (wt%)	Swelling ratio (%)
PEG-HDI PU	0	0	N/A (dissolved)
A21-20	20	0	780
A21-40	40	0	195
A21-20/CNC10	20	10	1080
A21-40/CNC10	40	10	380

**Table S2.** List of the values for the extent of water-responsive stiffness change ( $\Delta E = E'_{\text{dry}} - E'_{\text{wet}}$ ) for various polymer/cellulose nanocomposites (from the literature and from this study) with 10 wt% of nanocellulose (NC). These values were used to plot **Figure 6C**.

Matrix type	Nanocellulose content (wt%)	$E'_{\text{dry}}$ of matrix (MPa)	Average $\Delta E$ of matrix (MPa)	$E'_{\text{dry}}$ of polymer/cellulose nanocomposite (MPa)	Average $\Delta E$ of polymer/cellulose nanocomposite (MPa)	Nomenclature for nanocomposite	Ref.
Natural rubber (NR)	10	1	0	1.8	0.2	NR/NC10	[4]
Epoxidized natural (ENR)	10	1.5	0	10	8	ENR/NC10	[4]
Poly(styrene-co-butadiene) (SBR)	10	1	0	73	61	SBR/NC10	[5]
Polybutadiene (PBD)	10	0.5	0	94	72	PBD/NC10	[5]
Polyether-based polyurethane (PU)	10	16	-	125	78	PU/NC10	[6]
Thermoplastic polyurethane (TPU)	10	12	0	200	50	TPU/NC10	[7]
Peptide-polyurea	0			212	210	A21-20	Our work
Peptide-polyurea	0			88	73	A21-40	Our work
Peptide-polyurea	10	212	210	385	397	A21-20/CNC10	Our work
Peptide-polyurea	10	88	73	360	334	A21-40/CNC10	Our work



## References

1. J.C. Halpin, *Journal of Composite Materials*, 1969, **3**, 732 – 734.
2. M. Takayanagi, S. Uemura, S. Minami, *Journal of Polymer Science Part C: Polymer Symposia*, 1964, **5**, 113– 122.
3. N. Ouali, J. Cavaille, J. Perez, *Plastics, Rubber and Composites Processing and Applications*, 1991, **16**, 55-60.
4. M. Tian, X. Zhen, Z. Wang, H. Zou, L. Zhang and N. Ning, *ACS Appl. Mater. Interfaces*, 2017, **9**, 6482-6487.
5. K. L. Dagnon, K. Shanmuganathan, C. Weder and S. J. Rowan, *Macromolecules*, 2012, **45**, 4707-4715.
6. Y. Wang, Z. Cheng, Z. Liu, H. Kang and Y. Liu, *J. Mater. Chem. B*, 2018, **6**, 1668-1677.
7. Y. Zhu, J. Hu, H. Luo, R. J. Young, L. Deng, S. Zhang, Y. Fan and G. Ye, *Soft Matter*, 2012, **8**, 2509-2517.