

# Thermochemical production of ammonia via a two-step metal nitride cycle – Materials screening and the Strontium-based system

Daniel Notter,<sup>a</sup> Tiago Elias Abi-Ramia Silva,<sup>a</sup> María Elena Gálvez,<sup>b</sup> Brendan Bulfin,<sup>c</sup> and Aldo Steinfeld<sup>a,\*</sup>

## Supplementary Information

### 1. Theoretical Screening

#### 1.1 Formulation

Data was obtained from the Materials Project database (MP, database version: v2023.11.1)<sup>1</sup>. The Python library pymatgen (Python Material Genomics)<sup>2</sup> was used for the calculations. The essential data exported were the energy above convex hull per atom  $E_{hull}$ , the formation energy per atom  $E_{form}$ , and the elastic tensor  $C_{ij}$ .

The calculation of the heat capacity is based on the Debye model.<sup>3,4</sup> Longitudinal and transverse sound velocities  $v_l$  and  $v_t$  are calculated with the pymatgen functions `long_v` and `trans_v` which use the Voigt-Reuss-Hill average bulk modulus derived from the elastic tensor  $C_{ij}$ . The volume of the primitive cell  $v_0$  is

$$v_0 = \frac{v}{n_{sites}} \quad (S1)$$

where  $v$  is the volume of the conventional unit cell and  $n_{sites}$  the number of sites in the unit cell. The average sound velocity  $v_m$  is defined as

$$v_m = \left( \frac{3}{\frac{1}{v_l^3} + \frac{2}{v_t^3}} \right)^{1/3} \quad (S2)$$

The Debye temperature  $\Theta_D$  is given as

$$\Theta_D = \frac{\hbar}{k_B} v_m \left( \frac{6\pi^2}{v_0} \right)^{1/3} \quad (S3)$$

where  $\hbar$  is the reduced Planck constant and  $k_B$  is the Boltzmann constant. The specific heat capacity at constant volume  $c_v$  can then be approximated as

$$c_v(T) = 9R \cdot n \cdot \left( \frac{T}{\Theta_D} \right)^3 \int_0^{\Theta_D/T} \frac{x^4 \cdot e^x}{(e^x - 1)^2} dx \quad (S4)$$

where  $n$  is the number of atoms and  $T$  is the temperature in Kelvin. With the assumption that the heat capacity ratio of a solid is nearly 1, the specific heat capacity at constant pressure  $c_p$  is approximated as:

$$c_p(T) = c_v(T) \quad (S5)$$

The entropy is directly calculated from the approximation of the specific heat capacity as:

$$s(T) = \int_{0K}^T \frac{c_p}{T} dT \quad (S6)$$

The standard enthalpy of formation  $h_f^o$  is approximated with the help of the formation energy per atom  $E_{form}$ :

$$h_f^o = E_{form} \cdot e \cdot N_A \cdot n \quad (S7)$$

The enthalpy is then calculated as:

$$h(T) = h_f^o + \int_{298K}^T c_p dT \quad (S8)$$

<sup>a,\*</sup> Department of Mechanical Engineering, ETH Zürich, 8092 Zürich, Switzerland

<sup>b</sup> Instituto de Nanociencia y Materiales de Aragón (INMA), CSIC-Universidad de Zaragoza, C/ Pedro Cerbuna 12, 50009 Zaragoza, Spain.

<sup>c</sup> School of Chemistry & Environmental Research Institute, University College Cork, T12 YN60 Cork, Ireland.

\* Corresponding author; Email: aldo.steinfeld@ethz.ch

## 1.2 Validation of Thermodynamic Data Approximation

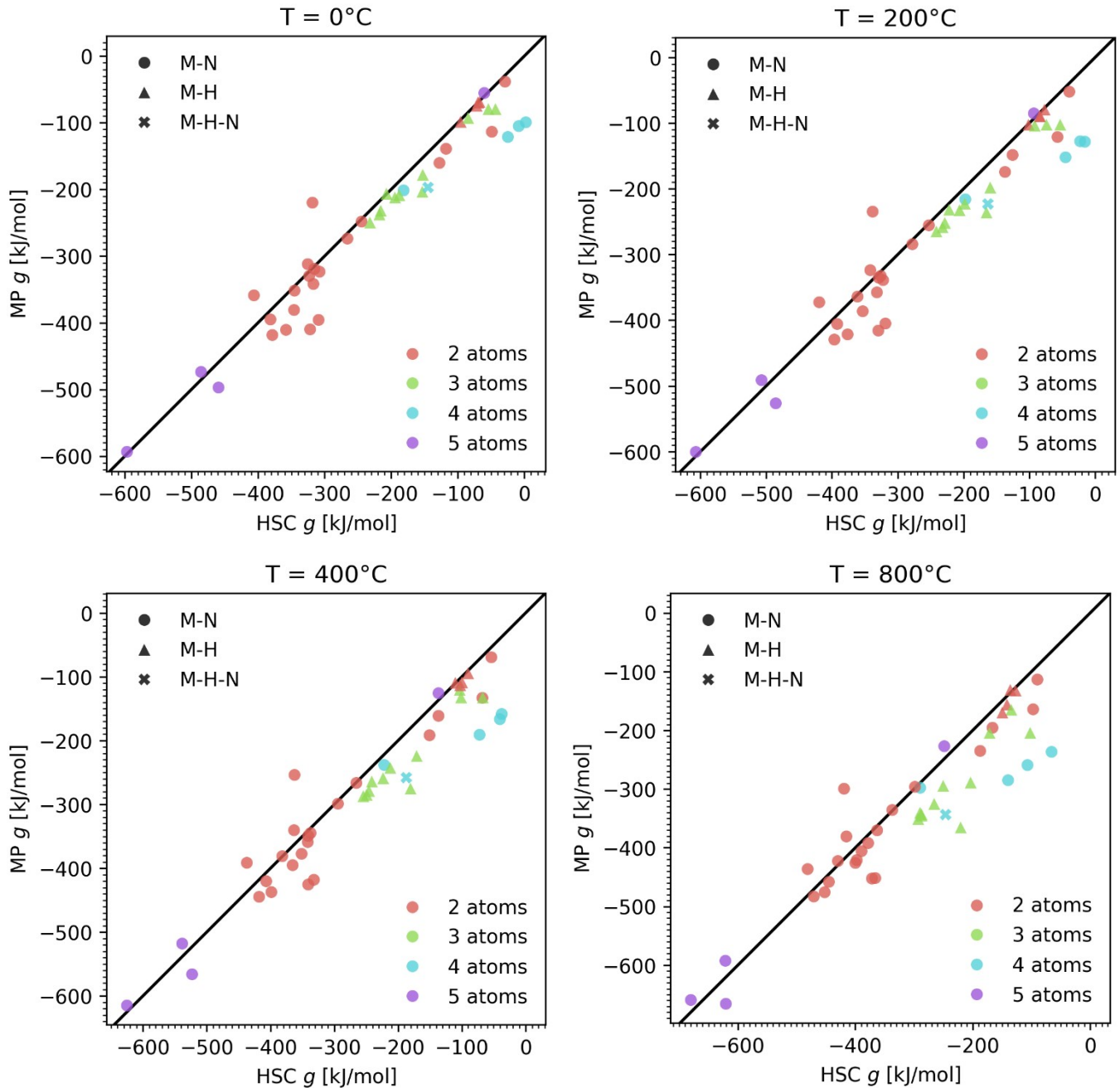


Figure S1: Comparison of Gibbs free energies calculated from MP database data, and Gibbs free energies taken from HSC database for 4 temperatures 0, 200, 400, 800 °C. The shape of the markers indicate the 3 type of materials: metal nitride (M-N), metal hydride (M-H), and metal imide (M-H-N). The color of the markers indicate the number of atoms (some MP data is calculated in eV/atom). The comparison included all available materials that were found in a stable form in both databases: 28 metal nitrides, 15 metal hydrides, 1 metal imide.

## 1.3 Source of thermodynamic data

Thermodynamic data was obtained from the Materials Project database (MP, database version: v2023.11.1) and from the HSC Chemistry 5 database (HSC). Some materials from the MP database were only used for the calculate of the stoichiometric weight changes since not all required properties for the calculations in Section 1.1 were available (marked with \*). When data was available from both databases, HSC data was given preference. The MP data was still used for validation purposes (marked with \*\*).

Table S1: The Al-based system

Formula	Source	mpid	E_hull [eV/atom]	E_form [eV/atom]	n
Al	HSC	-	-	-	-
Al <sub>3</sub> H*	MP	mp-1183138	0.413076	0.388532	4
AlH <sub>12</sub> *	MP	mp-1214891	0.12337	0.100714	13
AlH <sub>3</sub>	HSC	-	-	-	-
AlH <sub>6</sub> *	MP	mp-1214861	1.008702	0.966626	7

AlN	HSC	-	-	-	-
AlN**	MP	mp-661	0	-1.67967	2

Table S2: The Ca-based system

Formula	Source	mpid	E_hull [eV/atom]	E_form [eV/atom]	n
Ca	HSC	-	-	-	-
CaH2	HSC	-	-	-	-
CaH2**	MP	mp-23713	0	-0.66688	3
Ca(H2N)2*	MP	mp-644307	0	-0.6897	7
Ca16HN8*	MP	mp-675153	0.029588	-0.8758	25
Ca2HN*	MP	mp-24119	0	-0.94564	4
Ca8H3N4*	MP	mp-530696	0.05222	-0.88383	15
CaHN*	MP	mp-34932	0	-0.89293	3
Ca11N8*	MP	mp-680640	0.201076	-0.73335	19
Ca2N	MP	mp-2686	0	-0.89772	3
Ca3N2	HSC	-	-	-	-
Ca3N2**	MP	mp-844	0	-0.95972	5
CaN*	MP	mp-1058549	0.398168	-0.44138	2
CaN2	MP	mp-1009657	0	-0.63927	3
CaN6	MP	mp-676	0.040613	-0.23336	7

Table S3: The Co-based system

Formula	Source	mpid	E_hull [eV/atom]	E_form [eV/atom]	n
Co	HSC	-	-	-	-
Co3H	MP	mp-1025425	0.004233	-0.02174	4
Co4H*	MP	mp-1226072	0.012287	-0.00849	5
CoH*	MP	mp-1206874	0	-0.05194	2
CoH3*	MP	mp-1183678	0.153299	0.127328	4
Co2N	MP	mp-22631	0.177865	0.177865	3
Co3N	HSC	-	-	-	-
Co3N**	MP	mp-1205986	0.159141	0.159141	4
Co4N*	MP	mp-1206425	0.069595	0.069595	5
CoN	MP	mp-448	0.102861	0.102861	2
CoN12*	MP	mp-1194075	1.244613	1.244613	13
CoN3*	MP	mp-22762	0.383968	0.383968	4

Table S4: The Cr-based system

Formula	Source	mpid	E_hull [eV/atom]	E_form [eV/atom]	n
Cr	HSC	-	-	-	-
Cr3H*	MP	mp-1183723	0.757946	0.757946	4
CrH	MP	mp-24669	0.1659	0.1659	2
CrH2*	MP	mp-24208	0.00228	0.00228	3
CrH3*	MP	mp-1183679	0.123355	0.123355	4
Cr2N	HSC	-	-	-	-
Cr2N**	MP	mp-8780	0.244667	-0.25479	3
Cr3N2	MP	mp-1014303	0.087926	-0.51142	5
Cr3N4	MP	mp-1014460	0.277954	-0.36421	7

CrN	HSC	-	-	-	-
CrN**	MP	mp-2132	0	-0.74919	2
CrN2	MP	mp-1014993	0.296759	-0.2027	3

Table S5: The Cu-based system

Formula	Source	mpid	E_hull [eV/atom]	E_form [eV/atom]	n
Cu	HSC	-	-	-	-
CuH	MP	mp-24093	0.115168	0.115168	2
Cu10N3*	MP	mp-1225831	0.197459	0.197459	13
Cu2N*	MP	mp-1147700	0.351218	0.351218	3
Cu3N	MP	mp-1933	0.19208	0.19208	4
CuN	MP	mp-13117	0.795979	0.795979	2
CuN3	MP	mp-27954	0.293795	0.293795	4
CuN6	MP	mp-608366	0.339206	0.339206	7
CuN8*	MP	mp-1198545	1.244581	1.244581	9

Table S6: The Fe-based system

Formula	Source	mpid	E_hull [eV/atom]	E_form [eV/atom]	n
Fe	HSC	-	-	-	-
Fe3H*	MP	mp-984102	0.600378	0.566751	4
FeH	MP	mp-1009077	0	-0.06726	2
FeH3	MP	mp-1018061	0.182623	0.148996	4
FeH4*	MP	mp-1079939	0.243415	0.216513	5
Fe12N5*	MP	mp-27908	0.026315	-0.15899	17
Fe24N11*	MP	mp-684887	0.049817	-0.14807	35
Fe2N	HSC	-	-	-	-
Fe2N**	MP	mp-21476	0.056841	-0.15293	3
Fe3N	MP	mp-1804	0	-0.15778	4
Fe4N	HSC	-	-	-	-
Fe4N**	MP	mp-535	0.069992	-0.05623	5
Fe8N	MP	mp-555	0.001092	-0.06903	9
Fe8N3	MP	mp-673174	0.017508	-0.15445	11
FeN	MP	mp-6988	0	-0.31375	2
FeN2*	MP	mp-1080202	0.148476	-0.06069	3

Table S7: The Li-based system

Formula	Source	mpid	E_hull [eV/atom]	E_form [eV/atom]	n
Li	HSC	-	-	-	-
LiH	HSC	-	-	-	-
LiH**	MP	mp-23703	0	-0.48936	2
Li(H3N)4*	MP	mp-707454	0.02814	-0.41663	17
Li15H9N8*	MP	mp-1201065	0.005666	-0.5779	32
Li2HN*	MP	mp-1189725	0	-0.58257	4
Li3(HN)2*	MP	mp-1210795	0.184018	-0.38728	7
Li3H3N2*	MP	mp-977164	0.0236	-0.56295	8
Li4HN*	MP	mp-30228	0	-0.4702	6
Li7H5N4*	MP	mp-1200910	0.005943	-0.57862	16



LiH2N	MP	mp-23702	0	-0.59054	4
Li2N*	MP	mp-1062345	0.263625	-0.17276	3
Li3N	HSC	-	-	-	-
Li3N**	MP	mp-2251	0	-0.4825	4
Li3N2*	MP	mp-1222421	0.759322	0.359824	5
LiN*	MP	mp-1059612	1.335792	0.99163	2
LiN3	MP	mp-2659	0	-0.20582	4

Table S8: The Mn-based system

Formula	Source	mpid	E_hull [eV/atom]	E_form [eV/atom]	n
Mn	HSC	-	-	-	-
Mn29H2*	MP	mp-1222194	0	-0.01634	31
MnH*	MP	mp-24416	0.150346	0.141612	2
Mn(H15N8)2*	MP	mp-1195097	0.009936	-0.36817	47
Mn(H2N)2*	MP	mp-703486	0.503855	0.08049	7
Mn2N	MP	mp-9981	0	-0.43548	3
Mn3N2	HSC	-	-	-	-
Mn3N4*	MP	mp-1080204	0.076293	-0.20366	7
Mn4N	HSC	-	-	-	-
Mn5N2	HSC	-	-	-	-
MnN	MP	mp-1009130	0.015086	-0.31153	2

Table S9: The Mo-based system

Formula	Source	mpid	E_hull [eV/atom]	E_form [eV/atom]	n
Mo	HSC	-	-	-	-
Mo2	HSC	-	-	-	-
Mo3H	MP	mp-975912	0.850179	0.850179	4
MoH	MP	mp-24417	0.393956	0.393956	2
Mo15N16*	MP	mp-530081	0	-0.53798	31
Mo2N	HSC	-	-	-	-
Mo2N**	MP	mp-27953	0.004064	-0.36008	3
Mo2N3*	MP	mp-1080195	0.155517	-0.28922	5
Mo3N2*	MP	mp-32652	0.571802	0.134825	5
MoN	HSC	-	-	-	-
MoN**	MP	mp-2811	0	-0.54622	2
MoN2	MP	mp-1402363	0.274727	-0.09588	3

Table S10: The Ni-based system

Formula	Source	mpid	E_hull [eV/atom]	E_form [eV/atom]	n
Ni	HSC	-	-	-	-
Ni2H	MP	mp-753890	0.046298	0.03888	3
Ni3H*	MP	mp-976948	0.515277	0.509713	4
NiH	MP	mp-24719	0	-0.01113	2
NiH0.5	HSC	-	-	-	-
NiH0.59	HSC	-	-	-	-
NiH0.68	HSC	-	-	-	-
NiH3*	MP	mp-973963	0.219315	0.213751	4
Ni(H2N)2*	MP	mp-28686	0.024374	-0.24142	7

Ni3N	HSC	-	-	-	-
Ni3N**	MP	mp-2033	0.014725	0.014725	4
Ni4N*	MP	mp-1094090	0.066688	0.066688	5
Ni4N3*	MP	mp-1094084	0.29447	0.29447	7
NiN	MP	mp-973933	0.31253	0.31253	2

Table S11: The Sr-based system

Formula	Source	mpid	E_hull [eV/atom]	E_form [eV/atom]	n
Sr	HSC	-	-	-	-
Sr3H*	MP	mp-1187129	0.68131	0.438468	4
SrH2	HSC	-	-	-	-
SrH2**	MP	mp-23714	0	-0.64758	3
SrH3	MP	mp-978856	0.340568	-0.14512	4
Sr(H2N)2*	MP	mp-643905	0	-0.65119	7
Sr2HN	MP	mp-690794	0	-0.75828	4
SrHN*	MP	mp-1187172	0	-0.82252	3
Sr2N	MP	mp-1245	0	-0.67197	3
Sr3N2	HSC	-	-	-	-
Sr3N2**	MP	mp-986716	0.03106	-0.63965	5
Sr4N3*	MP	mp-1173210	0.145913	-0.52426	7
SrN	MP	mp-29973	0	-0.66883	2
SrN2	MP	mp-10564	0	-0.62324	3
SrN6*	MP	mp-2131	0.009174	-0.25793	7

Table S12: The W-based system

Formula	Source	mpid	E_hull [eV/atom]	E_form [eV/atom]	n
W	HSC	-	-	-	-
W2N	HSC	-	-	-	-
W2N3*	MP	mp-1216242	0	-0.5573	5
W3N4	MP	mp-8102	0.365057	-0.16571	7
W7N6*	MP	mp-1216967	0.145784	-0.28291	13
WN	MP	mp-991	0.288264	-0.17616	2
WN18*	MP	mp-672264	0.304768	0.231438	19
WN2	MP	mp-2679804	0.063144	-0.40128	3
WN6*	MP	mp-1208477	2.410438	2.2114	7

Table S13: The Zn-based system

Formula	Source	mpid	E_hull [eV/atom]	E_form [eV/atom]	n
Zn	HSC	-	-	-	-
ZnH*		mp-971820	0.326733	0.326733	2
ZnH6*		mp-1207466	0.028949	0.028949	7
Zn(H15N8)2*		mp-1195558	0	-0.37232	47
Zn(H2N)2*		mp-24694	0	-0.41502	7
Zn(H4N5)2*		mp-1188715	0.12868	-0.14239	19
Zn3N*		mp-981366	0.769759	0.742932	4
Zn3N2	HSC	-	-	-	-
Zn3N2**		mp-9460	0	-0.04292	5
ZnN		mp-971911	0.555736	0.519967	2

ZnN6*		mp-1103897	0.089476	0.08187	7
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#### 1.4 Reactions

The following tables contain all reactions considered in the combined theoretical and experimental screenings. All possible combinations with the materials listed in Section 1.2 have been included. '*dm\_stoich [%]*' is the stoichiometric weight change in % from the reactant solid to the product solid. '*h298 [kJ/mol]*' is the standard enthalpy change of the reaction at 25°C. '*T\_eq [°C]*' is the equilibrium temperature. '*Type*' denotes if the reaction has an exergonic region, i.e. reaction proceeds spontaneously in the investigated temperature range 0-800°C.

Table S14: The Al-based system

ID	Reaction	dm_stoich [%]	h298 [kJ/mol]	T_eq [°C]	Type
Al-R01	$6\text{Al} + \text{H}_2 = 2\text{Al}_3\text{H}$	1.25	-	-	-
Al-R02	$1/6\text{Al} + \text{H}_2 = 1/6\text{AlH}_{12}$	44.83	-	-	-
Al-R03	$2/3\text{Al} + \text{H}_2 = 2/3\text{AlH}_3$	11.21	-7.6	-	endergonic
Al-R04	$1/3\text{Al} + \text{H}_2 = 1/3\text{AlH}_6$	22.41	-	-	-
Al-R05	$2/35\text{Al}_3\text{H} + \text{H}_2 = 6/35\text{AlH}_{12}$	43.05	-	-	-
Al-R06	$1/4\text{Al}_3\text{H} + \text{H}_2 = 3/4\text{AlH}_3$	9.84	-	-	-
Al-R07	$2/17\text{Al}_3\text{H} + \text{H}_2 = 6/17\text{AlH}_6$	20.91	-	-	-
Al-R08	$2/9\text{AlH}_3 + \text{H}_2 = 2/9\text{AlH}_{12}$	30.23	-	-	-
Al-R09	$2/3\text{AlH}_3 + \text{H}_2 = 2/3\text{AlH}_6$	10.08	-	-	-
Al-R10	$1/3\text{AlH}_6 + \text{H}_2 = 1/3\text{AlH}_{12}$	18.31	-	-	-
Al-R11	$6\text{AlN} + \text{H}_2 = 2\text{Al}_3\text{H} + 3\text{N}_2$	-33.35	-	-	-
Al-R12	$1/6\text{AlN} + \text{H}_2 = 1/6\text{AlH}_{12} + 1/12\text{N}_2$	-4.66	-	-	-
Al-R13	$2/3\text{AlN} + \text{H}_2 = 2/3\text{AlH}_3 + 1/3\text{N}_2$	-26.79	204.39	-	endergonic
Al-R14	$1/3\text{AlN} + \text{H}_2 = 1/3\text{AlH}_6 + 1/6\text{N}_2$	-19.42	-	-	-
Al-R15	$2/3\text{AlN} + \text{H}_2 = 2/3\text{Al} + 2/3\text{NH}_3$	-34.17	181.39	-	endergonic
Al-R16	$3/5\text{AlN} + \text{H}_2 = 1/5\text{Al}_3\text{H} + 3/5\text{NH}_3$	-33.35	-	-	-
Al-R17	$2/15\text{AlN} + \text{H}_2 = 2/15\text{AlH}_{12} + 2/15\text{NH}_3$	-4.66	-	-	-
Al-R18	$1/3\text{AlN} + \text{H}_2 = 1/3\text{AlH}_3 + 1/3\text{NH}_3$	-26.79	86.9	-	endergonic
Al-R19	$2/9\text{AlN} + \text{H}_2 = 2/9\text{AlH}_6 + 2/9\text{NH}_3$	-19.42	-	-	-
Al-R20	$2\text{Al} + \text{N}_2 = 2\text{AlN}$	51.91	-635.97	-	exergonic
Al-R21	$2/3\text{Al}_3\text{H} + \text{N}_2 = 2\text{AlN} + 1/3\text{H}_2$	50.04	-	-	-
Al-R22	$6\text{Al}_3\text{H} + \text{N}_2 = 18\text{Al} + 2\text{NH}_3$	-1.23	-	-	-
Al-R23	$3/5\text{Al}_3\text{H} + \text{N}_2 = 9/5\text{AlN} + 1/5\text{NH}_3$	50.04	-	-	-
Al-R24	$2\text{AlH}_{12} + \text{N}_2 = 2\text{AlN} + 12\text{H}_2$	4.89	-	-	-
Al-R25	$1/2\text{AlH}_{12} + \text{N}_2 = 1/2\text{Al} + 2\text{NH}_3$	-30.95	-	-	-
Al-R26	$18/35\text{AlH}_{12} + \text{N}_2 = 6/35\text{Al}_3\text{H} + 2\text{NH}_3$	-30.09	-	-	-
Al-R27	$2/3\text{AlH}_{12} + \text{N}_2 = 2/3\text{AlH}_3 + 2\text{NH}_3$	-23.22	-	-	-
Al-R28	$\text{AlH}_{12} + \text{N}_2 = \text{AlH}_6 + 2\text{NH}_3$	-15.48	-	-	-
Al-R29	$2/5\text{AlH}_{12} + \text{N}_2 = 2/5\text{AlN} + 8/5\text{NH}_3$	4.89	-	-	-

Al-R30	$2\text{AlH}_3 + \text{N}_2 = 2\text{AlN} + 3\text{H}_2$	36.6	-613.17	-	exergonic
Al-R31	$2\text{AlH}_3 + \text{N}_2 = 2\text{Al} + 2\text{NH}_3$	-10.08	-69	-	exergonic
Al-R32	$9/4\text{AlH}_3 + \text{N}_2 = 3/4\text{Al}_3\text{H} + 2\text{NH}_3$	-8.96	-	-	-
Al-R33	$\text{AlH}_3 + \text{N}_2 = \text{AlN} + \text{NH}_3$	36.6	-352.48	-	exergonic
Al-R34	$2\text{AlH}_6 + \text{N}_2 = 2\text{AlN} + 6\text{H}_2$	24.1	-	-	-
Al-R35	$\text{AlH}_6 + \text{N}_2 = \text{Al} + 2\text{NH}_3$	-18.31	-	-	-
Al-R36	$18/17\text{AlH}_6 + \text{N}_2 = 6/17\text{Al}_3\text{H} + 2\text{NH}_3$	-17.29	-	-	-
Al-R37	$2\text{AlH}_6 + \text{N}_2 = 2\text{AlH}_3 + 2\text{NH}_3$	-9.16	-	-	-
Al-R38	$2/3\text{AlH}_6 + \text{N}_2 = 2/3\text{AlN} + 4/3\text{NH}_3$	24.1	-	-	-

Table S15: The Ca-based system

ID	Reaction	dm_stoich [%]	h298 [kJ/mol]	T_eq [°C]	Type
Ca-R001	$\text{Ca} + \text{H}_2 = \text{CaH}_2$	5.03	-176.98	-	exergonic
Ca-R002	$2/3\text{Ca} + \text{H}_2 = 2/3\text{CaH}_3$	7.55	-	-	-
Ca-R003	$\text{Ca}(\text{H}_2\text{N})_2 + \text{H}_2 = \text{Ca} + 2\text{NH}_3$	-44.43	-	-	-
Ca-R004	$1/2\text{Ca}(\text{H}_2\text{N})_2 + \text{H}_2 = 1/2\text{CaH}_2 + \text{NH}_3$	-41.64	-	-	-
Ca-R005	$2/5\text{Ca}(\text{H}_2\text{N})_2 + \text{H}_2 = 2/5\text{CaH}_3 + 4/5\text{NH}_3$	-40.24	-	-	-
Ca-R006	$32/9\text{Ca}(\text{H}_2\text{N})_2 + \text{H}_2 = 2/9\text{Ca}_{16}\text{HN}_8 + 16/3\text{NH}_3$	-34.63	-	-	-
Ca-R007	$2\text{Ca}(\text{H}_2\text{N})_2 + \text{H}_2 = \text{Ca}_2\text{HN} + 3\text{NH}_3$	-34.02	-	-	-
Ca-R008	$16/7\text{Ca}(\text{H}_2\text{N})_2 + \text{H}_2 = 2/7\text{Ca}_8\text{H}_3\text{N}_4 + 24/7\text{NH}_3$	-34.2	-	-	-
Ca-R009	$4\text{Ca}(\text{H}_2\text{N})_2 + \text{H}_2 = 2\text{Ca}_2\text{N} + 6\text{NH}_3$	-34.72	-	-	-
Ca-R010	$1/11\text{Ca}_{11}\text{N}_8 + \text{H}_2 = \text{CaH}_2 + 4/11\text{N}_2$	-16.26	-	-	-
Ca-R011	$2/33\text{Ca}_{11}\text{N}_8 + \text{H}_2 = 2/3\text{CaH}_3 + 8/33\text{N}_2$	-14.25	-	-	-
Ca-R012	$32/11\text{Ca}_{11}\text{N}_8 + \text{H}_2 = 2\text{Ca}_{16}\text{HN}_8 + 40/11\text{N}_2$	-6.21	-	-	-
Ca-R013	$4/11\text{Ca}_{11}\text{N}_8 + \text{H}_2 = 2\text{Ca}_2\text{HN} + 5/11\text{N}_2$	-5.33	-	-	-
Ca-R014	$16/33\text{Ca}_{11}\text{N}_8 + \text{H}_2 = 2/3\text{Ca}_8\text{H}_3\text{N}_4 + 20/33\text{N}_2$	-5.58	-	-	-
Ca-R015	$1/12\text{Ca}_{11}\text{N}_8 + \text{H}_2 = 11/12\text{Ca} + 2/3\text{NH}_3$	-20.27	-	-	-
Ca-R016	$1/23\text{Ca}_{11}\text{N}_8 + \text{H}_2 = 11/23\text{CaH}_2 + 8/23\text{NH}_3$	-16.26	-	-	-
Ca-R017	$2/57\text{Ca}_{11}\text{N}_8 + \text{H}_2 = 22/57\text{CaH}_3 + 16/57\text{NH}_3$	-14.25	-	-	-
Ca-R018	$32/131\text{Ca}_{11}\text{N}_8 + \text{H}_2 = 22/131\text{Ca}_{16}\text{HN}_8 + 80/131\text{NH}_3$	-6.21	-	-	-
Ca-R019	$2/13\text{Ca}_{11}\text{N}_8 + \text{H}_2 = 11/13\text{Ca}_2\text{HN} + 5/13\text{NH}_3$	-5.33	-	-	-
Ca-R020	$16/93\text{Ca}_{11}\text{N}_8 + \text{H}_2 = 22/93\text{Ca}_8\text{H}_3\text{N}_4 + 40/93\text{NH}_3$	-5.58	-	-	-
Ca-R021	$4/15\text{Ca}_{11}\text{N}_8 + \text{H}_2 = 22/15\text{Ca}_2\text{N} + 2/3\text{NH}_3$	-6.33	-	-	-
Ca-R022	$\text{Ca}_{11}\text{N}_8 + \text{H}_2 = 11/3\text{Ca}_3\text{N}_2 + 2/3\text{NH}_3$	-1.69	-	-	-
Ca-R023	$2/31\text{Ca}_{16}\text{HN}_8 + \text{H}_2 = 32/31\text{CaH}_2 + 8/31\text{N}_2$	-10.71	-	-	-
Ca-R024	$2/47\text{Ca}_{16}\text{HN}_8 + \text{H}_2 = 32/47\text{CaH}_3 + 8/47\text{N}_2$	-8.57	-	-	-
Ca-R025	$2/7\text{Ca}_{16}\text{HN}_8 + \text{H}_2 = 16/7\text{Ca}_2\text{HN}$	0.94	-	-	-
Ca-R026	$2/5\text{Ca}_{16}\text{HN}_8 + \text{H}_2 = 4/5\text{Ca}_8\text{H}_3\text{N}_4$	0.67	-	-	-
Ca-R027	$2/23\text{Ca}_{16}\text{HN}_8 + \text{H}_2 = 32/23\text{Ca} + 16/23\text{NH}_3$	-14.99	-	-	-
Ca-R028	$2/55\text{Ca}_{16}\text{HN}_8 + \text{H}_2 = 32/55\text{CaH}_2 + 16/55\text{NH}_3$	-10.71	-	-	-
Ca-R029	$2/71\text{Ca}_{16}\text{HN}_8 + \text{H}_2 = 32/71\text{CaH}_3 + 16/71\text{NH}_3$	-8.57	-	-	-
Ca-R030	$2/3\text{Ca}_2\text{HN} + \text{H}_2 = 4/3\text{CaH}_2 + 1/3\text{N}_2$	-11.54	-	-	-
Ca-R031	$2/5\text{Ca}_2\text{HN} + \text{H}_2 = 4/5\text{CaH}_3 + 1/5\text{N}_2$	-9.42	-	-	-
Ca-R032	$\text{Ca}_2\text{HN} + \text{H}_2 = 2\text{Ca} + \text{NH}_3$	-15.78	-	-	-
Ca-R033	$1/3\text{Ca}_2\text{HN} + \text{H}_2 = 2/3\text{CaH}_2 + 1/3\text{NH}_3$	-11.54	-	-	-

Ca-R034	$1/4\text{Ca}_2\text{HN} + \text{H}_2 = 1/2\text{CaH}_3 + 1/4\text{NH}_3$	-9.42	-	-	-
Ca-R035	$1/2\text{Ca}_2\text{N} + \text{H}_2 = \text{CaH}_2 + 1/4\text{N}_2$	-10.59	-47.06	235.2	exergonic
Ca-R036	$1/3\text{Ca}_2\text{N} + \text{H}_2 = 2/3\text{CaH}_3 + 1/6\text{N}_2$	-8.45	-	-	-
Ca-R037	$16\text{Ca}_2\text{N} + \text{H}_2 = 2\text{Ca}_{16}\text{HN}_8$	0.13	-	-	-
Ca-R038	$2\text{Ca}_2\text{N} + \text{H}_2 = 2\text{Ca}_2\text{HN}$	1.07	-	-	-
Ca-R039	$8/3\text{Ca}_2\text{N} + \text{H}_2 = 2/3\text{Ca}_8\text{H}_3\text{N}_4$	0.8	-	-	-
Ca-R040	$2/3\text{Ca}_2\text{N} + \text{H}_2 = 4/3\text{Ca} + 2/3\text{NH}_3$	-14.88	142.63	-	endergonic
Ca-R041	$2/7\text{Ca}_2\text{N} + \text{H}_2 = 4/7\text{CaH}_2 + 2/7\text{NH}_3$	-10.59	-40	216.4	exergonic
Ca-R042	$2/9\text{Ca}_2\text{N} + \text{H}_2 = 4/9\text{CaH}_3 + 2/9\text{NH}_3$	-8.45	-	-	-
Ca-R043	$1/3\text{Ca}_3\text{N}_2 + \text{H}_2 = \text{CaH}_2 + 1/3\text{N}_2$	-14.82	-33.31	259.7	exergonic
Ca-R044	$2/9\text{Ca}_3\text{N}_2 + \text{H}_2 = 2/3\text{CaH}_3 + 2/9\text{N}_2$	-12.78	-	-	-
Ca-R045	$32/3\text{Ca}_3\text{N}_2 + \text{H}_2 = 2\text{Ca}_{16}\text{HN}_8 + 8/3\text{N}_2$	-4.6	-	-	-
Ca-R046	$4/3\text{Ca}_3\text{N}_2 + \text{H}_2 = 2\text{Ca}_2\text{HN} + 1/3\text{N}_2$	-3.7	-	-	-
Ca-R047	$16/9\text{Ca}_3\text{N}_2 + \text{H}_2 = 2/3\text{Ca}_8\text{H}_3\text{N}_4 + 4/9\text{N}_2$	-3.96	-	-	-
Ca-R048	$1/3\text{Ca}_3\text{N}_2 + \text{H}_2 = \text{Ca} + 2/3\text{NH}_3$	-18.9	113.07	-	endergonic
Ca-R049	$1/6\text{Ca}_3\text{N}_2 + \text{H}_2 = 1/2\text{CaH}_2 + 1/3\text{NH}_3$	-14.82	-31.96	220.2	exergonic
Ca-R050	$2/15\text{Ca}_3\text{N}_2 + \text{H}_2 = 2/5\text{CaH}_3 + 4/15\text{NH}_3$	-12.78	-	-	-
Ca-R051	$32/27\text{Ca}_3\text{N}_2 + \text{H}_2 = 2/9\text{Ca}_{16}\text{HN}_8 + 16/27\text{NH}_3$	-4.6	-	-	-
Ca-R052	$2/3\text{Ca}_3\text{N}_2 + \text{H}_2 = \text{Ca}_2\text{HN} + 1/3\text{NH}_3$	-3.7	-	-	-
Ca-R053	$16/21\text{Ca}_3\text{N}_2 + \text{H}_2 = 2/7\text{Ca}_8\text{H}_3\text{N}_4 + 8/21\text{NH}_3$	-3.96	-	-	-
Ca-R054	$4/3\text{Ca}_3\text{N}_2 + \text{H}_2 = 2\text{Ca}_2\text{N} + 2/3\text{NH}_3$	-4.72	24.39	170.3	exergonic
Ca-R055	$2/13\text{Ca}_8\text{H}_3\text{N}_4 + \text{H}_2 = 16/13\text{CaH}_2 + 4/13\text{N}_2$	-11.31	-	-	-
Ca-R056	$2/21\text{Ca}_8\text{H}_3\text{N}_4 + \text{H}_2 = 16/21\text{CaH}_3 + 4/21\text{N}_2$	-9.18	-	-	-
Ca-R057	$2\text{Ca}_8\text{H}_3\text{N}_4 + \text{H}_2 = 8\text{Ca}_2\text{HN}$	0.27	-	-	-
Ca-R058	$2/9\text{Ca}_8\text{H}_3\text{N}_4 + \text{H}_2 = 16/9\text{Ca} + 8/9\text{NH}_3$	-15.55	-	-	-
Ca-R059	$2/25\text{Ca}_8\text{H}_3\text{N}_4 + \text{H}_2 = 16/25\text{CaH}_2 + 8/25\text{NH}_3$	-11.31	-	-	-
Ca-R060	$2/33\text{Ca}_8\text{H}_3\text{N}_4 + \text{H}_2 = 16/33\text{CaH}_3 + 8/33\text{NH}_3$	-9.18	-	-	-
Ca-R061	$2\text{CaH}_2 + \text{H}_2 = 2\text{CaH}_3$	2.39	-	-	-
Ca-R062	$2\text{CaHN} + \text{H}_2 = 2\text{CaH}_2 + \text{N}_2$	-23.59	-	-	-
Ca-R063	$\text{CaHN} + \text{H}_2 = \text{CaH}_3 + 1/2\text{N}_2$	-21.77	-	-	-
Ca-R064	$\text{CaHN} + \text{H}_2 = \text{Ca} + \text{NH}_3$	-27.25	-	-	-
Ca-R065	$1/2\text{CaHN} + \text{H}_2 = 1/2\text{CaH}_2 + 1/2\text{NH}_3$	-23.59	-	-	-
Ca-R066	$2/5\text{CaHN} + \text{H}_2 = 2/5\text{CaH}_3 + 2/5\text{NH}_3$	-21.77	-	-	-
Ca-R067	$32/9\text{CaHN} + \text{H}_2 = 2/9\text{Ca}_{16}\text{HN}_8 + 16/9\text{NH}_3$	-14.43	-	-	-
Ca-R068	$2\text{CaHN} + \text{H}_2 = \text{Ca}_2\text{HN} + \text{NH}_3$	-13.63	-	-	-
Ca-R069	$16/7\text{CaHN} + \text{H}_2 = 2/7\text{Ca}_8\text{H}_3\text{N}_4 + 8/7\text{NH}_3$	-13.86	-	-	-
Ca-R070	$4\text{CaHN} + \text{H}_2 = 2\text{Ca}_2\text{N} + 2\text{NH}_3$	-14.54	-	-	-
Ca-R071	$\text{CaN} + \text{H}_2 = \text{CaH}_2 + 1/2\text{N}_2$	-22.17	-	-	-
Ca-R072	$2/3\text{CaN} + \text{H}_2 = 2/3\text{CaH}_3 + 1/3\text{N}_2$	-20.31	-	-	-
Ca-R073	$32\text{CaN} + \text{H}_2 = 2\text{Ca}_{16}\text{HN}_8 + 8\text{N}_2$	-12.83	-	-	-
Ca-R074	$4\text{CaN} + \text{H}_2 = 2\text{Ca}_2\text{HN} + \text{N}_2$	-12.02	-	-	-
Ca-R075	$16/3\text{CaN} + \text{H}_2 = 2/3\text{Ca}_8\text{H}_3\text{N}_4 + 4/3\text{N}_2$	-12.25	-	-	-
Ca-R076	$2\text{CaN} + \text{H}_2 = 2\text{CaHN}$	1.86	-	-	-
Ca-R077	$2/3\text{CaN} + \text{H}_2 = 2/3\text{Ca} + 2/3\text{NH}_3$	-25.9	-	-	-
Ca-R078	$2/5\text{CaN} + \text{H}_2 = 2/5\text{CaH}_2 + 2/5\text{NH}_3$	-22.17	-	-	-
Ca-R079	$1/3\text{CaN} + \text{H}_2 = 1/3\text{CaH}_3 + 1/3\text{NH}_3$	-20.31	-	-	-
Ca-R080	$32/25\text{CaN} + \text{H}_2 = 2/25\text{Ca}_{16}\text{HN}_8 + 16/25\text{NH}_3$	-12.83	-	-	-
Ca-R081	$\text{CaN} + \text{H}_2 = 1/2\text{Ca}_2\text{HN} + 1/2\text{NH}_3$	-12.02	-	-	-
Ca-R082	$16/15\text{CaN} + \text{H}_2 = 2/15\text{Ca}_8\text{H}_3\text{N}_4 + 8/15\text{NH}_3$	-12.25	-	-	-

Ca-R083	$22/9\text{CaN} + \text{H}_2 = 2/9\text{Ca}_{11}\text{N}_8 + 2/3\text{NH}_3$	-7.06	-	-	-
Ca-R084	$4/3\text{CaN} + \text{H}_2 = 2/3\text{Ca}_2\text{N} + 2/3\text{NH}_3$	-12.95	-	-	-
Ca-R085	$2\text{CaN} + \text{H}_2 = 2/3\text{Ca}_3\text{N}_2 + 2/3\text{NH}_3$	-8.63	-	-	-
Ca-R086	$\text{CaN}_2 + \text{H}_2 = \text{CaH}_2 + \text{N}_2$	-38.18	8.05	-	exergonic
Ca-R087	$2/3\text{CaN}_2 + \text{H}_2 = 2/3\text{CaH}_3 + 2/3\text{N}_2$	-36.7	-	-	-
Ca-R088	$1/2\text{CaN}_2 + \text{H}_2 = 1/2\text{Ca}(\text{H}_2\text{N})_2$	5.92	-	-	-
Ca-R089	$32\text{CaN}_2 + \text{H}_2 = 2\text{Ca}_{16}\text{HN}_8 + 24\text{N}_2$	-30.76	-	-	-
Ca-R090	$4\text{CaN}_2 + \text{H}_2 = 2\text{Ca}_2\text{HN} + 3\text{N}_2$	-30.12	-	-	-
Ca-R091	$16/3\text{CaN}_2 + \text{H}_2 = 2/3\text{Ca}_8\text{H}_3\text{N}_4 + 4\text{N}_2$	-30.3	-	-	-
Ca-R092	$2\text{CaN}_2 + \text{H}_2 = 2\text{CaHN} + \text{N}_2$	-19.09	-	-	-
Ca-R093	$1/3\text{CaN}_2 + \text{H}_2 = 1/3\text{Ca} + 2/3\text{NH}_3$	-41.14	31.08	-	endergonic
Ca-R094	$1/4\text{CaN}_2 + \text{H}_2 = 1/4\text{CaH}_2 + 1/2\text{NH}_3$	-38.18	-20.94	228.3	exergonic
Ca-R095	$2/9\text{CaN}_2 + \text{H}_2 = 2/9\text{CaH}_3 + 4/9\text{NH}_3$	-36.7	-	-	-
Ca-R096	$32/73\text{CaN}_2 + \text{H}_2 = 2/73\text{Ca}_{16}\text{HN}_8 + 48/73\text{NH}_3$	-30.76	-	-	-
Ca-R097	$2/5\text{CaN}_2 + \text{H}_2 = 1/5\text{Ca}_2\text{HN} + 3/5\text{NH}_3$	-30.12	-	-	-
Ca-R098	$16/39\text{CaN}_2 + \text{H}_2 = 2/39\text{Ca}_8\text{H}_3\text{N}_4 + 8/13\text{NH}_3$	-30.3	-	-	-
Ca-R099	$1/2\text{CaN}_2 + \text{H}_2 = 1/2\text{CaHN} + 1/2\text{NH}_3$	-19.09	-	-	-
Ca-R100	$11/21\text{CaN}_2 + \text{H}_2 = 1/21\text{Ca}_{11}\text{N}_8 + 2/3\text{NH}_3$	-26.18	-	-	-
Ca-R101	$4/9\text{CaN}_2 + \text{H}_2 = 2/9\text{Ca}_2\text{N} + 2/3\text{NH}_3$	-30.86	-6.1	271.8	exergonic
Ca-R102	$1/2\text{CaN}_2 + \text{H}_2 = 1/6\text{Ca}_3\text{N}_2 + 2/3\text{NH}_3$	-27.43	-9.92	250.3	exergonic
Ca-R103	$2/3\text{CaN}_2 + \text{H}_2 = 2/3\text{CaN} + 2/3\text{NH}_3$	-20.57	-	-	-
Ca-R104	$\text{CaN}_6 + \text{H}_2 = \text{CaH}_2 + 3\text{N}_2$	-66.09	-19.39	-	exergonic
Ca-R105	$2/3\text{CaN}_6 + \text{H}_2 = 2/3\text{CaH}_3 + 2\text{N}_2$	-65.27	-	-	-
Ca-R106	$1/2\text{CaN}_6 + \text{H}_2 = 1/2\text{Ca}(\text{H}_2\text{N})_2 + \text{N}_2$	-41.89	-	-	-
Ca-R107	$32\text{CaN}_6 + \text{H}_2 = 2\text{Ca}_{16}\text{HN}_8 + 88\text{N}_2$	-62.02	-	-	-
Ca-R108	$4\text{CaN}_6 + \text{H}_2 = 2\text{Ca}_2\text{HN} + 11\text{N}_2$	-61.66	-	-	-
Ca-R109	$16/3\text{CaN}_6 + \text{H}_2 = 2/3\text{Ca}_8\text{H}_3\text{N}_4 + 44/3\text{N}_2$	-61.76	-	-	-
Ca-R110	$2\text{CaN}_6 + \text{H}_2 = 2\text{CaHN} + 5\text{N}_2$	-55.61	-	-	-
Ca-R111	$1/9\text{CaN}_6 + \text{H}_2 = 1/9\text{Ca} + 2/3\text{NH}_3$	-67.71	-13.09	367.6	exergonic
Ca-R112	$1/10\text{CaN}_6 + \text{H}_2 = 1/10\text{CaH}_2 + 3/5\text{NH}_3$	-66.09	-29.48	583.8	exergonic
Ca-R113	$2/21\text{CaN}_6 + \text{H}_2 = 2/21\text{CaH}_3 + 4/7\text{NH}_3$	-65.27	-	-	-
Ca-R114	$1/8\text{CaN}_6 + \text{H}_2 = 1/8\text{Ca}(\text{H}_2\text{N})_2 + 1/2\text{NH}_3$	-41.89	-	-	-
Ca-R115	$32/265\text{CaN}_6 + \text{H}_2 = 2/265\text{Ca}_{16}\text{HN}_8 + 176/265\text{NH}_3$	-62.02	-	-	-
Ca-R116	$2/17\text{CaN}_6 + \text{H}_2 = 1/17\text{Ca}_2\text{HN} + 11/17\text{NH}_3$	-61.66	-	-	-
Ca-R117	$16/135\text{CaN}_6 + \text{H}_2 = 2/135\text{Ca}_8\text{H}_3\text{N}_4 + 88/135\text{NH}_3$	-61.76	-	-	-
Ca-R118	$1/8\text{CaN}_6 + \text{H}_2 = 1/8\text{CaHN} + 5/8\text{NH}_3$	-55.61	-	-	-
Ca-R119	$11/87\text{CaN}_6 + \text{H}_2 = 1/87\text{Ca}_{11}\text{N}_8 + 2/3\text{NH}_3$	-59.5	-	-	-
Ca-R120	$4/33\text{CaN}_6 + \text{H}_2 = 2/33\text{Ca}_2\text{N} + 2/3\text{NH}_3$	-62.07	-27.24	783	exergonic
Ca-R121	$1/8\text{CaN}_6 + \text{H}_2 = 1/24\text{Ca}_3\text{N}_2 + 2/3\text{NH}_3$	-60.19	-28.86	767.3	exergonic
Ca-R122	$2/15\text{CaN}_6 + \text{H}_2 = 2/15\text{CaN} + 2/3\text{NH}_3$	-56.43	-	-	-
Ca-R123	$1/6\text{CaN}_6 + \text{H}_2 = 1/6\text{CaN}_2 + 2/3\text{NH}_3$	-45.14	-35.17	-	exergonic
Ca-R124	$11/4\text{Ca} + \text{N}_2 = 1/4\text{Ca}_{11}\text{N}_8$	25.42	-	-	-
Ca-R125	$4\text{Ca} + \text{N}_2 = 2\text{Ca}_2\text{N}$	17.47	-519.68	-	exergonic
Ca-R126	$3\text{Ca} + \text{N}_2 = \text{Ca}_3\text{N}_2$	23.3	-431	-	exergonic
Ca-R127	$2\text{Ca} + \text{N}_2 = 2\text{CaN}$	34.95	-	-	-
Ca-R128	$\text{Ca} + \text{N}_2 = \text{CaN}_2$	69.9	-185.03	-	exergonic
Ca-R129	$1/3\text{Ca} + \text{N}_2 = 1/3\text{CaN}_6$	209.7	-52.53	78.6	exergonic
Ca-R130	$1/2\text{Ca}(\text{H}_2\text{N})_2 + \text{N}_2 = 1/2\text{CaN}_6 + \text{H}_2$	72.09	-	-	-
Ca-R131	$33\text{Ca}(\text{H}_2\text{N})_2 + \text{N}_2 = 3\text{Ca}_{11}\text{N}_8 + 44\text{NH}_3$	-30.31	-	-	-

Ca-R132	$6\text{Ca}(\text{H}_2\text{N})_2 + \text{N}_2 = 6\text{CaN} + 8\text{NH}_3$	-25.01	-	-	-
Ca-R133	$3/2\text{Ca}(\text{H}_2\text{N})_2 + \text{N}_2 = 3/2\text{CaN}_2 + 2\text{NH}_3$	-5.59	-	-	-
Ca-R134	$3/8\text{Ca}(\text{H}_2\text{N})_2 + \text{N}_2 = 3/8\text{CaN}_6 + 1/2\text{NH}_3$	72.09	-	-	-
Ca-R135	$2/3\text{Ca}_11\text{N}_8 + \text{N}_2 = 22/3\text{CaN}$	7.6	-	-	-
Ca-R136	$1/7\text{Ca}_11\text{N}_8 + \text{N}_2 = 11/7\text{CaN}_2$	35.47	-	-	-
Ca-R137	$1/29\text{Ca}_11\text{N}_8 + \text{N}_2 = 11/29\text{CaN}_6$	146.93	-	-	-
Ca-R138	$11/20\text{Ca}_16\text{HN}_8 + \text{N}_2 = 4/5\text{Ca}_11\text{N}_8 + 11/40\text{H}_2$	6.62	-	-	-
Ca-R139	$3/4\text{Ca}_16\text{HN}_8 + \text{N}_2 = 4\text{Ca}_3\text{N}_2 + 3/8\text{H}_2$	4.82	-	-	-
Ca-R140	$1/4\text{Ca}_16\text{HN}_8 + \text{N}_2 = 4\text{CaN} + 1/8\text{H}_2$	14.72	-	-	-
Ca-R141	$1/12\text{Ca}_16\text{HN}_8 + \text{N}_2 = 4/3\text{CaN}_2 + 1/24\text{H}_2$	44.43	-	-	-
Ca-R142	$1/44\text{Ca}_16\text{HN}_8 + \text{N}_2 = 4/11\text{CaN}_6 + 1/88\text{H}_2$	163.28	-	-	-
Ca-R143	$66/131\text{Ca}_16\text{HN}_8 + \text{N}_2 = 96/131\text{Ca}_11\text{N}_8 + 22/131\text{NH}_3$	6.62	-	-	-
Ca-R144	$6\text{Ca}_16\text{HN}_8 + \text{N}_2 = 48\text{Ca}_2\text{N} + 2\text{NH}_3$	-0.13	-	-	-
Ca-R145	$2/3\text{Ca}_16\text{HN}_8 + \text{N}_2 = 32/9\text{Ca}_3\text{N}_2 + 2/9\text{NH}_3$	4.82	-	-	-
Ca-R146	$6/25\text{Ca}_16\text{HN}_8 + \text{N}_2 = 96/25\text{CaN} + 2/25\text{NH}_3$	14.72	-	-	-
Ca-R147	$6/73\text{Ca}_16\text{HN}_8 + \text{N}_2 = 96/73\text{CaN}_2 + 2/73\text{NH}_3$	44.43	-	-	-
Ca-R148	$6/265\text{Ca}_16\text{HN}_8 + \text{N}_2 = 96/265\text{CaN}_6 + 2/265\text{NH}_3$	163.28	-	-	-
Ca-R149	$22/5\text{Ca}_2\text{HN} + \text{N}_2 = 4/5\text{Ca}_11\text{N}_8 + 11/5\text{H}_2$	5.63	-	-	-
Ca-R150	$6\text{Ca}_2\text{HN} + \text{N}_2 = 4\text{Ca}_3\text{N}_2 + 3\text{H}_2$	3.85	-	-	-
Ca-R151	$2\text{Ca}_2\text{HN} + \text{N}_2 = 4\text{CaN} + \text{H}_2$	13.66	-	-	-
Ca-R152	$2/3\text{Ca}_2\text{HN} + \text{N}_2 = 4/3\text{CaN}_2 + 1/3\text{H}_2$	43.09	-	-	-
Ca-R153	$2/11\text{Ca}_2\text{HN} + \text{N}_2 = 4/11\text{CaN}_6 + 1/11\text{H}_2$	160.84	-	-	-
Ca-R154	$48/7\text{Ca}_2\text{HN} + \text{N}_2 = 6/7\text{Ca}_16\text{HN}_8 + 2\text{NH}_3$	-0.93	-	-	-
Ca-R155	$24\text{Ca}_2\text{HN} + \text{N}_2 = 6\text{Ca}_8\text{H}_3\text{N}_4 + 2\text{NH}_3$	-0.26	-	-	-
Ca-R156	$33/13\text{Ca}_2\text{HN} + \text{N}_2 = 6/13\text{Ca}_11\text{N}_8 + 11/13\text{NH}_3$	5.63	-	-	-
Ca-R157	$6\text{Ca}_2\text{HN} + \text{N}_2 = 6\text{Ca}_2\text{N} + 2\text{NH}_3$	-1.06	-	-	-
Ca-R158	$3\text{Ca}_2\text{HN} + \text{N}_2 = 2\text{Ca}_3\text{N}_2 + \text{NH}_3$	3.85	-	-	-
Ca-R159	$3/2\text{Ca}_2\text{HN} + \text{N}_2 = 3\text{CaN} + 1/2\text{NH}_3$	13.66	-	-	-
Ca-R160	$3/5\text{Ca}_2\text{HN} + \text{N}_2 = 6/5\text{CaN}_2 + 1/5\text{NH}_3$	43.09	-	-	-
Ca-R161	$3/17\text{Ca}_2\text{HN} + \text{N}_2 = 6/17\text{CaN}_6 + 1/17\text{NH}_3$	160.84	-	-	-
Ca-R162	$22/5\text{Ca}_2\text{N} + \text{N}_2 = 4/5\text{Ca}_11\text{N}_8$	6.76	-	-	-
Ca-R163	$6\text{Ca}_2\text{N} + \text{N}_2 = 4\text{Ca}_3\text{N}_2$	4.96	-164.95	177.7	exergonic
Ca-R164	$2\text{Ca}_2\text{N} + \text{N}_2 = 4\text{CaN}$	14.88	-	-	-
Ca-R165	$2/3\text{Ca}_2\text{N} + \text{N}_2 = 4/3\text{CaN}_2$	44.63	-73.48	154.4	exergonic
Ca-R166	$2/11\text{Ca}_2\text{N} + \text{N}_2 = 4/11\text{CaN}_6$	163.63	-10.06	-	endergonic
Ca-R167	$11\text{Ca}_3\text{N}_2 + \text{N}_2 = 3\text{Ca}_11\text{N}_8$	1.72	-	-	-
Ca-R168	$2\text{Ca}_3\text{N}_2 + \text{N}_2 = 6\text{CaN}$	9.45	-	-	-
Ca-R169	$1/2\text{Ca}_3\text{N}_2 + \text{N}_2 = 3/2\text{CaN}_2$	37.79	-62.05	147.1	exergonic
Ca-R170	$1/8\text{Ca}_3\text{N}_2 + \text{N}_2 = 3/8\text{CaN}_6$	151.17	-5.22	-	endergonic
Ca-R171	$11/10\text{Ca}_8\text{H}_3\text{N}_4 + \text{N}_2 = 4/5\text{Ca}_11\text{N}_8 + 33/20\text{H}_2$	5.91	-	-	-
Ca-R172	$3/2\text{Ca}_8\text{H}_3\text{N}_4 + \text{N}_2 = 4\text{Ca}_3\text{N}_2 + 9/4\text{H}_2$	4.12	-	-	-
Ca-R173	$1/2\text{Ca}_8\text{H}_3\text{N}_4 + \text{N}_2 = 4\text{CaN} + 3/4\text{H}_2$	13.96	-	-	-
Ca-R174	$1/6\text{Ca}_8\text{H}_3\text{N}_4 + \text{N}_2 = 4/3\text{CaN}_2 + 1/4\text{H}_2$	43.47	-	-	-
Ca-R175	$1/22\text{Ca}_8\text{H}_3\text{N}_4 + \text{N}_2 = 4/11\text{CaN}_6 + 3/44\text{H}_2$	161.53	-	-	-
Ca-R176	$12/5\text{Ca}_8\text{H}_3\text{N}_4 + \text{N}_2 = 6/5\text{Ca}_16\text{HN}_8 + 2\text{NH}_3$	-0.66	-	-	-
Ca-R177	$22/31\text{Ca}_8\text{H}_3\text{N}_4 + \text{N}_2 = 16/31\text{Ca}_11\text{N}_8 + 22/31\text{NH}_3$	5.91	-	-	-
Ca-R178	$2\text{Ca}_8\text{H}_3\text{N}_4 + \text{N}_2 = 8\text{Ca}_2\text{N} + 2\text{NH}_3$	-0.8	-	-	-
Ca-R179	$6/7\text{Ca}_8\text{H}_3\text{N}_4 + \text{N}_2 = 16/7\text{Ca}_3\text{N}_2 + 6/7\text{NH}_3$	4.12	-	-	-
Ca-R180	$2/5\text{Ca}_8\text{H}_3\text{N}_4 + \text{N}_2 = 16/5\text{CaN} + 2/5\text{NH}_3$	13.96	-	-	-

Ca-R181	$2/13\text{Ca}_8\text{H}_3\text{N}_4 + \text{N}_2 = 16/13\text{CaN}_2 + 2/13\text{NH}_3$	43.47	-	-	-
Ca-R182	$2/45\text{Ca}_8\text{H}_3\text{N}_4 + \text{N}_2 = 16/45\text{CaN}_6 + 2/45\text{NH}_3$	161.53	-	-	-
Ca-R183	$4\text{CaH}_2 + \text{N}_2 = 1/4\text{Ca}_{16}\text{HN}_8 + 31/8\text{H}_2$	12	-	-	-
Ca-R184	$4\text{CaH}_2 + \text{N}_2 = 2\text{Ca}_2\text{HN} + 3\text{H}_2$	13.05	-	-	-
Ca-R185	$4\text{CaH}_2 + \text{N}_2 = 1/2\text{Ca}_8\text{H}_3\text{N}_4 + 13/4\text{H}_2$	12.75	-	-	-
Ca-R186	$2\text{CaH}_2 + \text{N}_2 = 2\text{CaHN} + \text{H}_2$	30.88	-	-	-
Ca-R187	$11/4\text{CaH}_2 + \text{N}_2 = 1/4\text{Ca}_{11}\text{N}_8 + 11/4\text{H}_2$	19.41	-	-	-
Ca-R188	$4\text{CaH}_2 + \text{N}_2 = 2\text{Ca}_2\text{N} + 4\text{H}_2$	11.85	188.24	235.2	exergonic
Ca-R189	$3\text{CaH}_2 + \text{N}_2 = \text{Ca}_3\text{N}_2 + 3\text{H}_2$	17.39	99.94	259.7	exergonic
Ca-R190	$2\text{CaH}_2 + \text{N}_2 = 2\text{CaN} + 2\text{H}_2$	28.49	-	-	-
Ca-R191	$\text{CaH}_2 + \text{N}_2 = \text{CaN}_2 + \text{H}_2$	61.76	-8.05	-	endergonic
Ca-R192	$1/3\text{CaH}_2 + \text{N}_2 = 1/3\text{CaN}_6 + 1/3\text{H}_2$	194.86	6.46	-	endergonic
Ca-R193	$3\text{CaH}_2 + \text{N}_2 = 3\text{Ca} + 2\text{NH}_3$	-4.79	439.15	-	endergonic
Ca-R194	$96/55\text{CaH}_2 + \text{N}_2 = 6/55\text{Ca}_{16}\text{HN}_8 + 62/55\text{NH}_3$	12	-	-	-
Ca-R195	$2\text{CaH}_2 + \text{N}_2 = \text{Ca}_2\text{HN} + \text{NH}_3$	13.05	-	-	-
Ca-R196	$48/25\text{CaH}_2 + \text{N}_2 = 6/25\text{Ca}_8\text{H}_3\text{N}_4 + 26/25\text{NH}_3$	12.75	-	-	-
Ca-R197	$3/2\text{CaH}_2 + \text{N}_2 = 3/2\text{CaHN} + 1/2\text{NH}_3$	30.88	-	-	-
Ca-R198	$33/23\text{CaH}_2 + \text{N}_2 = 3/23\text{Ca}_{11}\text{N}_8 + 22/23\text{NH}_3$	19.41	-	-	-
Ca-R199	$12/7\text{CaH}_2 + \text{N}_2 = 6/7\text{Ca}_2\text{N} + 8/7\text{NH}_3$	11.85	28.22	389.3	exergonic
Ca-R200	$3/2\text{CaH}_2 + \text{N}_2 = 1/2\text{Ca}_3\text{N}_2 + \text{NH}_3$	17.39	4.08	-	endergonic
Ca-R201	$6/5\text{CaH}_2 + \text{N}_2 = 6/5\text{CaN} + 4/5\text{NH}_3$	28.49	-	-	-
Ca-R202	$3/4\text{CaH}_2 + \text{N}_2 = 3/4\text{CaN}_2 + 1/2\text{NH}_3$	61.76	-28.99	97.1	exergonic
Ca-R203	$3/10\text{CaH}_2 + \text{N}_2 = 3/10\text{CaN}_6 + 1/5\text{NH}_3$	194.86	-3.36	-	endergonic
Ca-R204	$4\text{CaH}_3 + \text{N}_2 = 1/4\text{Ca}_{16}\text{HN}_8 + 47/8\text{H}_2$	9.38	-	-	-
Ca-R205	$4\text{CaH}_3 + \text{N}_2 = 2\text{Ca}_2\text{HN} + 5\text{H}_2$	10.4	-	-	-
Ca-R206	$4\text{CaH}_3 + \text{N}_2 = 1/2\text{Ca}_8\text{H}_3\text{N}_4 + 21/4\text{H}_2$	10.11	-	-	-
Ca-R207	$2\text{CaH}_3 + \text{N}_2 = 2\text{CaHN} + 2\text{H}_2$	27.82	-	-	-
Ca-R208	$11/4\text{CaH}_3 + \text{N}_2 = 1/4\text{Ca}_{11}\text{N}_8 + 33/8\text{H}_2$	16.62	-	-	-
Ca-R209	$4\text{CaH}_3 + \text{N}_2 = 2\text{Ca}_2\text{N} + 6\text{H}_2$	9.23	-	-	-
Ca-R210	$3\text{CaH}_3 + \text{N}_2 = \text{Ca}_3\text{N}_2 + 9/2\text{H}_2$	14.65	-	-	-
Ca-R211	$2\text{CaH}_3 + \text{N}_2 = 2\text{CaN} + 3\text{H}_2$	25.48	-	-	-
Ca-R212	$\text{CaH}_3 + \text{N}_2 = \text{CaN}_2 + 3/2\text{H}_2$	57.98	-	-	-
Ca-R213	$1/3\text{CaH}_3 + \text{N}_2 = 1/3\text{CaN}_6 + 1/2\text{H}_2$	187.97	-	-	-
Ca-R214	$2\text{CaH}_3 + \text{N}_2 = 2\text{Ca} + 2\text{NH}_3$	-7.02	-	-	-
Ca-R215	$6\text{CaH}_3 + \text{N}_2 = 6\text{CaH}_2 + 2\text{NH}_3$	-2.34	-	-	-
Ca-R216	$96/71\text{CaH}_3 + \text{N}_2 = 6/71\text{Ca}_{16}\text{HN}_8 + 94/71\text{NH}_3$	9.38	-	-	-
Ca-R217	$3/2\text{CaH}_3 + \text{N}_2 = 3/4\text{Ca}_2\text{HN} + 5/4\text{NH}_3$	10.4	-	-	-
Ca-R218	$16/11\text{CaH}_3 + \text{N}_2 = 2/11\text{Ca}_8\text{H}_3\text{N}_4 + 14/11\text{NH}_3$	10.11	-	-	-
Ca-R219	$6/5\text{CaH}_3 + \text{N}_2 = 6/5\text{CaHN} + 4/5\text{NH}_3$	27.82	-	-	-
Ca-R220	$22/19\text{CaH}_3 + \text{N}_2 = 2/19\text{Ca}_{11}\text{N}_8 + 22/19\text{NH}_3$	16.62	-	-	-
Ca-R221	$4/3\text{CaH}_3 + \text{N}_2 = 2/3\text{Ca}_2\text{N} + 4/3\text{NH}_3$	9.23	-	-	-
Ca-R222	$6/5\text{CaH}_3 + \text{N}_2 = 2/5\text{Ca}_3\text{N}_2 + 6/5\text{NH}_3$	14.65	-	-	-
Ca-R223	$\text{CaH}_3 + \text{N}_2 = \text{CaN} + \text{NH}_3$	25.48	-	-	-
Ca-R224	$2/3\text{CaH}_3 + \text{N}_2 = 2/3\text{CaN}_2 + 2/3\text{NH}_3$	57.98	-	-	-
Ca-R225	$2/7\text{CaH}_3 + \text{N}_2 = 2/7\text{CaN}_6 + 2/7\text{NH}_3$	187.97	-	-	-
Ca-R226	$2\text{CaHN} + \text{N}_2 = 2\text{CaN}_2 + \text{H}_2$	23.59	-	-	-
Ca-R227	$2/5\text{CaHN} + \text{N}_2 = 2/5\text{CaN}_6 + 1/5\text{H}_2$	125.29	-	-	-
Ca-R228	$33\text{CaHN} + \text{N}_2 = 3\text{Ca}_{11}\text{N}_8 + 11\text{NH}_3$	-8.76	-	-	-
Ca-R229	$6\text{CaHN} + \text{N}_2 = 6\text{CaN} + 2\text{NH}_3$	-1.83	-	-	-



Ca-R230	$3/2\text{CaHN} + \text{N}_2 = 3/2\text{CaN}_2 + 1/2\text{NH}_3$	23.59	-	-	-
Ca-R231	$3/8\text{CaHN} + \text{N}_2 = 3/8\text{CaN}_6 + 1/8\text{NH}_3$	125.29	-	-	-
Ca-R232	$2\text{CaN} + \text{N}_2 = 2\text{CaN}_2$	25.9	-	-	-
Ca-R233	$2/5\text{CaN} + \text{N}_2 = 2/5\text{CaN}_6$	129.49	-	-	-
Ca-R234	$1/2\text{CaN}_2 + \text{N}_2 = 1/2\text{CaN}_6$	82.28	13.72	-	endergonic

Table S16: The Co-based system

ID	Reaction	dm_stoich [%]	h298 [kJ/mol]	T_eq [°C]	Type
Co-R001	$6\text{Co} + \text{H}_2 = 2\text{Co}_3\text{H}$	0.57	-16.75	-	endergonic
Co-R002	$8\text{Co} + \text{H}_2 = 2\text{Co}_4\text{H}$	0.43	-	-	-
Co-R003	$2\text{Co} + \text{H}_2 = 2\text{CoH}$	1.71	-	-	-
Co-R004	$2/3\text{Co} + \text{H}_2 = 2/3\text{CoH}_3$	5.13	-	-	-
Co-R005	$3\text{Co}_2\text{N} + \text{H}_2 = 2\text{Co}_3\text{H} + 3/2\text{N}_2$	-10.11	-171.23	-	exergonic
Co-R006	$4\text{Co}_2\text{N} + \text{H}_2 = 2\text{Co}_4\text{H} + 2\text{N}_2$	-10.24	-	-	-
Co-R007	$\text{Co}_2\text{N} + \text{H}_2 = 2\text{CoH} + 1/2\text{N}_2$	-9.09	-	-	-
Co-R008	$1/3\text{Co}_2\text{N} + \text{H}_2 = 2/3\text{CoH}_3 + 1/6\text{N}_2$	-6.04	-	-	-
Co-R009	$2/3\text{Co}_2\text{N} + \text{H}_2 = 4/3\text{Co} + 2/3\text{NH}_3$	-10.62	-64.93	-	exergonic
Co-R010	$6/11\text{Co}_2\text{N} + \text{H}_2 = 4/11\text{Co}_3\text{H} + 6/11\text{NH}_3$	-10.11	-56.17	-	exergonic
Co-R011	$4/7\text{Co}_2\text{N} + \text{H}_2 = 2/7\text{Co}_4\text{H} + 4/7\text{NH}_3$	-10.24	-	-	-
Co-R012	$2/5\text{Co}_2\text{N} + \text{H}_2 = 4/5\text{CoH} + 2/5\text{NH}_3$	-9.09	-	-	-
Co-R013	$2/9\text{Co}_2\text{N} + \text{H}_2 = 4/9\text{CoH}_3 + 2/9\text{NH}_3$	-6.04	-	-	-
Co-R014	$2\text{Co}_2\text{N} + \text{H}_2 = 4/3\text{Co}_3\text{N} + 2/3\text{NH}_3$	-3.54	-122.43	-	exergonic
Co-R015	$4/3\text{Co}_2\text{N} + \text{H}_2 = 2/3\text{Co}_4\text{N} + 2/3\text{NH}_3$	-5.31	-	-	-
Co-R016	$\text{Co}_3\text{H} + \text{H}_2 = 3\text{CoH}$	1.13	-	-	-
Co-R017	$1/4\text{Co}_3\text{H} + \text{H}_2 = 3/4\text{CoH}_3$	4.54	-	-	-
Co-R018	$2\text{Co}_3\text{N} + \text{H}_2 = 2\text{Co}_3\text{H} + \text{N}_2$	-6.81	-33.49	-	exergonic
Co-R019	$8/3\text{Co}_3\text{N} + \text{H}_2 = 2\text{Co}_4\text{H} + 4/3\text{N}_2$	-6.94	-	-	-
Co-R020	$2/3\text{Co}_3\text{N} + \text{H}_2 = 2\text{CoH} + 1/3\text{N}_2$	-5.76	-	-	-
Co-R021	$2/9\text{Co}_3\text{N} + \text{H}_2 = 2/3\text{CoH}_3 + 1/9\text{N}_2$	-2.59	-	-	-
Co-R022	$2/3\text{Co}_3\text{N} + \text{H}_2 = 2\text{Co} + 2/3\text{NH}_3$	-7.34	-36.18	-	exergonic
Co-R023	$1/2\text{Co}_3\text{N} + \text{H}_2 = 1/2\text{Co}_3\text{H} + 1/2\text{NH}_3$	-6.81	-31.32	352.1	exergonic
Co-R024	$8/15\text{Co}_3\text{N} + \text{H}_2 = 2/5\text{Co}_4\text{H} + 8/15\text{NH}_3$	-6.94	-	-	-
Co-R025	$1/3\text{Co}_3\text{N} + \text{H}_2 = \text{CoH} + 1/3\text{NH}_3$	-5.76	-	-	-
Co-R026	$1/6\text{Co}_3\text{N} + \text{H}_2 = 1/2\text{CoH}_3 + 1/6\text{NH}_3$	-2.59	-	-	-
Co-R027	$8/3\text{Co}_3\text{N} + \text{H}_2 = 2\text{Co}_4\text{N} + 2/3\text{NH}_3$	-1.84	-	-	-
Co-R028	$6\text{Co}_4\text{H} + \text{H}_2 = 8\text{Co}_3\text{H}$	0.14	-	-	-
Co-R029	$2/3\text{Co}_4\text{H} + \text{H}_2 = 8/3\text{CoH}$	1.28	-	-	-
Co-R030	$2/11\text{Co}_4\text{H} + \text{H}_2 = 8/11\text{CoH}_3$	4.68	-	-	-
Co-R031	$3/2\text{Co}_4\text{N} + \text{H}_2 = 2\text{Co}_3\text{H} + 3/4\text{N}_2$	-5.07	-	-	-
Co-R032	$2\text{Co}_4\text{N} + \text{H}_2 = 2\text{Co}_4\text{H} + \text{N}_2$	-5.21	-	-	-
Co-R033	$1/2\text{Co}_4\text{N} + \text{H}_2 = 2\text{CoH} + 1/4\text{N}_2$	-3.99	-	-	-
Co-R034	$1/6\text{Co}_4\text{N} + \text{H}_2 = 2/3\text{CoH}_3 + 1/12\text{N}_2$	-0.77	-	-	-
Co-R035	$2/3\text{Co}_4\text{N} + \text{H}_2 = 8/3\text{Co} + 2/3\text{NH}_3$	-5.61	-	-	-
Co-R036	$6/13\text{Co}_4\text{N} + \text{H}_2 = 8/13\text{Co}_3\text{H} + 6/13\text{NH}_3$	-5.07	-	-	-
Co-R037	$1/2\text{Co}_4\text{N} + \text{H}_2 = 1/2\text{Co}_4\text{H} + 1/2\text{NH}_3$	-5.21	-	-	-
Co-R038	$2/7\text{Co}_4\text{N} + \text{H}_2 = 8/7\text{CoH} + 2/7\text{NH}_3$	-3.99	-	-	-
Co-R039	$2/15\text{Co}_4\text{N} + \text{H}_2 = 8/15\text{CoH}_3 + 2/15\text{NH}_3$	-0.77	-	-	-
Co-R040	$\text{CoH} + \text{H}_2 = \text{CoH}_3$	3.36	-	-	-

Co-R041	$6\text{CoN} + \text{H}_2 = 2\text{Co}_3\text{H} + 3\text{N}_2$	-18.74	-135.88	-	exergonic
Co-R042	$8\text{CoN} + \text{H}_2 = 2\text{Co}_4\text{H} + 4\text{N}_2$	-18.86	-	-	-
Co-R043	$2\text{CoN} + \text{H}_2 = 2\text{CoH} + \text{N}_2$	-17.82	-	-	-
Co-R044	$2/3\text{CoN} + \text{H}_2 = 2/3\text{CoH}_3 + 1/3\text{N}_2$	-15.06	-	-	-
Co-R045	$2/3\text{CoN} + \text{H}_2 = 2/3\text{Co} + 2/3\text{NH}_3$	-19.2	-43.83	-	exergonic
Co-R046	$3/5\text{CoN} + \text{H}_2 = 1/5\text{Co}_3\text{H} + 3/5\text{NH}_3$	-18.74	-41.13	798.6	exergonic
Co-R047	$8/13\text{CoN} + \text{H}_2 = 2/13\text{Co}_4\text{H} + 8/13\text{NH}_3$	-18.86	-	-	-
Co-R048	$1/2\text{CoN} + \text{H}_2 = 1/2\text{CoH} + 1/2\text{NH}_3$	-17.82	-	-	-
Co-R049	$1/3\text{CoN} + \text{H}_2 = 1/3\text{CoH}_3 + 1/3\text{NH}_3$	-15.06	-	-	-
Co-R050	$4/3\text{CoN} + \text{H}_2 = 2/3\text{Co}_2\text{N} + 2/3\text{NH}_3$	-9.6	-22.74	422.8	exergonic
Co-R051	$\text{CoN} + \text{H}_2 = 1/3\text{Co}_3\text{N} + 2/3\text{NH}_3$	-12.8	-47.66	-	exergonic
Co-R052	$8/9\text{CoN} + \text{H}_2 = 2/9\text{Co}_4\text{N} + 2/3\text{NH}_3$	-14.4	-	-	-
Co-R053	$6\text{CoN}_{12} + \text{H}_2 = 2\text{Co}_3\text{H} + 36\text{N}_2$	-73.89	-	-	-
Co-R054	$8\text{CoN}_{12} + \text{H}_2 = 2\text{Co}_4\text{H} + 48\text{N}_2$	-73.93	-	-	-
Co-R055	$2\text{CoN}_{12} + \text{H}_2 = 2\text{CoH} + 12\text{N}_2$	-73.6	-	-	-
Co-R056	$2/3\text{CoN}_{12} + \text{H}_2 = 2/3\text{CoH}_3 + 4\text{N}_2$	-72.71	-	-	-
Co-R057	$1/18\text{CoN}_{12} + \text{H}_2 = 1/18\text{Co} + 2/3\text{NH}_3$	-74.04	-	-	-
Co-R058	$6/109\text{CoN}_{12} + \text{H}_2 = 2/109\text{Co}_3\text{H} + 72/109\text{NH}_3$	-73.89	-	-	-
Co-R059	$8/145\text{CoN}_{12} + \text{H}_2 = 2/145\text{Co}_4\text{H} + 96/145\text{NH}_3$	-73.93	-	-	-
Co-R060	$2/37\text{CoN}_{12} + \text{H}_2 = 2/37\text{CoH} + 24/37\text{NH}_3$	-73.6	-	-	-
Co-R061	$2/39\text{CoN}_{12} + \text{H}_2 = 2/39\text{CoH}_3 + 8/13\text{NH}_3$	-72.71	-	-	-
Co-R062	$4/69\text{CoN}_{12} + \text{H}_2 = 2/69\text{Co}_2\text{N} + 2/3\text{NH}_3$	-70.96	-	-	-
Co-R063	$2/35\text{CoN}_{12} + \text{H}_2 = 2/105\text{Co}_3\text{N} + 2/3\text{NH}_3$	-71.98	-	-	-
Co-R064	$8/141\text{CoN}_{12} + \text{H}_2 = 2/141\text{Co}_4\text{N} + 2/3\text{NH}_3$	-72.5	-	-	-
Co-R065	$2/33\text{CoN}_{12} + \text{H}_2 = 2/33\text{CoN} + 2/3\text{NH}_3$	-67.87	-	-	-
Co-R066	$2/27\text{CoN}_{12} + \text{H}_2 = 2/27\text{CoN}_3 + 2/3\text{NH}_3$	-55.53	-	-	-
Co-R067	$6\text{CoN}_3 + \text{H}_2 = 2\text{Co}_3\text{H} + 9\text{N}_2$	-41.29	-	-	-
Co-R068	$8\text{CoN}_3 + \text{H}_2 = 2\text{Co}_4\text{H} + 12\text{N}_2$	-41.37	-	-	-
Co-R069	$2\text{CoN}_3 + \text{H}_2 = 2\text{CoH} + 3\text{N}_2$	-40.63	-	-	-
Co-R070	$2/3\text{CoN}_3 + \text{H}_2 = 2/3\text{CoH}_3 + \text{N}_2$	-38.63	-	-	-
Co-R071	$2/9\text{CoN}_3 + \text{H}_2 = 2/9\text{Co} + 2/3\text{NH}_3$	-41.62	-	-	-
Co-R072	$3/14\text{CoN}_3 + \text{H}_2 = 1/14\text{Co}_3\text{H} + 9/14\text{NH}_3$	-41.29	-	-	-
Co-R073	$8/37\text{CoN}_3 + \text{H}_2 = 2/37\text{Co}_4\text{H} + 24/37\text{NH}_3$	-41.37	-	-	-
Co-R074	$1/5\text{CoN}_3 + \text{H}_2 = 1/5\text{CoH} + 3/5\text{NH}_3$	-40.63	-	-	-
Co-R075	$1/6\text{CoN}_3 + \text{H}_2 = 1/6\text{CoH}_3 + 1/2\text{NH}_3$	-38.63	-	-	-
Co-R076	$4/15\text{CoN}_3 + \text{H}_2 = 2/15\text{Co}_2\text{N} + 2/3\text{NH}_3$	-34.69	-	-	-
Co-R077	$1/4\text{CoN}_3 + \text{H}_2 = 1/12\text{Co}_3\text{N} + 2/3\text{NH}_3$	-37	-	-	-
Co-R078	$8/33\text{CoN}_3 + \text{H}_2 = 2/33\text{Co}_4\text{N} + 2/3\text{NH}_3$	-38.16	-	-	-
Co-R079	$1/3\text{CoN}_3 + \text{H}_2 = 1/3\text{CoN} + 2/3\text{NH}_3$	-27.75	-	-	-
Co-R080	$4\text{Co} + \text{N}_2 = 2\text{Co}_2\text{N}$	11.88	102.99	-	endergonic
Co-R081	$6\text{Co} + \text{N}_2 = 2\text{Co}_3\text{N}$	7.92	16.74	-	endergonic
Co-R082	$8\text{Co} + \text{N}_2 = 2\text{Co}_4\text{N}$	5.94	-	-	-
Co-R083	$2\text{Co} + \text{N}_2 = 2\text{CoN}$	23.77	39.71	-	endergonic
Co-R084	$1/6\text{Co} + \text{N}_2 = 1/6\text{CoN}_{12}$	285.21	-	-	-
Co-R085	$2/3\text{Co} + \text{N}_2 = 2/3\text{CoN}_3$	71.3	-	-	-
Co-R086	$2\text{Co}_2\text{N} + \text{N}_2 = 4\text{CoN}$	10.62	-23.57	-	endergonic
Co-R087	$2/23\text{Co}_2\text{N} + \text{N}_2 = 4/23\text{CoN}_{12}$	244.3	-	-	-
Co-R088	$2/5\text{Co}_2\text{N} + \text{N}_2 = 4/5\text{CoN}_3$	53.11	-	-	-
Co-R089	$4/3\text{Co}_3\text{H} + \text{N}_2 = 2\text{Co}_2\text{N} + 2/3\text{H}_2$	11.25	114.16	-	endergonic

Co-R090	$2\text{Co}_3\text{H} + \text{N}_2 = 2\text{Co}_3\text{N} + \text{H}_2$	7.31	33.49	-	endergonic
Co-R091	$8/3\text{Co}_3\text{H} + \text{N}_2 = 2\text{Co}_4\text{N} + 4/3\text{H}_2$	5.34	-	-	-
Co-R092	$2/3\text{Co}_3\text{H} + \text{N}_2 = 2\text{CoN} + 1/3\text{H}_2$	23.07	45.29	-	endergonic
Co-R093	$1/18\text{Co}_3\text{H} + \text{N}_2 = 1/6\text{CoN}_{12} + 1/36\text{H}_2$	283.03	-	-	-
Co-R094	$2/9\text{Co}_3\text{H} + \text{N}_2 = 2/3\text{CoN}_3 + 1/9\text{H}_2$	70.33	-	-	-
Co-R095	$6\text{Co}_3\text{H} + \text{N}_2 = 18\text{Co} + 2\text{NH}_3$	-0.57	-41.54	-	exergonic
Co-R096	$24\text{Co}_3\text{H} + \text{N}_2 = 18\text{Co}_4\text{H} + 2\text{NH}_3$	-0.14	-	-	-
Co-R097	$12/11\text{Co}_3\text{H} + \text{N}_2 = 18/11\text{Co}_2\text{N} + 4/11\text{NH}_3$	11.25	76.71	-	endergonic
Co-R098	$3/2\text{Co}_3\text{H} + \text{N}_2 = 3/2\text{Co}_3\text{N} + 1/2\text{NH}_3$	7.31	2.17	-	endergonic
Co-R099	$24/13\text{Co}_3\text{H} + \text{N}_2 = 18/13\text{Co}_4\text{N} + 8/13\text{NH}_3$	5.34	-	-	-
Co-R100	$3/5\text{Co}_3\text{H} + \text{N}_2 = 9/5\text{CoN} + 1/5\text{NH}_3$	23.07	31.59	-	endergonic
Co-R101	$6/109\text{Co}_3\text{H} + \text{N}_2 = 18/109\text{CoN}_{12} + 2/109\text{NH}_3$	283.03	-	-	-
Co-R102	$3/14\text{Co}_3\text{H} + \text{N}_2 = 9/14\text{CoN}_3 + 1/14\text{NH}_3$	70.33	-	-	-
Co-R103	$4\text{Co}_3\text{N} + \text{N}_2 = 6\text{Co}_2\text{N}$	3.67	275.49	-	endergonic
Co-R104	$\text{Co}_3\text{N} + \text{N}_2 = 3\text{CoN}$	14.68	51.2	-	endergonic
Co-R105	$2/35\text{Co}_3\text{N} + \text{N}_2 = 6/35\text{CoN}_{12}$	256.93	-	-	-
Co-R106	$1/4\text{Co}_3\text{N} + \text{N}_2 = 3/4\text{CoN}_3$	58.73	-	-	-
Co-R107	$\text{Co}_4\text{H} + \text{N}_2 = 2\text{Co}_2\text{N} + 1/2\text{H}_2$	11.41	-	-	-
Co-R108	$3/2\text{Co}_4\text{H} + \text{N}_2 = 2\text{Co}_3\text{N} + 3/4\text{H}_2$	7.46	-	-	-
Co-R109	$2\text{Co}_4\text{H} + \text{N}_2 = 2\text{Co}_4\text{N} + \text{H}_2$	5.49	-	-	-
Co-R110	$1/2\text{Co}_4\text{H} + \text{N}_2 = 2\text{CoN} + 1/4\text{H}_2$	23.24	-	-	-
Co-R111	$1/24\text{Co}_4\text{H} + \text{N}_2 = 1/6\text{CoN}_{12} + 1/48\text{H}_2$	283.57	-	-	-
Co-R112	$1/6\text{Co}_4\text{H} + \text{N}_2 = 2/3\text{CoN}_3 + 1/12\text{H}_2$	70.57	-	-	-
Co-R113	$6\text{Co}_4\text{H} + \text{N}_2 = 24\text{Co} + 2\text{NH}_3$	-0.43	-	-	-
Co-R114	$6/7\text{Co}_4\text{H} + \text{N}_2 = 12/7\text{Co}_2\text{N} + 2/7\text{NH}_3$	11.41	-	-	-
Co-R115	$6/5\text{Co}_4\text{H} + \text{N}_2 = 8/5\text{Co}_3\text{N} + 2/5\text{NH}_3$	7.46	-	-	-
Co-R116	$3/2\text{Co}_4\text{H} + \text{N}_2 = 3/2\text{Co}_4\text{N} + 1/2\text{NH}_3$	5.49	-	-	-
Co-R117	$6/13\text{Co}_4\text{H} + \text{N}_2 = 24/13\text{CoN} + 2/13\text{NH}_3$	23.24	-	-	-
Co-R118	$6/145\text{Co}_4\text{H} + \text{N}_2 = 24/145\text{CoN}_{12} + 2/145\text{NH}_3$	283.57	-	-	-
Co-R119	$6/37\text{Co}_4\text{H} + \text{N}_2 = 24/37\text{CoN}_3 + 2/37\text{NH}_3$	70.57	-	-	-
Co-R120	$2\text{Co}_4\text{N} + \text{N}_2 = 4\text{Co}_2\text{N}$	5.61	-	-	-
Co-R121	$6\text{Co}_4\text{N} + \text{N}_2 = 8\text{Co}_3\text{N}$	1.87	-	-	-
Co-R122	$2/3\text{Co}_4\text{N} + \text{N}_2 = 8/3\text{CoN}$	16.83	-	-	-
Co-R123	$2/47\text{Co}_4\text{N} + \text{N}_2 = 8/47\text{CoN}_{12}$	263.61	-	-	-
Co-R124	$2/11\text{Co}_4\text{N} + \text{N}_2 = 8/11\text{CoN}_3$	61.7	-	-	-
Co-R125	$4\text{CoH} + \text{N}_2 = 2\text{Co}_2\text{N} + 2\text{H}_2$	10	-	-	-
Co-R126	$6\text{CoH} + \text{N}_2 = 2\text{Co}_3\text{N} + 3\text{H}_2$	6.11	-	-	-
Co-R127	$8\text{CoH} + \text{N}_2 = 2\text{Co}_4\text{N} + 4\text{H}_2$	4.16	-	-	-
Co-R128	$2\text{CoH} + \text{N}_2 = 2\text{CoN} + \text{H}_2$	21.69	-	-	-
Co-R129	$1/6\text{CoH} + \text{N}_2 = 1/6\text{CoN}_{12} + 1/12\text{H}_2$	278.73	-	-	-
Co-R130	$2/3\text{CoH} + \text{N}_2 = 2/3\text{CoN}_3 + 1/3\text{H}_2$	68.42	-	-	-
Co-R131	$6\text{CoH} + \text{N}_2 = 6\text{Co} + 2\text{NH}_3$	-1.68	-	-	-
Co-R132	$9\text{CoH} + \text{N}_2 = 3\text{Co}_3\text{H} + 2\text{NH}_3$	-1.12	-	-	-
Co-R133	$8\text{CoH} + \text{N}_2 = 2\text{Co}_4\text{H} + 2\text{NH}_3$	-1.26	-	-	-
Co-R134	$12/5\text{CoH} + \text{N}_2 = 6/5\text{Co}_2\text{N} + 4/5\text{NH}_3$	10	-	-	-
Co-R135	$3\text{CoH} + \text{N}_2 = \text{Co}_3\text{N} + \text{NH}_3$	6.11	-	-	-
Co-R136	$24/7\text{CoH} + \text{N}_2 = 6/7\text{Co}_4\text{N} + 8/7\text{NH}_3$	4.16	-	-	-
Co-R137	$3/2\text{CoH} + \text{N}_2 = 3/2\text{CoN} + 1/2\text{NH}_3$	21.69	-	-	-
Co-R138	$6/37\text{CoH} + \text{N}_2 = 6/37\text{CoN}_{12} + 2/37\text{NH}_3$	278.73	-	-	-

Co-R139	$3/5\text{CoH} + \text{N}_2 = 3/5\text{CoN}_3 + 1/5\text{NH}_3$	68.42	-	-	-
Co-R140	$4\text{CoH}_3 + \text{N}_2 = 2\text{Co}_2\text{N} + 6\text{H}_2$	6.42	-	-	-
Co-R141	$6\text{CoH}_3 + \text{N}_2 = 2\text{Co}_3\text{N} + 9\text{H}_2$	2.66	-	-	-
Co-R142	$8\text{CoH}_3 + \text{N}_2 = 2\text{Co}_4\text{N} + 12\text{H}_2$	0.77	-	-	-
Co-R143	$2\text{CoH}_3 + \text{N}_2 = 2\text{CoN} + 3\text{H}_2$	17.73	-	-	-
Co-R144	$1/6\text{CoH}_3 + \text{N}_2 = 1/6\text{CoN}_{12} + 1/4\text{H}_2$	266.41	-	-	-
Co-R145	$2/3\text{CoH}_3 + \text{N}_2 = 2/3\text{CoN}_3 + \text{H}_2$	62.94	-	-	-
Co-R146	$2\text{CoH}_3 + \text{N}_2 = 2\text{Co} + 2\text{NH}_3$	-4.88	-	-	-
Co-R147	$9/4\text{CoH}_3 + \text{N}_2 = 3/4\text{Co}_3\text{H} + 2\text{NH}_3$	-4.34	-	-	-
Co-R148	$24/11\text{CoH}_3 + \text{N}_2 = 6/11\text{Co}_4\text{H} + 2\text{NH}_3$	-4.47	-	-	-
Co-R149	$3\text{CoH}_3 + \text{N}_2 = 3\text{CoH} + 2\text{NH}_3$	-3.25	-	-	-
Co-R150	$4/3\text{CoH}_3 + \text{N}_2 = 2/3\text{Co}_2\text{N} + 4/3\text{NH}_3$	6.42	-	-	-
Co-R151	$3/2\text{CoH}_3 + \text{N}_2 = 1/2\text{Co}_3\text{N} + 3/2\text{NH}_3$	2.66	-	-	-
Co-R152	$8/5\text{CoH}_3 + \text{N}_2 = 2/5\text{Co}_4\text{N} + 8/5\text{NH}_3$	0.77	-	-	-
Co-R153	$\text{CoH}_3 + \text{N}_2 = \text{CoN} + \text{NH}_3$	17.73	-	-	-
Co-R154	$2/13\text{CoH}_3 + \text{N}_2 = 2/13\text{CoN}_{12} + 2/13\text{NH}_3$	266.41	-	-	-
Co-R155	$1/2\text{CoH}_3 + \text{N}_2 = 1/2\text{CoN}_3 + 1/2\text{NH}_3$	62.94	-	-	-
Co-R156	$2/11\text{CoN} + \text{N}_2 = 2/11\text{CoN}_{12}$	211.24	-	-	-
Co-R157	$\text{CoN} + \text{N}_2 = \text{CoN}_3$	38.41	-	-	-
Co-R158	$2/9\text{CoN}_3 + \text{N}_2 = 2/9\text{CoN}_{12}$	124.87	-	-	-

Table S17: The Cr-based system

ID	Reaction	dm_stoich [%]	h298 [kJ/mol]	T_eq [°C]	Type
Cr-R001	$6\text{Cr} + \text{H}_2 = 2\text{Cr}_3\text{H}$	0.65	-	-	-
Cr-R002	$2\text{Cr} + \text{H}_2 = 2\text{CrH}$	1.94	64.04	-	endergonic
Cr-R003	$\text{Cr} + \text{H}_2 = \text{CrH}_2$	3.88	-	-	-
Cr-R004	$2/3\text{Cr} + \text{H}_2 = 2/3\text{CrH}_3$	5.82	-	-	-
Cr-R005	$3\text{Cr}_2\text{N} + \text{H}_2 = 2\text{Cr}_3\text{H} + 3/2\text{N}_2$	-11.3	-	-	-
Cr-R006	$\text{Cr}_2\text{N} + \text{H}_2 = 2\text{CrH} + 1/2\text{N}_2$	-10.16	189.56	-	endergonic
Cr-R007	$1/2\text{Cr}_2\text{N} + \text{H}_2 = \text{CrH}_2 + 1/4\text{N}_2$	-8.45	-	-	-
Cr-R008	$1/3\text{Cr}_2\text{N} + \text{H}_2 = 2/3\text{CrH}_3 + 1/6\text{N}_2$	-6.74	-	-	-
Cr-R009	$2/3\text{Cr}_2\text{N} + \text{H}_2 = 4/3\text{Cr} + 2/3\text{NH}_3$	-11.87	53.08	-	endergonic
Cr-R010	$6/11\text{Cr}_2\text{N} + \text{H}_2 = 4/11\text{Cr}_3\text{H} + 6/11\text{NH}_3$	-11.3	-	-	-
Cr-R011	$2/5\text{Cr}_2\text{N} + \text{H}_2 = 4/5\text{CrH} + 2/5\text{NH}_3$	-10.16	57.47	-	endergonic
Cr-R012	$2/7\text{Cr}_2\text{N} + \text{H}_2 = 4/7\text{CrH}_2 + 2/7\text{NH}_3$	-8.45	-	-	-
Cr-R013	$2/9\text{Cr}_2\text{N} + \text{H}_2 = 4/9\text{CrH}_3 + 2/9\text{NH}_3$	-6.74	-	-	-
Cr-R014	$\text{Cr}_3\text{H} + \text{H}_2 = 3\text{CrH}$	1.28	-	-	-
Cr-R015	$2/5\text{Cr}_3\text{H} + \text{H}_2 = 6/5\text{CrH}_2$	3.21	-	-	-
Cr-R016	$1/4\text{Cr}_3\text{H} + \text{H}_2 = 3/4\text{CrH}_3$	5.14	-	-	-
Cr-R017	$2\text{Cr}_3\text{N}_2 + \text{H}_2 = 2\text{Cr}_3\text{H} + 2\text{N}_2$	-14.68	-	-	-
Cr-R018	$2/3\text{Cr}_3\text{N}_2 + \text{H}_2 = 2\text{CrH} + 2/3\text{N}_2$	-13.58	228.51	-	endergonic
Cr-R019	$1/3\text{Cr}_3\text{N}_2 + \text{H}_2 = \text{CrH}_2 + 1/3\text{N}_2$	-11.94	-	-	-
Cr-R020	$2/9\text{Cr}_3\text{N}_2 + \text{H}_2 = 2/3\text{CrH}_3 + 2/9\text{N}_2$	-10.29	-	-	-
Cr-R021	$1/3\text{Cr}_3\text{N}_2 + \text{H}_2 = \text{Cr} + 2/3\text{NH}_3$	-15.22	51.64	-	endergonic
Cr-R022	$2/7\text{Cr}_3\text{N}_2 + \text{H}_2 = 2/7\text{Cr}_3\text{H} + 4/7\text{NH}_3$	-14.68	-	-	-
Cr-R023	$2/9\text{Cr}_3\text{N}_2 + \text{H}_2 = 2/3\text{CrH} + 4/9\text{NH}_3$	-13.58	55.77	-	endergonic
Cr-R024	$1/6\text{Cr}_3\text{N}_2 + \text{H}_2 = 1/2\text{CrH}_2 + 1/3\text{NH}_3$	-11.94	-	-	-
Cr-R025	$2/15\text{Cr}_3\text{N}_2 + \text{H}_2 = 2/5\text{CrH}_3 + 4/15\text{NH}_3$	-10.29	-	-	-

Cr-R026	$4/3\text{Cr}_3\text{N}_2 + \text{H}_2 = 2\text{Cr}_2\text{N} + 2/3\text{NH}_3$	-3.81	47.31	-	endergonic
Cr-R027	$2\text{Cr}_3\text{N}_4 + \text{H}_2 = 2\text{Cr}_3\text{H} + 4\text{N}_2$	-25.95	-	-	-
Cr-R028	$2/3\text{Cr}_3\text{N}_4 + \text{H}_2 = 2\text{CrH} + 4/3\text{N}_2$	-25	228.02	-	endergonic
Cr-R029	$1/3\text{Cr}_3\text{N}_4 + \text{H}_2 = \text{CrH}_2 + 2/3\text{N}_2$	-23.57	-	-	-
Cr-R030	$2/9\text{Cr}_3\text{N}_4 + \text{H}_2 = 2/3\text{CrH}_3 + 4/9\text{N}_2$	-22.15	-	-	-
Cr-R031	$1/6\text{Cr}_3\text{N}_4 + \text{H}_2 = 1/2\text{Cr} + 2/3\text{NH}_3$	-26.43	10.4	-	endergonic
Cr-R032	$2/13\text{Cr}_3\text{N}_4 + \text{H}_2 = 2/13\text{Cr}_3\text{H} + 8/13\text{NH}_3$	-25.95	-	-	-
Cr-R033	$2/15\text{Cr}_3\text{N}_4 + \text{H}_2 = 2/5\text{CrH} + 8/15\text{NH}_3$	-25	21.13	-	endergonic
Cr-R034	$1/9\text{Cr}_3\text{N}_4 + \text{H}_2 = 1/3\text{CrH}_2 + 4/9\text{NH}_3$	-23.57	-	-	-
Cr-R035	$2/21\text{Cr}_3\text{N}_4 + \text{H}_2 = 2/7\text{CrH}_3 + 8/21\text{NH}_3$	-22.15	-	-	-
Cr-R036	$4/15\text{Cr}_3\text{N}_4 + \text{H}_2 = 2/5\text{Cr}_2\text{N} + 2/3\text{NH}_3$	-16.52	-15.22	-	exergonic
Cr-R037	$1/3\text{Cr}_3\text{N}_4 + \text{H}_2 = 1/3\text{Cr}_3\text{N}_2 + 2/3\text{NH}_3$	-13.21	-30.85	-	exergonic
Cr-R038	$2/3\text{Cr}_3\text{N}_4 + \text{H}_2 = 2\text{CrN} + 2/3\text{NH}_3$	-6.61	-100.93	-	exergonic
Cr-R039	$2\text{CrH} + \text{H}_2 = 2\text{CrH}_2$	1.9	-	-	-
Cr-R040	$\text{CrH} + \text{H}_2 = \text{CrH}_3$	3.8	-	-	-
Cr-R041	$2\text{CrH}_2 + \text{H}_2 = 2\text{CrH}_3$	1.87	-	-	-
Cr-R042	$6\text{CrN} + \text{H}_2 = 2\text{Cr}_3\text{H} + 3\text{N}_2$	-20.71	-	-	-
Cr-R043	$2\text{CrN} + \text{H}_2 = 2\text{CrH} + \text{N}_2$	-19.69	298.35	-	endergonic
Cr-R044	$\text{CrN} + \text{H}_2 = \text{CrH}_2 + 1/2\text{N}_2$	-18.17	-	-	-
Cr-R045	$2/3\text{CrN} + \text{H}_2 = 2/3\text{CrH}_3 + 1/3\text{N}_2$	-16.64	-	-	-
Cr-R046	$2/3\text{CrN} + \text{H}_2 = 2/3\text{Cr} + 2/3\text{NH}_3$	-21.22	47.51	-	endergonic
Cr-R047	$3/5\text{CrN} + \text{H}_2 = 1/5\text{Cr}_3\text{H} + 3/5\text{NH}_3$	-20.71	-	-	-
Cr-R048	$1/2\text{CrN} + \text{H}_2 = 1/2\text{CrH} + 1/2\text{NH}_3$	-19.69	51.64	-	endergonic
Cr-R049	$2/5\text{CrN} + \text{H}_2 = 2/5\text{CrH}_2 + 2/5\text{NH}_3$	-18.17	-	-	-
Cr-R050	$1/3\text{CrN} + \text{H}_2 = 1/3\text{CrH}_3 + 1/3\text{NH}_3$	-16.64	-	-	-
Cr-R051	$4/3\text{CrN} + \text{H}_2 = 2/3\text{Cr}_2\text{N} + 2/3\text{NH}_3$	-10.61	41.93	-	endergonic
Cr-R052	$2\text{CrN} + \text{H}_2 = 2/3\text{Cr}_3\text{N}_2 + 2/3\text{NH}_3$	-7.07	39.24	-	endergonic
Cr-R053	$6\text{CrN}_2 + \text{H}_2 = 2\text{Cr}_3\text{H} + 6\text{N}_2$	-34.59	-	-	-
Cr-R054	$2\text{CrN}_2 + \text{H}_2 = 2\text{CrH} + 2\text{N}_2$	-33.75	181.37	259.7	exergonic
Cr-R055	$\text{CrN}_2 + \text{H}_2 = \text{CrH}_2 + \text{N}_2$	-32.49	-	-	-
Cr-R056	$2/3\text{CrN}_2 + \text{H}_2 = 2/3\text{CrH}_3 + 2/3\text{N}_2$	-31.23	-	-	-
Cr-R057	$1/3\text{CrN}_2 + \text{H}_2 = 1/3\text{Cr} + 2/3\text{NH}_3$	-35.01	-11.04	-	exergonic
Cr-R058	$6/19\text{CrN}_2 + \text{H}_2 = 2/19\text{Cr}_3\text{H} + 12/19\text{NH}_3$	-34.59	-	-	-
Cr-R059	$2/7\text{CrN}_2 + \text{H}_2 = 2/7\text{CrH} + 4/7\text{NH}_3$	-33.75	-0.32	-	endergonic
Cr-R060	$1/4\text{CrN}_2 + \text{H}_2 = 1/4\text{CrH}_2 + 1/2\text{NH}_3$	-32.49	-	-	-
Cr-R061	$2/9\text{CrN}_2 + \text{H}_2 = 2/9\text{CrH}_3 + 4/9\text{NH}_3$	-31.23	-	-	-
Cr-R062	$4/9\text{CrN}_2 + \text{H}_2 = 2/9\text{Cr}_2\text{N} + 2/3\text{NH}_3$	-26.26	-32.42	-	exergonic
Cr-R063	$1/2\text{CrN}_2 + \text{H}_2 = 1/6\text{Cr}_3\text{N}_2 + 2/3\text{NH}_3$	-23.34	-42.38	-	exergonic
Cr-R064	$\text{CrN}_2 + \text{H}_2 = 1/3\text{Cr}_3\text{N}_4 + 2/3\text{NH}_3$	-11.67	-53.92	-	exergonic
Cr-R065	$2/3\text{CrN}_2 + \text{H}_2 = 2/3\text{CrN} + 2/3\text{NH}_3$	-17.51	-69.59	-	exergonic
Cr-R066	$4\text{Cr} + \text{N}_2 = 2\text{Cr}_2\text{N}$	13.47	-251.04	-	exergonic
Cr-R067	$3\text{Cr} + \text{N}_2 = \text{Cr}_3\text{N}_2$	17.96	-246.71	-	exergonic
Cr-R068	$3/2\text{Cr} + \text{N}_2 = 1/2\text{Cr}_3\text{N}_4$	35.92	-122.98	409.5	exergonic
Cr-R069	$2\text{Cr} + \text{N}_2 = 2\text{CrN}$	26.94	-234.31	-	exergonic
Cr-R070	$\text{Cr} + \text{N}_2 = \text{CrN}_2$	53.88	-58.66	-	endergonic
Cr-R071	$6\text{Cr}_2\text{N} + \text{N}_2 = 4\text{Cr}_3\text{N}_2$	3.96	-233.71	513.8	exergonic
Cr-R072	$6/5\text{Cr}_2\text{N} + \text{N}_2 = 4/5\text{Cr}_3\text{N}_4$	19.78	-46.15	-	endergonic
Cr-R073	$2\text{Cr}_2\text{N} + \text{N}_2 = 4\text{CrN}$	11.87	-217.58	-	exergonic
Cr-R074	$2/3\text{Cr}_2\text{N} + \text{N}_2 = 4/3\text{CrN}_2$	35.61	5.46	-	endergonic

Cr-R075	$4/3\text{Cr}_3\text{H} + \text{N}_2 = 2\text{Cr}_2\text{N} + 2/3\text{H}_2$	12.74	-	-	-
Cr-R076	$\text{Cr}_3\text{H} + \text{N}_2 = \text{Cr}_3\text{N}_2 + 1/2\text{H}_2$	17.2	-	-	-
Cr-R077	$1/2\text{Cr}_3\text{H} + \text{N}_2 = 1/2\text{Cr}_3\text{N}_4 + 1/4\text{H}_2$	35.05	-	-	-
Cr-R078	$2/3\text{Cr}_3\text{H} + \text{N}_2 = 2\text{CrN} + 1/3\text{H}_2$	26.12	-	-	-
Cr-R079	$1/3\text{Cr}_3\text{H} + \text{N}_2 = \text{CrN}_2 + 1/6\text{H}_2$	52.89	-	-	-
Cr-R080	$6\text{Cr}_3\text{H} + \text{N}_2 = 18\text{Cr} + 2\text{NH}_3$	-0.64	-	-	-
Cr-R081	$12/11\text{Cr}_3\text{H} + \text{N}_2 = 18/11\text{Cr}_2\text{N} + 4/11\text{NH}_3$	12.74	-	-	-
Cr-R082	$6/7\text{Cr}_3\text{H} + \text{N}_2 = 6/7\text{Cr}_3\text{N}_2 + 2/7\text{NH}_3$	17.2	-	-	-
Cr-R083	$6/13\text{Cr}_3\text{H} + \text{N}_2 = 6/13\text{Cr}_3\text{N}_4 + 2/13\text{NH}_3$	35.05	-	-	-
Cr-R084	$3/5\text{Cr}_3\text{H} + \text{N}_2 = 9/5\text{CrN} + 1/5\text{NH}_3$	26.12	-	-	-
Cr-R085	$6/19\text{Cr}_3\text{H} + \text{N}_2 = 18/19\text{Cr}_2\text{N}_2 + 2/19\text{NH}_3$	52.89	-	-	-
Cr-R086	$\text{Cr}_3\text{N}_2 + \text{N}_2 = \text{Cr}_3\text{N}_4$	15.22	0.74	-	endergonic
Cr-R087	$2\text{Cr}_3\text{N}_2 + \text{N}_2 = 6\text{CrN}$	7.61	-209.51	-	exergonic
Cr-R088	$1/2\text{Cr}_3\text{N}_2 + \text{N}_2 = 3/2\text{CrN}_2$	30.45	35.36	-	endergonic
Cr-R089	$\text{Cr}_3\text{N}_4 + \text{N}_2 = 3\text{CrN}_2$	13.21	69.97	-	endergonic
Cr-R090	$4\text{CrH} + \text{N}_2 = 2\text{Cr}_2\text{N} + 2\text{H}_2$	11.31	-379.12	-	exergonic
Cr-R091	$3\text{CrH} + \text{N}_2 = \text{Cr}_3\text{N}_2 + 3/2\text{H}_2$	15.72	-342.77	-	exergonic
Cr-R092	$3/2\text{CrH} + \text{N}_2 = 1/2\text{Cr}_3\text{N}_4 + 3/4\text{H}_2$	33.33	-171.01	-	exergonic
Cr-R093	$2\text{CrH} + \text{N}_2 = 2\text{CrN} + \text{H}_2$	24.52	-298.35	-	exergonic
Cr-R094	$\text{CrH} + \text{N}_2 = \text{CrN}_2 + 1/2\text{H}_2$	50.95	-90.68	259.7	exergonic
Cr-R095	$6\text{CrH} + \text{N}_2 = 6\text{Cr} + 2\text{NH}_3$	-1.9	-283.91	-	exergonic
Cr-R096	$9\text{CrH} + \text{N}_2 = 3\text{Cr}_3\text{H} + 2\text{NH}_3$	-1.27	-	-	-
Cr-R097	$12/5\text{CrH} + \text{N}_2 = 6/5\text{Cr}_2\text{N} + 4/5\text{NH}_3$	11.31	-264.19	-	exergonic
Cr-R098	$2\text{CrH} + \text{N}_2 = 2/3\text{Cr}_3\text{N}_2 + 2/3\text{NH}_3$	15.72	-259.11	-	exergonic
Cr-R099	$6/5\text{CrH} + \text{N}_2 = 2/5\text{Cr}_3\text{N}_4 + 2/5\text{NH}_3$	33.33	-155.17	-	exergonic
Cr-R100	$3/2\text{CrH} + \text{N}_2 = 3/2\text{CrN} + 1/2\text{NH}_3$	24.52	-246.71	-	exergonic
Cr-R101	$6/7\text{CrH} + \text{N}_2 = 6/7\text{Cr}_2\text{N}_2 + 2/7\text{NH}_3$	50.95	-90.84	247.6	exergonic
Cr-R102	$4\text{CrH}_2 + \text{N}_2 = 2\text{Cr}_2\text{N} + 4\text{H}_2$	9.23	-	-	-
Cr-R103	$3\text{CrH}_2 + \text{N}_2 = \text{Cr}_3\text{N}_2 + 3\text{H}_2$	13.56	-	-	-
Cr-R104	$3/2\text{CrH}_2 + \text{N}_2 = 1/2\text{Cr}_3\text{N}_4 + 3/2\text{H}_2$	30.84	-	-	-
Cr-R105	$2\text{CrH}_2 + \text{N}_2 = 2\text{CrN} + 2\text{H}_2$	22.2	-	-	-
Cr-R106	$\text{CrH}_2 + \text{N}_2 = \text{CrN}_2 + \text{H}_2$	48.13	-	-	-
Cr-R107	$3\text{CrH}_2 + \text{N}_2 = 3\text{Cr} + 2\text{NH}_3$	-3.73	-	-	-
Cr-R108	$18/5\text{CrH}_2 + \text{N}_2 = 6/5\text{Cr}_3\text{H} + 2\text{NH}_3$	-3.11	-	-	-
Cr-R109	$6\text{CrH}_2 + \text{N}_2 = 6\text{CrH} + 2\text{NH}_3$	-1.87	-	-	-
Cr-R110	$12/7\text{CrH}_2 + \text{N}_2 = 6/7\text{Cr}_2\text{N} + 8/7\text{NH}_3$	9.23	-	-	-
Cr-R111	$3/2\text{CrH}_2 + \text{N}_2 = 1/2\text{Cr}_3\text{N}_2 + \text{NH}_3$	13.56	-	-	-
Cr-R112	$\text{CrH}_2 + \text{N}_2 = 1/3\text{Cr}_3\text{N}_4 + 2/3\text{NH}_3$	30.84	-	-	-
Cr-R113	$6/5\text{CrH}_2 + \text{N}_2 = 6/5\text{CrN} + 4/5\text{NH}_3$	22.2	-	-	-
Cr-R114	$3/4\text{CrH}_2 + \text{N}_2 = 3/4\text{Cr}_2\text{N}_2 + 1/2\text{NH}_3$	48.13	-	-	-
Cr-R115	$4\text{CrH}_3 + \text{N}_2 = 2\text{Cr}_2\text{N} + 6\text{H}_2$	7.23	-	-	-
Cr-R116	$3\text{CrH}_3 + \text{N}_2 = \text{Cr}_3\text{N}_2 + 9/2\text{H}_2$	11.48	-	-	-
Cr-R117	$3/2\text{CrH}_3 + \text{N}_2 = 1/2\text{Cr}_3\text{N}_4 + 9/4\text{H}_2$	28.45	-	-	-
Cr-R118	$2\text{CrH}_3 + \text{N}_2 = 2\text{CrN} + 3\text{H}_2$	19.96	-	-	-
Cr-R119	$\text{CrH}_3 + \text{N}_2 = \text{CrN}_2 + 3/2\text{H}_2$	45.42	-	-	-
Cr-R120	$2\text{CrH}_3 + \text{N}_2 = 2\text{Cr} + 2\text{NH}_3$	-5.5	-	-	-
Cr-R121	$9/4\text{CrH}_3 + \text{N}_2 = 3/4\text{Cr}_3\text{H} + 2\text{NH}_3$	-4.89	-	-	-
Cr-R122	$3\text{CrH}_3 + \text{N}_2 = 3\text{CrH} + 2\text{NH}_3$	-3.66	-	-	-
Cr-R123	$6\text{CrH}_3 + \text{N}_2 = 6\text{CrH}_2 + 2\text{NH}_3$	-1.83	-	-	-

Cr-R124	$4/3\text{CrH}_3 + \text{N}_2 = 2/3\text{Cr}_2\text{N} + 4/3\text{NH}_3$	7.23	-	-	-
Cr-R125	$6/5\text{CrH}_3 + \text{N}_2 = 2/5\text{Cr}_3\text{N}_2 + 6/5\text{NH}_3$	11.48	-	-	-
Cr-R126	$6/7\text{CrH}_3 + \text{N}_2 = 2/7\text{Cr}_3\text{N}_4 + 6/7\text{NH}_3$	28.45	-	-	-
Cr-R127	$\text{CrH}_3 + \text{N}_2 = \text{CrN} + \text{NH}_3$	19.96	-	-	-
Cr-R128	$2/3\text{CrH}_3 + \text{N}_2 = 2/3\text{Cr}_2\text{N} + 2/3\text{NH}_3$	45.42	-	-	-
Cr-R129	$6\text{CrN} + \text{N}_2 = 2\text{Cr}_3\text{N}_4$	7.07	211	-	endergonic
Cr-R130	$2\text{CrN} + \text{N}_2 = 2\text{CrN}_2$	21.22	116.98	-	endergonic

Table S18: The Cu-based system

ID	Reaction	dm_stoich [%]	h298 [kJ/mol]	T_eq [°C]	Type
Cu-R01	$2\text{Cu} + \text{H}_2 = 2\text{CuH}$	1.59	44.46	-	endergonic
Cu-R02	$1/5\text{Cu}_{10}\text{N}_3 + \text{H}_2 = 2\text{CuH} + 3/10\text{N}_2$	-4.71	-	-	-
Cu-R03	$2/9\text{Cu}_{10}\text{N}_3 + \text{H}_2 = 20/9\text{Cu} + 2/3\text{NH}_3$	-6.2	-	-	-
Cu-R04	$2/19\text{Cu}_{10}\text{N}_3 + \text{H}_2 = 20/19\text{CuH} + 6/19\text{NH}_3$	-4.71	-	-	-
Cu-R05	$\text{Cu}_2\text{N} + \text{H}_2 = 2\text{CuH} + 1/2\text{N}_2$	-8.5	-	-	-
Cu-R06	$2/3\text{Cu}_2\text{N} + \text{H}_2 = 4/3\text{Cu} + 2/3\text{NH}_3$	-9.93	-	-	-
Cu-R07	$2/5\text{Cu}_2\text{N} + \text{H}_2 = 4/5\text{CuH} + 2/5\text{NH}_3$	-8.5	-	-	-
Cu-R08	$5/3\text{Cu}_2\text{N} + \text{H}_2 = 1/3\text{Cu}_{10}\text{N}_3 + 2/3\text{NH}_3$	-3.97	-	-	-
Cu-R09	$2\text{Cu}_2\text{N} + \text{H}_2 = 4/3\text{Cu}_3\text{N} + 2/3\text{NH}_3$	-3.31	-	-	-
Cu-R10	$2/3\text{Cu}_3\text{N} + \text{H}_2 = 2\text{CuH} + 1/3\text{N}_2$	-5.37	-4.97	-	endergonic
Cu-R11	$2/3\text{Cu}_3\text{N} + \text{H}_2 = 2\text{Cu} + 2/3\text{NH}_3$	-6.84	-80.03	-	exergonic
Cu-R12	$1/3\text{Cu}_3\text{N} + \text{H}_2 = \text{CuH} + 1/3\text{NH}_3$	-5.37	-17.78	78.7	exergonic
Cu-R13	$20/3\text{Cu}_3\text{N} + \text{H}_2 = 2\text{Cu}_{10}\text{N}_3 + 2/3\text{NH}_3$	-0.68	-	-	-
Cu-R14	$2\text{CuN} + \text{H}_2 = 2\text{CuH} + \text{N}_2$	-16.76	-262.75	-	exergonic
Cu-R15	$2/3\text{CuN} + \text{H}_2 = 2/3\text{Cu} + 2/3\text{NH}_3$	-18.06	-133	-	exergonic
Cu-R16	$1/2\text{CuN} + \text{H}_2 = 1/2\text{CuH} + 1/2\text{NH}_3$	-16.76	-88.64	-	exergonic
Cu-R17	$20/21\text{CuN} + \text{H}_2 = 2/21\text{Cu}_{10}\text{N}_3 + 2/3\text{NH}_3$	-12.64	-	-	-
Cu-R18	$4/3\text{CuN} + \text{H}_2 = 2/3\text{Cu}_2\text{N} + 2/3\text{NH}_3$	-9.03	-	-	-
Cu-R19	$\text{CuN} + \text{H}_2 = 1/3\text{Cu}_3\text{N} + 2/3\text{NH}_3$	-12.04	-159.49	-	exergonic
Cu-R20	$2\text{CuN}_3 + \text{H}_2 = 2\text{CuH} + 3\text{N}_2$	-38.85	-182.34	-	exergonic
Cu-R21	$2/9\text{CuN}_3 + \text{H}_2 = 2/9\text{Cu} + 2/3\text{NH}_3$	-39.81	-55.8	-	exergonic
Cu-R22	$1/5\text{CuN}_3 + \text{H}_2 = 1/5\text{CuH} + 3/5\text{NH}_3$	-38.85	-45.77	681.5	exergonic
Cu-R23	$20/81\text{CuN}_3 + \text{H}_2 = 2/81\text{Cu}_{10}\text{N}_3 + 2/3\text{NH}_3$	-35.82	-	-	-
Cu-R24	$4/15\text{CuN}_3 + \text{H}_2 = 2/15\text{Cu}_2\text{N} + 2/3\text{NH}_3$	-33.17	-	-	-
Cu-R25	$1/4\text{CuN}_3 + \text{H}_2 = 1/12\text{Cu}_3\text{N} + 2/3\text{NH}_3$	-35.38	-52.77	-	exergonic
Cu-R26	$1/3\text{CuN}_3 + \text{H}_2 = 1/3\text{CuN} + 2/3\text{NH}_3$	-26.54	-17.19	114.8	exergonic
Cu-R27	$2\text{CuN}_6 + \text{H}_2 = 2\text{CuH} + 6\text{N}_2$	-56.26	-413.77	-	exergonic
Cu-R28	$1/9\text{CuN}_6 + \text{H}_2 = 1/9\text{Cu} + 2/3\text{NH}_3$	-56.94	-56.05	-	exergonic
Cu-R29	$2/19\text{CuN}_6 + \text{H}_2 = 2/19\text{CuH} + 12/19\text{NH}_3$	-56.26	-50.76	-	exergonic
Cu-R30	$20/171\text{CuN}_6 + \text{H}_2 = 2/171\text{Cu}_{10}\text{N}_3 + 2/3\text{NH}_3$	-54.1	-	-	-
Cu-R31	$4/33\text{CuN}_6 + \text{H}_2 = 2/33\text{Cu}_2\text{N} + 2/3\text{NH}_3$	-52.2	-	-	-
Cu-R32	$2/17\text{CuN}_6 + \text{H}_2 = 2/51\text{Cu}_3\text{N} + 2/3\text{NH}_3$	-53.78	-54.64	-	exergonic
Cu-R33	$2/15\text{CuN}_6 + \text{H}_2 = 2/15\text{CuN} + 2/3\text{NH}_3$	-47.45	-40.67	784.7	exergonic
Cu-R34	$2/9\text{CuN}_6 + \text{H}_2 = 2/9\text{CuN}_3 + 2/3\text{NH}_3$	-28.47	-56.31	-	exergonic
Cu-R35	$2\text{CuN}_8 + \text{H}_2 = 2\text{CuH} + 8\text{N}_2$	-63.24	-	-	-
Cu-R36	$1/12\text{CuN}_8 + \text{H}_2 = 1/12\text{Cu} + 2/3\text{NH}_3$	-63.81	-	-	-
Cu-R37	$2/25\text{CuN}_8 + \text{H}_2 = 2/25\text{CuH} + 16/25\text{NH}_3$	-63.24	-	-	-
Cu-R38	$20/231\text{CuN}_8 + \text{H}_2 = 2/231\text{Cu}_{10}\text{N}_3 + 2/3\text{NH}_3$	-61.42	-	-	-

Cu-R39	$4/45\text{CuN}_8 + \text{H}_2 = 2/45\text{Cu}_2\text{N} + 2/3\text{NH}_3$	-59.82	-	-	-
Cu-R40	$2/23\text{CuN}_8 + \text{H}_2 = 2/69\text{Cu}_3\text{N} + 2/3\text{NH}_3$	-61.15	-	-	-
Cu-R41	$2/21\text{CuN}_8 + \text{H}_2 = 2/21\text{CuN} + 2/3\text{NH}_3$	-55.84	-	-	-
Cu-R42	$2/15\text{CuN}_8 + \text{H}_2 = 2/15\text{Cu}_3\text{N} + 2/3\text{NH}_3$	-39.88	-	-	-
Cu-R43	$1/3\text{CuN}_8 + \text{H}_2 = 1/3\text{CuN}_6 + 2/3\text{NH}_3$	-15.95	-	-	-
Cu-R44	$20/3\text{Cu} + \text{N}_2 = 2/3\text{Cu}_{10}\text{N}_3$	6.61	-	-	-
Cu-R45	$4\text{Cu} + \text{N}_2 = 2\text{Cu}_2\text{N}$	11.02	-	-	-
Cu-R46	$6\text{Cu} + \text{N}_2 = 2\text{Cu}_3\text{N}$	7.35	148.29	-	endergonic
Cu-R47	$2\text{Cu} + \text{N}_2 = 2\text{CuN}$	22.04	307.21	-	endergonic
Cu-R48	$2/3\text{Cu} + \text{N}_2 = 2/3\text{Cu}_3\text{N}$	66.13	75.6	-	endergonic
Cu-R49	$1/3\text{Cu} + \text{N}_2 = 1/3\text{CuN}_6$	132.25	76.37	-	endergonic
Cu-R50	$1/4\text{Cu} + \text{N}_2 = 1/4\text{CuN}_8$	176.34	-	-	-
Cu-R51	$\text{Cu}_{10}\text{N}_3 + \text{N}_2 = 5\text{Cu}_2\text{N}$	4.14	-	-	-
Cu-R52	$6\text{Cu}_{10}\text{N}_3 + \text{N}_2 = 20\text{Cu}_3\text{N}$	0.69	-	-	-
Cu-R53	$2/7\text{Cu}_{10}\text{N}_3 + \text{N}_2 = 20/7\text{CuN}$	14.47	-	-	-
Cu-R54	$2/27\text{Cu}_{10}\text{N}_3 + \text{N}_2 = 20/27\text{Cu}_3\text{N}$	55.82	-	-	-
Cu-R55	$2/57\text{Cu}_{10}\text{N}_3 + \text{N}_2 = 20/57\text{CuN}_6$	117.85	-	-	-
Cu-R56	$2/77\text{Cu}_{10}\text{N}_3 + \text{N}_2 = 20/77\text{CuN}_8$	159.2	-	-	-
Cu-R57	$2\text{Cu}_2\text{N} + \text{N}_2 = 4\text{CuN}$	9.93	-	-	-
Cu-R58	$2/5\text{Cu}_2\text{N} + \text{N}_2 = 4/5\text{Cu}_3\text{N}$	49.64	-	-	-
Cu-R59	$2/11\text{Cu}_2\text{N} + \text{N}_2 = 4/11\text{CuN}_6$	109.2	-	-	-
Cu-R60	$2/15\text{Cu}_2\text{N} + \text{N}_2 = 4/15\text{CuN}_8$	148.91	-	-	-
Cu-R61	$4\text{Cu}_3\text{N} + \text{N}_2 = 6\text{Cu}_2\text{N}$	3.42	-	-	-
Cu-R62	$\text{Cu}_3\text{N} + \text{N}_2 = 3\text{CuN}$	13.69	386.67	-	endergonic
Cu-R63	$1/4\text{Cu}_3\text{N} + \text{N}_2 = 3/4\text{Cu}_3\text{N}$	54.76	66.51	-	endergonic
Cu-R64	$2/17\text{Cu}_3\text{N} + \text{N}_2 = 6/17\text{CuN}_6$	116.36	72.14	-	endergonic
Cu-R65	$2/23\text{Cu}_3\text{N} + \text{N}_2 = 6/23\text{CuN}_8$	157.42	-	-	-
Cu-R66	$20/3\text{CuH} + \text{N}_2 = 2/3\text{Cu}_{10}\text{N}_3 + 10/3\text{H}_2$	4.95	-	-	-
Cu-R67	$4\text{CuH} + \text{N}_2 = 2\text{Cu}_2\text{N} + 2\text{H}_2$	9.29	-	-	-
Cu-R68	$6\text{CuH} + \text{N}_2 = 2\text{Cu}_3\text{N} + 3\text{H}_2$	5.67	14.91	-	exergonic
Cu-R69	$2\text{CuH} + \text{N}_2 = 2\text{CuN} + \text{H}_2$	20.14	262.75	-	endergonic
Cu-R70	$2/3\text{CuH} + \text{N}_2 = 2/3\text{Cu}_3\text{N} + 1/3\text{H}_2$	63.53	60.78	-	endergonic
Cu-R71	$1/3\text{CuH} + \text{N}_2 = 1/3\text{CuN}_6 + 1/6\text{H}_2$	128.63	68.96	-	endergonic
Cu-R72	$1/4\text{CuH} + \text{N}_2 = 1/4\text{CuN}_8 + 1/8\text{H}_2$	172.02	-	-	-
Cu-R73	$6\text{CuH} + \text{N}_2 = 6\text{Cu} + 2\text{NH}_3$	-1.56	-225.17	-	exergonic
Cu-R74	$60/19\text{CuH} + \text{N}_2 = 6/19\text{Cu}_{10}\text{N}_3 + 20/19\text{NH}_3$	4.95	-	-	-
Cu-R75	$12/5\text{CuH} + \text{N}_2 = 6/5\text{Cu}_2\text{N} + 4/5\text{NH}_3$	9.29	-	-	-
Cu-R76	$3\text{CuH} + \text{N}_2 = \text{Cu}_3\text{N} + \text{NH}_3$	5.67	-38.44	408.9	exergonic
Cu-R77	$3/2\text{CuH} + \text{N}_2 = 3/2\text{CuN} + 1/2\text{NH}_3$	20.14	174.12	-	endergonic
Cu-R78	$3/5\text{CuH} + \text{N}_2 = 3/5\text{Cu}_3\text{N} + 1/5\text{NH}_3$	63.53	45.52	-	endergonic
Cu-R79	$6/19\text{CuH} + \text{N}_2 = 6/19\text{CuN}_6 + 2/19\text{NH}_3$	128.63	60.5	-	endergonic
Cu-R80	$6/25\text{CuH} + \text{N}_2 = 6/25\text{CuN}_8 + 2/25\text{NH}_3$	172.02	-	-	-
Cu-R81	$\text{CuN} + \text{N}_2 = \text{CuN}_3$	36.12	-40.21	374.1	exergonic
Cu-R82	$2/5\text{CuN} + \text{N}_2 = 2/5\text{CuN}_6$	90.31	30.2	-	endergonic
Cu-R83	$2/7\text{CuN} + \text{N}_2 = 2/7\text{CuN}_8$	126.43	-	-	-
Cu-R84	$2/3\text{Cu}_3\text{N} + \text{N}_2 = 2/3\text{CuN}_6$	39.81	77.14	-	endergonic
Cu-R85	$2/5\text{Cu}_3\text{N} + \text{N}_2 = 2/5\text{CuN}_8$	66.34	-	-	-
Cu-R86	$\text{CuN}_6 + \text{N}_2 = \text{CuN}_8$	18.98	-	-	-



Table S19: The Fe-based system

ID	Reaction	dm_stoich [%]	h298 [kJ/mol]	T_eq [°C]	Type
Fe-R001	$6\text{Fe} + \text{H}_2 = 2\text{Fe}_3\text{H}$	0.6	-	-	-
Fe-R002	$2\text{Fe} + \text{H}_2 = 2\text{FeH}$	1.8	-25.94	-	endergonic
Fe-R003	$2/3\text{Fe} + \text{H}_2 = 2/3\text{FeH}_3$	5.41	38.34	-	endergonic
Fe-R004	$1/2\text{Fe} + \text{H}_2 = 1/2\text{FeH}_4$	7.22	-	-	-
Fe-R005	$1/2\text{Fe}12\text{N}_5 + \text{H}_2 = 2\text{Fe}_3\text{H} + 5/4\text{N}_2$	-8.92	-	-	-
Fe-R006	$1/6\text{Fe}12\text{N}_5 + \text{H}_2 = 2\text{FeH} + 5/12\text{N}_2$	-7.83	-	-	-
Fe-R007	$1/18\text{Fe}12\text{N}_5 + \text{H}_2 = 2/3\text{FeH}_3 + 5/36\text{N}_2$	-4.56	-	-	-
Fe-R008	$1/24\text{Fe}12\text{N}_5 + \text{H}_2 = 1/2\text{FeH}_4 + 5/48\text{N}_2$	-2.93	-	-	-
Fe-R009	$2/15\text{Fe}12\text{N}_5 + \text{H}_2 = 8/5\text{Fe} + 2/3\text{NH}_3$	-9.46	-	-	-
Fe-R010	$2/19\text{Fe}12\text{N}_5 + \text{H}_2 = 8/19\text{Fe}_3\text{H} + 10/19\text{NH}_3$	-8.92	-	-	-
Fe-R011	$2/27\text{Fe}12\text{N}_5 + \text{H}_2 = 8/9\text{FeH} + 10/27\text{NH}_3$	-7.83	-	-	-
Fe-R012	$2/51\text{Fe}12\text{N}_5 + \text{H}_2 = 8/17\text{FeH}_3 + 10/51\text{NH}_3$	-4.56	-	-	-
Fe-R013	$2/63\text{Fe}12\text{N}_5 + \text{H}_2 = 8/21\text{FeH}_4 + 10/63\text{NH}_3$	-2.93	-	-	-
Fe-R014	$2/3\text{Fe}12\text{N}_5 + \text{H}_2 = 8/3\text{Fe}_3\text{N} + 2/3\text{NH}_3$	-1.89	-	-	-
Fe-R015	$1/3\text{Fe}12\text{N}_5 + \text{H}_2 = \text{Fe}_4\text{N} + 2/3\text{NH}_3$	-3.78	-	-	-
Fe-R016	$4/21\text{Fe}12\text{N}_5 + \text{H}_2 = 2/7\text{Fe}_8\text{N} + 2/3\text{NH}_3$	-6.62	-	-	-
Fe-R017	$4/3\text{Fe}12\text{N}_5 + \text{H}_2 = 2\text{Fe}_8\text{N}_3 + 2/3\text{NH}_3$	-0.95	-	-	-
Fe-R018	$1/4\text{Fe}24\text{N}_{11} + \text{H}_2 = 2\text{Fe}_3\text{H} + 11/8\text{N}_2$	-9.77	-	-	-
Fe-R019	$1/12\text{Fe}24\text{N}_{11} + \text{H}_2 = 2\text{FeH} + 11/24\text{N}_2$	-8.69	-	-	-
Fe-R020	$1/36\text{Fe}24\text{N}_{11} + \text{H}_2 = 2/3\text{FeH}_3 + 11/72\text{N}_2$	-5.45	-	-	-
Fe-R021	$1/48\text{Fe}24\text{N}_{11} + \text{H}_2 = 1/2\text{FeH}_4 + 11/96\text{N}_2$	-3.84	-	-	-
Fe-R022	$2/33\text{Fe}24\text{N}_{11} + \text{H}_2 = 16/11\text{Fe} + 2/3\text{NH}_3$	-10.31	-	-	-
Fe-R023	$2/41\text{Fe}24\text{N}_{11} + \text{H}_2 = 16/41\text{Fe}_3\text{H} + 22/41\text{NH}_3$	-9.77	-	-	-
Fe-R024	$2/57\text{Fe}24\text{N}_{11} + \text{H}_2 = 16/19\text{FeH} + 22/57\text{NH}_3$	-8.69	-	-	-
Fe-R025	$2/105\text{Fe}24\text{N}_{11} + \text{H}_2 = 16/35\text{FeH}_3 + 22/105\text{NH}_3$	-5.45	-	-	-
Fe-R026	$2/129\text{Fe}24\text{N}_{11} + \text{H}_2 = 16/43\text{FeH}_4 + 22/129\text{NH}_3$	-3.84	-	-	-
Fe-R027	$2/3\text{Fe}24\text{N}_{11} + \text{H}_2 = 4/3\text{Fe}12\text{N}_5 + 2/3\text{NH}_3$	-0.94	-	-	-
Fe-R028	$2/9\text{Fe}24\text{N}_{11} + \text{H}_2 = 16/9\text{Fe}_3\text{N} + 2/3\text{NH}_3$	-2.81	-	-	-
Fe-R029	$2/15\text{Fe}24\text{N}_{11} + \text{H}_2 = 4/5\text{Fe}_4\text{N} + 2/3\text{NH}_3$	-4.69	-	-	-
Fe-R030	$1/12\text{Fe}24\text{N}_{11} + \text{H}_2 = 1/4\text{Fe}_8\text{N} + 2/3\text{NH}_3$	-7.5	-	-	-
Fe-R031	$1/3\text{Fe}24\text{N}_{11} + \text{H}_2 = \text{Fe}_8\text{N}_3 + 2/3\text{NH}_3$	-1.87	-	-	-
Fe-R032	$3\text{Fe}_2\text{N} + \text{H}_2 = 2\text{Fe}_3\text{H} + 3/2\text{N}_2$	-10.61	-	-	-
Fe-R033	$\text{Fe}_2\text{N} + \text{H}_2 = 2\text{FeH} + 1/2\text{N}_2$	-9.54	-22.18	61.6	exergonic
Fe-R034	$1/3\text{Fe}_2\text{N} + \text{H}_2 = 2/3\text{FeH}_3 + 1/6\text{N}_2$	-6.33	39.6	-	endergonic
Fe-R035	$1/4\text{Fe}_2\text{N} + \text{H}_2 = 1/2\text{FeH}_4 + 1/8\text{N}_2$	-4.73	-	-	-
Fe-R036	$2/3\text{Fe}_2\text{N} + \text{H}_2 = 4/3\text{Fe} + 2/3\text{NH}_3$	-11.14	-28.09	468.6	exergonic
Fe-R037	$6/11\text{Fe}_2\text{N} + \text{H}_2 = 4/11\text{Fe}_3\text{H} + 6/11\text{NH}_3$	-10.61	-	-	-
Fe-R038	$2/5\text{Fe}_2\text{N} + \text{H}_2 = 4/5\text{FeH} + 2/5\text{NH}_3$	-9.54	-27.23	136.2	exergonic
Fe-R039	$2/9\text{Fe}_2\text{N} + \text{H}_2 = 4/9\text{FeH}_3 + 2/9\text{NH}_3$	-6.33	16.2	-	endergonic
Fe-R040	$2/11\text{Fe}_2\text{N} + \text{H}_2 = 4/11\text{FeH}_4 + 2/11\text{NH}_3$	-4.73	-	-	-
Fe-R041	$4\text{Fe}_2\text{N} + \text{H}_2 = 2/3\text{Fe}12\text{N}_5 + 2/3\text{NH}_3$	-1.86	-	-	-
Fe-R042	$8\text{Fe}_2\text{N} + \text{H}_2 = 2/3\text{Fe}24\text{N}_{11} + 2/3\text{NH}_3$	-0.93	-	-	-
Fe-R043	$2\text{Fe}_2\text{N} + \text{H}_2 = 4/3\text{Fe}_3\text{N} + 2/3\text{NH}_3$	-3.71	-104.24	459.3	exergonic
Fe-R044	$4/3\text{Fe}_2\text{N} + \text{H}_2 = 2/3\text{Fe}_4\text{N} + 2/3\text{NH}_3$	-5.57	-32.97	571.6	exergonic
Fe-R045	$8/9\text{Fe}_2\text{N} + \text{H}_2 = 2/9\text{Fe}_8\text{N} + 2/3\text{NH}_3$	-8.36	-40.56	456.5	exergonic

Fe-R046	$8/3\text{Fe}_2\text{N} + \text{H}_2 = 2/3\text{Fe}_8\text{N}_3 + 2/3\text{NH}_3$	-2.79	-129.81	656.3	exergonic
Fe-R047	$\text{Fe}_3\text{H} + \text{H}_2 = 3\text{FeH}$	1.2	-	-	-
Fe-R048	$1/4\text{Fe}_3\text{H} + \text{H}_2 = 3/4\text{FeH}_3$	4.78	-	-	-
Fe-R049	$2/11\text{Fe}_3\text{H} + \text{H}_2 = 6/11\text{FeH}_4$	6.58	-	-	-
Fe-R050	$2\text{Fe}_3\text{N} + \text{H}_2 = 2\text{Fe}_3\text{H} + \text{N}_2$	-7.16	-	-	-
Fe-R051	$2/3\text{Fe}_3\text{N} + \text{H}_2 = 2\text{FeH} + 1/3\text{N}_2$	-6.05	14.64	-	endergonic
Fe-R052	$2/9\text{Fe}_3\text{N} + \text{H}_2 = 2/3\text{FeH}_3 + 1/9\text{N}_2$	-2.72	51.87	-	endergonic
Fe-R053	$1/6\text{Fe}_3\text{N} + \text{H}_2 = 1/2\text{FeH}_4 + 1/12\text{N}_2$	-1.05	-	-	-
Fe-R054	$2/3\text{Fe}_3\text{N} + \text{H}_2 = 2\text{Fe} + 2/3\text{NH}_3$	-7.72	9.99	415.8	exergonic
Fe-R055	$1/2\text{Fe}_3\text{N} + \text{H}_2 = 1/2\text{Fe}_3\text{H} + 1/2\text{NH}_3$	-7.16	-	-	-
Fe-R056	$1/3\text{Fe}_3\text{N} + \text{H}_2 = \text{FeH} + 1/3\text{NH}_3$	-6.05	-7.98	-	endergonic
Fe-R057	$1/6\text{Fe}_3\text{N} + \text{H}_2 = 1/2\text{FeH}_3 + 1/6\text{NH}_3$	-2.72	31.25	-	endergonic
Fe-R058	$2/15\text{Fe}_3\text{N} + \text{H}_2 = 2/5\text{FeH}_4 + 2/15\text{NH}_3$	-1.05	-	-	-
Fe-R059	$8/3\text{Fe}_3\text{N} + \text{H}_2 = 2\text{Fe}_4\text{N} + 2/3\text{NH}_3$	-1.93	109.57	380.7	exergonic
Fe-R060	$16/15\text{Fe}_3\text{N} + \text{H}_2 = 2/5\text{Fe}_8\text{N} + 2/3\text{NH}_3$	-4.82	10.38	507.1	exergonic
Fe-R061	$3/2\text{Fe}_4\text{N} + \text{H}_2 = 2\text{Fe}_3\text{H} + 3/4\text{N}_2$	-5.33	-	-	-
Fe-R062	$1/2\text{Fe}_4\text{N} + \text{H}_2 = 2\text{FeH} + 1/4\text{N}_2$	-4.2	-20.4	-	endergonic
Fe-R063	$1/6\text{Fe}_4\text{N} + \text{H}_2 = 2/3\text{FeH}_3 + 1/12\text{N}_2$	-0.81	40.19	-	endergonic
Fe-R064	$1/8\text{Fe}_4\text{N} + \text{H}_2 = 1/2\text{FeH}_4 + 1/16\text{N}_2$	0.89	-	-	-
Fe-R065	$2/3\text{Fe}_4\text{N} + \text{H}_2 = 8/3\text{Fe} + 2/3\text{NH}_3$	-5.9	-23.21	365.4	exergonic
Fe-R066	$6/13\text{Fe}_4\text{N} + \text{H}_2 = 8/13\text{Fe}_3\text{H} + 6/13\text{NH}_3$	-5.33	-	-	-
Fe-R067	$2/7\text{Fe}_4\text{N} + \text{H}_2 = 8/7\text{FeH} + 2/7\text{NH}_3$	-4.2	-24.77	36.4	exergonic
Fe-R068	$2/15\text{Fe}_4\text{N} + \text{H}_2 = 8/15\text{FeH}_3 + 2/15\text{NH}_3$	-0.81	26.03	-	endergonic
Fe-R069	$2/19\text{Fe}_4\text{N} + \text{H}_2 = 8/19\text{FeH}_4 + 2/19\text{NH}_3$	0.89	-	-	-
Fe-R070	$4/3\text{Fe}_4\text{N} + \text{H}_2 = 2/3\text{Fe}_8\text{N} + 2/3\text{NH}_3$	-2.95	-55.75	365.2	exergonic
Fe-R071	$3/4\text{Fe}_8\text{N} + \text{H}_2 = 2\text{Fe}_3\text{H} + 3/8\text{N}_2$	-2.46	-	-	-
Fe-R072	$1/4\text{Fe}_8\text{N} + \text{H}_2 = 2\text{FeH} + 1/8\text{N}_2$	-1.29	-10.97	-	endergonic
Fe-R073	$1/12\text{Fe}_8\text{N} + \text{H}_2 = 2/3\text{FeH}_3 + 1/24\text{N}_2$	2.21	43.34	-	endergonic
Fe-R074	$1/16\text{Fe}_8\text{N} + \text{H}_2 = 1/2\text{FeH}_4 + 1/32\text{N}_2$	3.96	-	-	-
Fe-R075	$2/3\text{Fe}_8\text{N} + \text{H}_2 = 16/3\text{Fe} + 2/3\text{NH}_3$	-3.04	9.34	363.9	exergonic
Fe-R076	$6/17\text{Fe}_8\text{N} + \text{H}_2 = 16/17\text{Fe}_3\text{H} + 6/17\text{NH}_3$	-2.46	-	-	-
Fe-R077	$2/11\text{Fe}_8\text{N} + \text{H}_2 = 16/11\text{FeH} + 2/11\text{NH}_3$	-1.29	-16.32	-	endergonic
Fe-R078	$2/27\text{Fe}_8\text{N} + \text{H}_2 = 16/27\text{FeH}_3 + 2/27\text{NH}_3$	2.21	35.12	-	endergonic
Fe-R079	$2/35\text{Fe}_8\text{N} + \text{H}_2 = 16/35\text{FeH}_4 + 2/35\text{NH}_3$	3.96	-	-	-
Fe-R080	$3/4\text{Fe}_8\text{N}_3 + \text{H}_2 = 2\text{Fe}_3\text{H} + 9/8\text{N}_2$	-8.05	-	-	-
Fe-R081	$1/4\text{Fe}_8\text{N}_3 + \text{H}_2 = 2\text{FeH} + 3/8\text{N}_2$	-6.95	15.03	-	endergonic
Fe-R082	$1/12\text{Fe}_8\text{N}_3 + \text{H}_2 = 2/3\text{FeH}_3 + 1/8\text{N}_2$	-3.65	52	-	endergonic
Fe-R083	$1/16\text{Fe}_8\text{N}_3 + \text{H}_2 = 1/2\text{FeH}_4 + 3/32\text{N}_2$	-2	-	-	-
Fe-R084	$2/9\text{Fe}_8\text{N}_3 + \text{H}_2 = 16/9\text{Fe} + 2/3\text{NH}_3$	-8.6	5.82	-	endergonic
Fe-R085	$6/35\text{Fe}_8\text{N}_3 + \text{H}_2 = 16/35\text{Fe}_3\text{H} + 18/35\text{NH}_3$	-8.05	-	-	-
Fe-R086	$2/17\text{Fe}_8\text{N}_3 + \text{H}_2 = 16/17\text{FeH} + 6/17\text{NH}_3$	-6.95	-9.13	-	endergonic
Fe-R087	$2/33\text{Fe}_8\text{N}_3 + \text{H}_2 = 16/33\text{FeH}_3 + 2/11\text{NH}_3$	-3.65	29.47	-	endergonic
Fe-R088	$2/41\text{Fe}_8\text{N}_3 + \text{H}_2 = 16/41\text{FeH}_4 + 6/41\text{NH}_3$	-2	-	-	-
Fe-R089	$2\text{Fe}_8\text{N}_3 + \text{H}_2 = 16/3\text{Fe}_3\text{N} + 2/3\text{NH}_3$	-0.96	-27.52	-	endergonic
Fe-R090	$2/3\text{Fe}_8\text{N}_3 + \text{H}_2 = 4/3\text{Fe}_4\text{N} + 2/3\text{NH}_3$	-2.87	63.88	751.2	exergonic
Fe-R091	$1/3\text{Fe}_8\text{N}_3 + \text{H}_2 = 1/3\text{Fe}_8\text{N} + 2/3\text{NH}_3$	-5.73	4.06	-	endergonic
Fe-R092	$\text{FeH} + \text{H}_2 = \text{FeH}_3$	3.55	70.49	-	endergonic
Fe-R093	$2/3\text{FeH} + \text{H}_2 = 2/3\text{FeH}_4$	5.32	-	-	-
Fe-R094	$2\text{FeH}_3 + \text{H}_2 = 2\text{FeH}_4$	1.71	-	-	-

Fe-R095	$6\text{FeN} + \text{H}_2 = 2\text{Fe}_3\text{H} + 3\text{N}_2$	-19.57	-	-	-
Fe-R096	$2\text{FeN} + \text{H}_2 = 2\text{FeH} + \text{N}_2$	-18.61	95.13	-	endergonic
Fe-R097	$2/3\text{FeN} + \text{H}_2 = 2/3\text{FeH}_3 + 1/3\text{N}_2$	-15.72	78.7	-	endergonic
Fe-R098	$1/2\text{FeN} + \text{H}_2 = 1/2\text{FeH}_4 + 1/4\text{N}_2$	-14.28	-	-	-
Fe-R099	$2/3\text{FeN} + \text{H}_2 = 2/3\text{Fe} + 2/3\text{NH}_3$	-20.05	9.76	-	endergonic
Fe-R100	$3/5\text{FeN} + \text{H}_2 = 1/5\text{Fe}_3\text{H} + 3/5\text{NH}_3$	-19.57	-	-	-
Fe-R101	$1/2\text{FeN} + \text{H}_2 = 1/2\text{FeH} + 1/2\text{NH}_3$	-18.61	0.83	-	endergonic
Fe-R102	$1/3\text{FeN} + \text{H}_2 = 1/3\text{FeH}_3 + 1/3\text{NH}_3$	-15.72	24.05	-	endergonic
Fe-R103	$2/7\text{FeN} + \text{H}_2 = 2/7\text{FeH}_4 + 2/7\text{NH}_3$	-14.28	-	-	-
Fe-R104	$8/7\text{FeN} + \text{H}_2 = 2/21\text{Fe}_{12}\text{N}_5 + 2/3\text{NH}_3$	-11.7	-	-	-
Fe-R105	$16/13\text{FeN} + \text{H}_2 = 2/39\text{Fe}_{24}\text{N}_{11} + 2/3\text{NH}_3$	-10.86	-	-	-
Fe-R106	$4/3\text{FeN} + \text{H}_2 = 2/3\text{Fe}_2\text{N} + 2/3\text{NH}_3$	-10.03	47.61	-	endergonic
Fe-R107	$\text{FeN} + \text{H}_2 = 1/3\text{Fe}_3\text{N} + 2/3\text{NH}_3$	-13.37	9.65	-	endergonic
Fe-R108	$8/9\text{FeN} + \text{H}_2 = 2/9\text{Fe}_4\text{N} + 2/3\text{NH}_3$	-15.04	20.75	-	endergonic
Fe-R109	$16/21\text{FeN} + \text{H}_2 = 2/21\text{Fe}_8\text{N}_3 + 2/3\text{NH}_3$	-17.55	9.82	-	endergonic
Fe-R110	$16/15\text{FeN} + \text{H}_2 = 2/15\text{Fe}_8\text{N}_3 + 2/3\text{NH}_3$	-12.53	12.12	-	endergonic
Fe-R111	$6\text{FeN}_2 + \text{H}_2 = 2\text{Fe}_3\text{H} + 6\text{N}_2$	-33.01	-	-	-
Fe-R112	$2\text{FeN}_2 + \text{H}_2 = 2\text{FeH} + 2\text{N}_2$	-32.2	-	-	-
Fe-R113	$2/3\text{FeN}_2 + \text{H}_2 = 2/3\text{FeH}_3 + 2/3\text{N}_2$	-29.8	-	-	-
Fe-R114	$1/2\text{FeN}_2 + \text{H}_2 = 1/2\text{FeH}_4 + 1/2\text{N}_2$	-28.6	-	-	-
Fe-R115	$1/3\text{FeN}_2 + \text{H}_2 = 1/3\text{Fe} + 2/3\text{NH}_3$	-33.41	-	-	-
Fe-R116	$6/19\text{FeN}_2 + \text{H}_2 = 2/19\text{Fe}_3\text{H} + 12/19\text{NH}_3$	-33.01	-	-	-
Fe-R117	$2/7\text{FeN}_2 + \text{H}_2 = 2/7\text{FeH} + 4/7\text{NH}_3$	-32.2	-	-	-
Fe-R118	$2/9\text{FeN}_2 + \text{H}_2 = 2/9\text{FeH}_3 + 4/9\text{NH}_3$	-29.8	-	-	-
Fe-R119	$1/5\text{FeN}_2 + \text{H}_2 = 1/5\text{FeH}_4 + 2/5\text{NH}_3$	-28.6	-	-	-
Fe-R120	$8/19\text{FeN}_2 + \text{H}_2 = 2/57\text{Fe}_{12}\text{N}_5 + 2/3\text{NH}_3$	-26.45	-	-	-
Fe-R121	$16/37\text{FeN}_2 + \text{H}_2 = 2/111\text{Fe}_{24}\text{N}_{11} + 2/3\text{NH}_3$	-25.75	-	-	-
Fe-R122	$4/9\text{FeN}_2 + \text{H}_2 = 2/9\text{Fe}_2\text{N} + 2/3\text{NH}_3$	-25.05	-	-	-
Fe-R123	$2/5\text{FeN}_2 + \text{H}_2 = 2/15\text{Fe}_3\text{N} + 2/3\text{NH}_3$	-27.84	-	-	-
Fe-R124	$8/21\text{FeN}_2 + \text{H}_2 = 2/21\text{Fe}_4\text{N} + 2/3\text{NH}_3$	-29.23	-	-	-
Fe-R125	$16/45\text{FeN}_2 + \text{H}_2 = 2/45\text{Fe}_8\text{N}_3 + 2/3\text{NH}_3$	-31.32	-	-	-
Fe-R126	$16/39\text{FeN}_2 + \text{H}_2 = 2/39\text{Fe}_8\text{N}_3 + 2/3\text{NH}_3$	-27.14	-	-	-
Fe-R127	$2/3\text{FeN}_2 + \text{H}_2 = 2/3\text{FeN} + 2/3\text{NH}_3$	-16.7	-	-	-
Fe-R128	$24/5\text{Fe} + \text{N}_2 = 2/5\text{Fe}_{12}\text{N}_5$	10.45	-	-	-
Fe-R129	$48/11\text{Fe} + \text{N}_2 = 2/11\text{Fe}_{24}\text{N}_{11}$	11.5	-	-	-
Fe-R130	$4\text{Fe} + \text{N}_2 = 2\text{Fe}_2\text{N}$	12.54	-7.53	-	endergonic
Fe-R131	$6\text{Fe} + \text{N}_2 = 2\text{Fe}_3\text{N}$	8.36	-121.76	218.7	exergonic
Fe-R132	$8\text{Fe} + \text{N}_2 = 2\text{Fe}_4\text{N}$	6.27	-22.18	-	endergonic
Fe-R133	$16\text{Fe} + \text{N}_2 = 2\text{Fe}_8\text{N}$	3.14	-119.82	218.2	exergonic
Fe-R134	$16/3\text{Fe} + \text{N}_2 = 2/3\text{Fe}_8\text{N}_3$	9.41	-109.26	297.7	exergonic
Fe-R135	$2\text{Fe} + \text{N}_2 = 2\text{FeN}$	25.08	-121.07	450.3	exergonic
Fe-R136	$\text{Fe} + \text{N}_2 = \text{FeN}_2$	50.16	-	-	-
Fe-R137	$4\text{Fe}_{12}\text{N}_5 + \text{N}_2 = 2\text{Fe}_{24}\text{N}_{11}$	0.95	-	-	-
Fe-R138	$2\text{Fe}_{12}\text{N}_5 + \text{N}_2 = 12\text{Fe}_2\text{N}$	1.89	-	-	-
Fe-R139	$2/7\text{Fe}_{12}\text{N}_5 + \text{N}_2 = 24/7\text{FeN}$	13.25	-	-	-
Fe-R140	$2/19\text{Fe}_{12}\text{N}_5 + \text{N}_2 = 24/19\text{FeN}_2$	35.96	-	-	-
Fe-R141	$2\text{Fe}_{24}\text{N}_{11} + \text{N}_2 = 24\text{Fe}_2\text{N}$	0.94	-	-	-
Fe-R142	$2/13\text{Fe}_{24}\text{N}_{11} + \text{N}_2 = 48/13\text{FeN}$	12.19	-	-	-
Fe-R143	$2/37\text{Fe}_{24}\text{N}_{11} + \text{N}_2 = 48/37\text{FeN}_2$	34.68	-	-	-

Fe-R144	$2\text{Fe}_2\text{N} + \text{N}_2 = 4\text{FeN}$	11.14	-234.62	713.9	exergonic
Fe-R145	$2/3\text{Fe}_2\text{N} + \text{N}_2 = 4/3\text{FeN}_2$	33.43	-	-	-
Fe-R146	$8/5\text{Fe}_3\text{H} + \text{N}_2 = 2/5\text{Fe}_{12}\text{N}_5 + 4/5\text{H}_2$	9.79	-	-	-
Fe-R147	$16/11\text{Fe}_3\text{H} + \text{N}_2 = 2/11\text{Fe}_{24}\text{N}_{11} + 8/11\text{H}_2$	10.83	-	-	-
Fe-R148	$4/3\text{Fe}_3\text{H} + \text{N}_2 = 2\text{Fe}_2\text{N} + 2/3\text{H}_2$	11.87	-	-	-
Fe-R149	$2\text{Fe}_3\text{H} + \text{N}_2 = 2\text{Fe}_3\text{N} + \text{H}_2$	7.71	-	-	-
Fe-R150	$8/3\text{Fe}_3\text{H} + \text{N}_2 = 2\text{Fe}_4\text{N} + 4/3\text{H}_2$	5.63	-	-	-
Fe-R151	$16/3\text{Fe}_3\text{H} + \text{N}_2 = 2\text{Fe}_8\text{N} + 8/3\text{H}_2$	2.52	-	-	-
Fe-R152	$16/9\text{Fe}_3\text{H} + \text{N}_2 = 2/3\text{Fe}_8\text{N}_3 + 8/9\text{H}_2$	8.75	-	-	-
Fe-R153	$2/3\text{Fe}_3\text{H} + \text{N}_2 = 2\text{FeN} + 1/3\text{H}_2$	24.33	-	-	-
Fe-R154	$1/3\text{Fe}_3\text{H} + \text{N}_2 = \text{FeN}_2 + 1/6\text{H}_2$	49.27	-	-	-
Fe-R155	$6\text{Fe}_3\text{H} + \text{N}_2 = 18\text{Fe} + 2\text{NH}_3$	-0.6	-	-	-
Fe-R156	$24/19\text{Fe}_3\text{H} + \text{N}_2 = 6/19\text{Fe}_{12}\text{N}_5 + 8/19\text{NH}_3$	9.79	-	-	-
Fe-R157	$48/41\text{Fe}_3\text{H} + \text{N}_2 = 6/41\text{Fe}_{24}\text{N}_{11} + 16/41\text{NH}_3$	10.83	-	-	-
Fe-R158	$12/11\text{Fe}_3\text{H} + \text{N}_2 = 18/11\text{Fe}_2\text{N} + 4/11\text{NH}_3$	11.87	-	-	-
Fe-R159	$3/2\text{Fe}_3\text{H} + \text{N}_2 = 3/2\text{Fe}_3\text{N} + 1/2\text{NH}_3$	7.71	-	-	-
Fe-R160	$24/13\text{Fe}_3\text{H} + \text{N}_2 = 18/13\text{Fe}_4\text{N} + 8/13\text{NH}_3$	5.63	-	-	-
Fe-R161	$48/17\text{Fe}_3\text{H} + \text{N}_2 = 18/17\text{Fe}_8\text{N} + 16/17\text{NH}_3$	2.52	-	-	-
Fe-R162	$48/35\text{Fe}_3\text{H} + \text{N}_2 = 18/35\text{Fe}_8\text{N}_3 + 16/35\text{NH}_3$	8.75	-	-	-
Fe-R163	$3/5\text{Fe}_3\text{H} + \text{N}_2 = 9/5\text{FeN} + 1/5\text{NH}_3$	24.33	-	-	-
Fe-R164	$6/19\text{Fe}_3\text{H} + \text{N}_2 = 18/19\text{FeN}_2 + 2/19\text{NH}_3$	49.27	-	-	-
Fe-R165	$8\text{Fe}_3\text{N} + \text{N}_2 = 2\text{Fe}_{12}\text{N}_5$	1.93	-	-	-
Fe-R166	$16/3\text{Fe}_3\text{N} + \text{N}_2 = 2/3\text{Fe}_{24}\text{N}_{11}$	2.89	-	-	-
Fe-R167	$4\text{Fe}_3\text{N} + \text{N}_2 = 6\text{Fe}_2\text{N}$	3.86	220.92	687.5	exergonic
Fe-R168	$16\text{Fe}_3\text{N} + \text{N}_2 = 6\text{Fe}_8\text{N}_3$	0.96	-9.24	-	exergonic
Fe-R169	$\text{Fe}_3\text{N} + \text{N}_2 = 3\text{FeN}$	15.43	-120.73	731.6	exergonic
Fe-R170	$2/5\text{Fe}_3\text{N} + \text{N}_2 = 6/5\text{FeN}_2$	38.58	-	-	-
Fe-R171	$3\text{Fe}_4\text{N} + \text{N}_2 = \text{Fe}_{12}\text{N}_5$	3.93	-	-	-
Fe-R172	$12/5\text{Fe}_4\text{N} + \text{N}_2 = 2/5\text{Fe}_{24}\text{N}_{11}$	4.92	-	-	-
Fe-R173	$2\text{Fe}_4\text{N} + \text{N}_2 = 4\text{Fe}_2\text{N}$	5.9	7.11	-	endergonic
Fe-R174	$6\text{Fe}_4\text{N} + \text{N}_2 = 8\text{Fe}_3\text{N}$	1.97	-420.51	323.2	exergonic
Fe-R175	$4\text{Fe}_4\text{N} + \text{N}_2 = 2\text{Fe}_8\text{N}_3$	2.95	-283.42	466.7	exergonic
Fe-R176	$2/3\text{Fe}_4\text{N} + \text{N}_2 = 8/3\text{FeN}$	17.7	-154.04	536.2	exergonic
Fe-R177	$2/7\text{Fe}_4\text{N} + \text{N}_2 = 8/7\text{FeN}_2$	41.3	-	-	-
Fe-R178	$6/7\text{Fe}_8\text{N} + \text{N}_2 = 4/7\text{Fe}_{12}\text{N}_5$	7.09	-	-	-
Fe-R179	$3/4\text{Fe}_8\text{N} + \text{N}_2 = 1/4\text{Fe}_{24}\text{N}_{11}$	8.11	-	-	-
Fe-R180	$2/3\text{Fe}_8\text{N} + \text{N}_2 = 8/3\text{Fe}_2\text{N}$	9.12	29.9	-	endergonic
Fe-R181	$6/5\text{Fe}_8\text{N} + \text{N}_2 = 16/5\text{Fe}_3\text{N}$	5.07	-122.92	219.1	exergonic
Fe-R182	$2\text{Fe}_8\text{N} + \text{N}_2 = 4\text{Fe}_4\text{N}$	3.04	75.47	669.5	exergonic
Fe-R183	$\text{Fe}_8\text{N} + \text{N}_2 = \text{Fe}_8\text{N}_3$	6.08	-103.97	366.5	exergonic
Fe-R184	$2/7\text{Fe}_8\text{N} + \text{N}_2 = 16/7\text{FeN}$	21.28	-121.25	515.3	exergonic
Fe-R185	$2/15\text{Fe}_8\text{N} + \text{N}_2 = 16/15\text{FeN}_2$	45.6	-	-	-
Fe-R186	$6\text{Fe}_8\text{N}_3 + \text{N}_2 = 4\text{Fe}_{12}\text{N}_5$	0.96	-	-	-
Fe-R187	$3\text{Fe}_8\text{N}_3 + \text{N}_2 = \text{Fe}_{24}\text{N}_{11}$	1.91	-	-	-
Fe-R188	$2\text{Fe}_8\text{N}_3 + \text{N}_2 = 8\text{Fe}_2\text{N}$	2.87	297.64	-	endergonic
Fe-R189	$2/5\text{Fe}_8\text{N}_3 + \text{N}_2 = 16/5\text{FeN}$	14.33	-128.17	580.2	exergonic
Fe-R190	$2/13\text{Fe}_8\text{N}_3 + \text{N}_2 = 16/13\text{FeN}_2$	37.25	-	-	-
Fe-R191	$24/5\text{FeH} + \text{N}_2 = 2/5\text{Fe}_{12}\text{N}_5 + 12/5\text{H}_2$	8.49	-	-	-
Fe-R192	$48/11\text{FeH} + \text{N}_2 = 2/11\text{Fe}_{24}\text{N}_{11} + 24/11\text{H}_2$	9.52	-	-	-

Fe-R193	$4\text{FeH} + \text{N}_2 = 2\text{Fe}_2\text{N} + 2\text{H}_2$	10.55	44.36	61.6	exergonic
Fe-R194	$6\text{FeH} + \text{N}_2 = 2\text{Fe}_3\text{N} + 3\text{H}_2$	6.44	-43.93	-	exergonic
Fe-R195	$8\text{FeH} + \text{N}_2 = 2\text{Fe}_4\text{N} + 4\text{H}_2$	4.39	81.6	-	exergonic
Fe-R196	$16\text{FeH} + \text{N}_2 = 2\text{Fe}_8\text{N} + 8\text{H}_2$	1.31	87.73	-	exergonic
Fe-R197	$16/3\text{FeH} + \text{N}_2 = 2/3\text{Fe}_8\text{N}_3 + 8/3\text{H}_2$	7.47	-40.07	-	exergonic
Fe-R198	$2\text{FeH} + \text{N}_2 = 2\text{FeN} + \text{H}_2$	22.86	-95.13	-	exergonic
Fe-R199	$\text{FeH} + \text{N}_2 = \text{FeN}_2 + 1/2\text{H}_2$	47.5	-	-	-
Fe-R200	$6\text{FeH} + \text{N}_2 = 6\text{Fe} + 2\text{NH}_3$	-1.77	-13.96	-	exergonic
Fe-R201	$9\text{FeH} + \text{N}_2 = 3\text{Fe}_3\text{H} + 2\text{NH}_3$	-1.18	-	-	-
Fe-R202	$8/3\text{FeH} + \text{N}_2 = 2/9\text{Fe}_{12}\text{N}_5 + 8/9\text{NH}_3$	8.49	-	-	-
Fe-R203	$48/19\text{FeH} + \text{N}_2 = 2/19\text{Fe}_{24}\text{N}_{11} + 16/19\text{NH}_3$	9.52	-	-	-
Fe-R204	$12/5\text{FeH} + \text{N}_2 = 6/5\text{Fe}_2\text{N} + 4/5\text{NH}_3$	10.55	-10.1	-	exergonic
Fe-R205	$3\text{FeH} + \text{N}_2 = \text{Fe}_3\text{N} + \text{NH}_3$	6.44	-67.86	732.7	exergonic
Fe-R206	$24/7\text{FeH} + \text{N}_2 = 6/7\text{Fe}_4\text{N} + 8/7\text{NH}_3$	4.39	-17.48	-	exergonic
Fe-R207	$48/11\text{FeH} + \text{N}_2 = 6/11\text{Fe}_8\text{N} + 16/11\text{NH}_3$	1.31	-42.83	-	exergonic
Fe-R208	$48/17\text{FeH} + \text{N}_2 = 6/17\text{Fe}_8\text{N}_3 + 16/17\text{NH}_3$	7.47	-64.41	-	exergonic
Fe-R209	$3/2\text{FeH} + \text{N}_2 = 3/2\text{FeN} + 1/2\text{NH}_3$	22.86	-94.3	732.1	exergonic
Fe-R210	$6/7\text{FeH} + \text{N}_2 = 6/7\text{FeN}_2 + 2/7\text{NH}_3$	47.5	-	-	-
Fe-R211	$24/5\text{FeH}_3 + \text{N}_2 = 2/5\text{Fe}_{12}\text{N}_5 + 36/5\text{H}_2$	4.78	-	-	-
Fe-R212	$48/11\text{FeH}_3 + \text{N}_2 = 2/11\text{Fe}_{24}\text{N}_{11} + 72/11\text{H}_2$	5.77	-	-	-
Fe-R213	$4\text{FeH}_3 + \text{N}_2 = 2\text{Fe}_2\text{N} + 6\text{H}_2$	6.76	-237.59	-	exergonic
Fe-R214	$6\text{FeH}_3 + \text{N}_2 = 2\text{Fe}_3\text{N} + 9\text{H}_2$	2.79	-466.84	-	exergonic
Fe-R215	$8\text{FeH}_3 + \text{N}_2 = 2\text{Fe}_4\text{N} + 12\text{H}_2$	0.81	-482.29	-	exergonic
Fe-R216	$16\text{FeH}_3 + \text{N}_2 = 2\text{Fe}_8\text{N} + 24\text{H}_2$	-2.16	-1040.04	-	exergonic
Fe-R217	$16/3\text{FeH}_3 + \text{N}_2 = 2/3\text{Fe}_8\text{N}_3 + 8\text{H}_2$	3.79	-416	-	exergonic
Fe-R218	$2\text{FeH}_3 + \text{N}_2 = 2\text{FeN} + 3\text{H}_2$	18.66	-236.1	-	exergonic
Fe-R219	$\text{FeH}_3 + \text{N}_2 = \text{FeN}_2 + 3/2\text{H}_2$	42.45	-	-	-
Fe-R220	$2\text{FeH}_3 + \text{N}_2 = 2\text{Fe} + 2\text{NH}_3$	-5.14	-206.82	-	exergonic
Fe-R221	$9/4\text{FeH}_3 + \text{N}_2 = 3/4\text{Fe}_3\text{H} + 2\text{NH}_3$	-4.57	-	-	-
Fe-R222	$3\text{FeH}_3 + \text{N}_2 = 3\text{FeH} + 2\text{NH}_3$	-3.42	-303.25	-	exergonic
Fe-R223	$24/17\text{FeH}_3 + \text{N}_2 = 2/17\text{Fe}_{12}\text{N}_5 + 24/17\text{NH}_3$	4.78	-	-	-
Fe-R224	$48/35\text{FeH}_3 + \text{N}_2 = 2/35\text{Fe}_{24}\text{N}_{11} + 48/35\text{NH}_3$	5.77	-	-	-
Fe-R225	$4/3\text{FeH}_3 + \text{N}_2 = 2/3\text{Fe}_2\text{N} + 4/3\text{NH}_3$	6.76	-140.39	-	exergonic
Fe-R226	$3/2\text{FeH}_3 + \text{N}_2 = 1/2\text{Fe}_3\text{N} + 3/2\text{NH}_3$	2.79	-185.55	-	exergonic
Fe-R227	$8/5\text{FeH}_3 + \text{N}_2 = 2/5\text{Fe}_4\text{N} + 8/5\text{NH}_3$	0.81	-169.89	-	exergonic
Fe-R228	$16/9\text{FeH}_3 + \text{N}_2 = 2/9\text{Fe}_8\text{N} + 16/9\text{NH}_3$	-2.16	-197.15	-	exergonic
Fe-R229	$16/11\text{FeH}_3 + \text{N}_2 = 2/11\text{Fe}_8\text{N}_3 + 16/11\text{NH}_3$	3.79	-180.21	-	exergonic
Fe-R230	$\text{FeH}_3 + \text{N}_2 = \text{FeN} + \text{NH}_3$	18.66	-163.95	-	exergonic
Fe-R231	$2/3\text{FeH}_3 + \text{N}_2 = 2/3\text{FeN}_2 + 2/3\text{NH}_3$	42.45	-	-	-
Fe-R232	$24/5\text{FeH}_4 + \text{N}_2 = 2/5\text{Fe}_{12}\text{N}_5 + 48/5\text{H}_2$	3.01	-	-	-
Fe-R233	$48/11\text{FeH}_4 + \text{N}_2 = 2/11\text{Fe}_{24}\text{N}_{11} + 96/11\text{H}_2$	3.99	-	-	-
Fe-R234	$4\text{FeH}_4 + \text{N}_2 = 2\text{Fe}_2\text{N} + 8\text{H}_2$	4.96	-	-	-
Fe-R235	$6\text{FeH}_4 + \text{N}_2 = 2\text{Fe}_3\text{N} + 12\text{H}_2$	1.06	-	-	-
Fe-R236	$8\text{FeH}_4 + \text{N}_2 = 2\text{Fe}_4\text{N} + 16\text{H}_2$	-0.89	-	-	-
Fe-R237	$16\text{FeH}_4 + \text{N}_2 = 2\text{Fe}_8\text{N} + 32\text{H}_2$	-3.81	-	-	-
Fe-R238	$16/3\text{FeH}_4 + \text{N}_2 = 2/3\text{Fe}_8\text{N}_3 + 32/3\text{H}_2$	2.04	-	-	-
Fe-R239	$2\text{FeH}_4 + \text{N}_2 = 2\text{FeN} + 4\text{H}_2$	16.66	-	-	-
Fe-R240	$\text{FeH}_4 + \text{N}_2 = \text{FeN}_2 + 2\text{H}_2$	40.05	-	-	-
Fe-R241	$3/2\text{FeH}_4 + \text{N}_2 = 3/2\text{Fe} + 2\text{NH}_3$	-6.73	-	-	-

Fe-R242	$18/11\text{FeH}_4 + \text{N}_2 = 6/11\text{Fe}_3\text{H} + 2\text{NH}_3$	-6.17	-	-	-
Fe-R243	$2\text{FeH}_4 + \text{N}_2 = 2\text{FeH} + 2\text{NH}_3$	-5.05	-	-	-
Fe-R244	$6\text{FeH}_4 + \text{N}_2 = 6\text{FeH}_3 + 2\text{NH}_3$	-1.68	-	-	-
Fe-R245	$8/7\text{FeH}_4 + \text{N}_2 = 2/21\text{Fe}_{12}\text{N}_5 + 32/21\text{NH}_3$	3.01	-	-	-
Fe-R246	$48/43\text{FeH}_4 + \text{N}_2 = 2/43\text{Fe}_{24}\text{N}_{11} + 64/43\text{NH}_3$	3.99	-	-	-
Fe-R247	$12/11\text{FeH}_4 + \text{N}_2 = 6/11\text{Fe}_2\text{N} + 16/11\text{NH}_3$	4.96	-	-	-
Fe-R248	$6/5\text{FeH}_4 + \text{N}_2 = 2/5\text{Fe}_3\text{N} + 8/5\text{NH}_3$	1.06	-	-	-
Fe-R249	$24/19\text{FeH}_4 + \text{N}_2 = 6/19\text{Fe}_4\text{N} + 32/19\text{NH}_3$	-0.89	-	-	-
Fe-R250	$48/35\text{FeH}_4 + \text{N}_2 = 6/35\text{Fe}_8\text{N} + 64/35\text{NH}_3$	-3.81	-	-	-
Fe-R251	$48/41\text{FeH}_4 + \text{N}_2 = 6/41\text{Fe}_8\text{N}_3 + 64/41\text{NH}_3$	2.04	-	-	-
Fe-R252	$6/7\text{FeH}_4 + \text{N}_2 = 6/7\text{FeN} + 8/7\text{NH}_3$	16.66	-	-	-
Fe-R253	$3/5\text{FeH}_4 + \text{N}_2 = 3/5\text{FeN}_2 + 4/5\text{NH}_3$	40.05	-	-	-
Fe-R254	$2\text{FeN} + \text{N}_2 = 2\text{FeN}_2$	20.05	-	-	-

Table S20: The Li-based system

ID	Reaction	dm_stoich [%]	h298 [kJ/mol]	T_eq [°C]	Type
Li-R001	$2\text{Li} + \text{H}_2 = 2\text{LiH}$	14.52	-181.08	-	exergonic
Li-R002	$2\text{Li}(\text{H}_3\text{N})_4 + \text{H}_2 = 2\text{LiH} + 8\text{NH}_3$	-89.41	-	-	-
Li-R003	$1/3\text{Li}_{15}\text{H}_9\text{N}_8 + \text{H}_2 = 5\text{LiH} + 4/3\text{N}_2$	-47.07	-	-	-
Li-R004	$2/15\text{Li}_{15}\text{H}_9\text{N}_8 + \text{H}_2 = 2\text{Li} + 16/15\text{NH}_3$	-53.78	-	-	-
Li-R005	$1/15\text{Li}_{15}\text{H}_9\text{N}_8 + \text{H}_2 = \text{LiH} + 8/15\text{NH}_3$	-47.07	-	-	-
Li-R006	$4/15\text{Li}_{15}\text{H}_9\text{N}_8 + \text{H}_2 = \text{Li}_4\text{HN} + 17/15\text{NH}_3$	-28.78	-	-	-
Li-R007	$2\text{Li}_2\text{HN} + \text{H}_2 = 4\text{LiH} + \text{N}_2$	-44.99	-	-	-
Li-R008	$\text{Li}_2\text{HN} + \text{H}_2 = 2\text{Li} + \text{NH}_3$	-51.96	-	-	-
Li-R009	$1/2\text{Li}_2\text{HN} + \text{H}_2 = \text{LiH} + 1/2\text{NH}_3$	-44.99	-	-	-
Li-R010	$2\text{Li}_2\text{HN} + \text{H}_2 = \text{Li}_4\text{HN} + \text{NH}_3$	-25.98	-	-	-
Li-R011	$\text{Li}_2\text{N} + \text{H}_2 = 2\text{LiH} + 1/2\text{N}_2$	-43	-	-	-
Li-R012	$2\text{Li}_2\text{N} + \text{H}_2 = 2\text{Li}_2\text{HN}$	3.61	-	-	-
Li-R013	$4\text{Li}_2\text{N} + \text{H}_2 = 2\text{Li}_4\text{HN} + \text{N}_2$	-23.31	-	-	-
Li-R014	$2/3\text{Li}_2\text{N} + \text{H}_2 = 4/3\text{Li} + 2/3\text{NH}_3$	-50.23	-	-	-
Li-R015	$2/5\text{Li}_2\text{N} + \text{H}_2 = 4/5\text{LiH} + 2/5\text{NH}_3$	-43	-	-	-
Li-R016	$\text{Li}_2\text{N} + \text{H}_2 = 1/2\text{Li}_4\text{HN} + 1/2\text{NH}_3$	-23.31	-	-	-
Li-R017	$2\text{Li}_2\text{N} + \text{H}_2 = 4/3\text{Li}_3\text{N} + 2/3\text{NH}_3$	-16.74	-	-	-
Li-R018	$2\text{Li}_3(\text{HN})_2 + \text{H}_2 = 6\text{LiH} + 2\text{N}_2$	-53.11	-	-	-
Li-R019	$2\text{Li}_3(\text{HN})_2 + \text{H}_2 = 2\text{Li}_3\text{H}_3\text{N}_2$	1.98	-	-	-
Li-R020	$14\text{Li}_3(\text{HN})_2 + \text{H}_2 = 6\text{Li}_7\text{H}_5\text{N}_4 + 2\text{N}_2$	-7.59	-	-	-
Li-R021	$1/2\text{Li}_3(\text{HN})_2 + \text{H}_2 = 3/2\text{Li} + \text{NH}_3$	-59.06	-	-	-
Li-R022	$2/7\text{Li}_3(\text{HN})_2 + \text{H}_2 = 6/7\text{LiH} + 4/7\text{NH}_3$	-53.11	-	-	-
Li-R023	$2\text{Li}_3(\text{HN})_2 + \text{H}_2 = 2/5\text{Li}_{15}\text{H}_9\text{N}_8 + 4/5\text{NH}_3$	-11.41	-	-	-
Li-	$2\text{Li}_3(\text{HN})_2 + \text{H}_2 = 3\text{Li}_2\text{HN} + \text{NH}_3$	-14.76	-	-	-

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Li-R025	$4/5\text{Li}_3(\text{HN})_2 + \text{H}_2 = 3/5\text{Li}_4\text{HN} + \text{NH}_3$	-36.91	-	-	-
Li-R026	$2\text{Li}_3(\text{HN})_2 + \text{H}_2 = 6/7\text{Li}_7\text{H}_5\text{N}_4 + 4/7\text{NH}_3$	-7.59	-	-	-
Li-R027	$2\text{Li}_3(\text{HN})_2 + \text{H}_2 = 2\text{Li}_3\text{N} + 2\text{NH}_3$	-31.51	-	-	-
Li-R028	$2/3\text{Li}_3\text{H}_3\text{N}_2 + \text{H}_2 = 2\text{Li} + 4/3\text{NH}_3$	-59.85	-	-	-
Li-R029	$1/3\text{Li}_3\text{H}_3\text{N}_2 + \text{H}_2 = \text{LiH} + 2/3\text{NH}_3$	-54.02	-	-	-
Li-R030	$4/3\text{Li}_3\text{H}_3\text{N}_2 + \text{H}_2 = \text{Li}_4\text{HN} + 5/3\text{NH}_3$	-38.14	-	-	-
Li-R031	$2/3\text{Li}_3\text{N} + \text{H}_2 = 2\text{LiH} + 1/3\text{N}_2$	-31.54	-71.38	-	exergonic
Li-R032	$8/3\text{Li}_3\text{N} + \text{H}_2 = 2\text{Li}_4\text{HN} + 1/3\text{N}_2$	-7.88	-	-	-
Li-R033	$2/3\text{Li}_3\text{N} + \text{H}_2 = 2\text{Li} + 2/3\text{NH}_3$	-40.22	79.11	-	endergonic
Li-R034	$1/3\text{Li}_3\text{N} + \text{H}_2 = \text{LiH} + 1/3\text{NH}_3$	-31.54	-50.99	454.2	exergonic
Li-R035	$4/3\text{Li}_3\text{N} + \text{H}_2 = \text{Li}_4\text{HN} + 1/3\text{NH}_3$	-7.88	-	-	-
Li-R036	$2/3\text{Li}_3\text{N}_2 + \text{H}_2 = 2\text{LiH} + 2/3\text{N}_2$	-51.17	-	-	-
Li-R037	$10/9\text{Li}_3\text{N}_2 + \text{H}_2 = 2/9\text{Li}_{15}\text{H}_9\text{N}_8 + 2/9\text{N}_2$	-7.76	-	-	-
Li-R038	$4/3\text{Li}_3\text{N}_2 + \text{H}_2 = 2\text{Li}_2\text{HN} + 1/3\text{N}_2$	-11.25	-	-	-
Li-R039	$\text{Li}_3\text{N}_2 + \text{H}_2 = \text{Li}_3(\text{HN})_2$	4.13	-	-	-
Li-R040	$2/3\text{Li}_3\text{N}_2 + \text{H}_2 = 2/3\text{Li}_3\text{H}_3\text{N}_2$	6.19	-	-	-
Li-R041	$8/3\text{Li}_3\text{N}_2 + \text{H}_2 = 2\text{Li}_4\text{HN} + 5/3\text{N}_2$	-34.31	-	-	-
Li-R042	$14/15\text{Li}_3\text{N}_2 + \text{H}_2 = 2/5\text{Li}_7\text{H}_5\text{N}_4 + 2/15\text{N}_2$	-3.77	-	-	-
Li-R043	$1/3\text{Li}_3\text{N}_2 + \text{H}_2 = \text{Li} + 2/3\text{NH}_3$	-57.37	-	-	-
Li-R044	$2/9\text{Li}_3\text{N}_2 + \text{H}_2 = 2/3\text{LiH} + 4/9\text{NH}_3$	-51.17	-	-	-
Li-R045	$2/3\text{Li}_3\text{N}_2 + \text{H}_2 = 2/15\text{Li}_{15}\text{H}_9\text{N}_8 + 4/15\text{NH}_3$	-7.76	-	-	-
Li-R046	$2/3\text{Li}_3\text{N}_2 + \text{H}_2 = \text{Li}_2\text{HN} + 1/3\text{NH}_3$	-11.25	-	-	-
Li-R047	$4/9\text{Li}_3\text{N}_2 + \text{H}_2 = 1/3\text{Li}_4\text{HN} + 5/9\text{NH}_3$	-34.31	-	-	-
Li-R048	$2/3\text{Li}_3\text{N}_2 + \text{H}_2 = 2/7\text{Li}_7\text{H}_5\text{N}_4 + 4/21\text{NH}_3$	-3.77	-	-	-
Li-R049	$4/3\text{Li}_3\text{N}_2 + \text{H}_2 = 2\text{Li}_2\text{N} + 2/3\text{NH}_3$	-14.34	-	-	-
Li-R050	$2/3\text{Li}_3\text{N}_2 + \text{H}_2 = 2/3\text{Li}_3\text{N} + 2/3\text{NH}_3$	-28.68	-	-	-
Li-R051	$2/3\text{Li}_4\text{HN} + \text{H}_2 = 8/3\text{LiH} + 1/3\text{N}_2$	-25.68	-	-	-
Li-R052	$\text{Li}_4\text{HN} + \text{H}_2 = 4\text{Li} + \text{NH}_3$	-35.1	-	-	-
Li-R053	$1/3\text{Li}_4\text{HN} + \text{H}_2 = 4/3\text{LiH} + 1/3\text{NH}_3$	-25.68	-	-	-
Li-R054	$\text{Li}_7\text{H}_5\text{N}_4 + \text{H}_2 = 7\text{LiH} + 2\text{N}_2$	-49.26	-	-	-
Li-R055	$2/7\text{Li}_7\text{H}_5\text{N}_4 + \text{H}_2 = 2\text{Li} + 8/7\text{NH}_3$	-55.69	-	-	-
Li-R056	$1/7\text{Li}_7\text{H}_5\text{N}_4 + \text{H}_2 = \text{LiH} + 4/7\text{NH}_3$	-49.26	-	-	-
Li-R057	$4/7\text{Li}_7\text{H}_5\text{N}_4 + \text{H}_2 = \text{Li}_4\text{HN} + 9/7\text{NH}_3$	-31.73	-	-	-
Li-R058	$2\text{LiH}_2\text{N} + \text{H}_2 = 2\text{Li} + 2\text{NH}_3$	-69.78	364.01	-	endergonic
Li-R059	$\text{LiH}_2\text{N} + \text{H}_2 = \text{LiH} + \text{NH}_3$	-65.39	91.47	-	endergonic

Li-R060	$4\text{LiH}_2\text{N} + \text{H}_2 = \text{Li}_4\text{HN} + 3\text{NH}_3$	-53.43	-	-	-
Li-R061	$2\text{LiN} + \text{H}_2 = 2\text{LiH} + \text{N}_2$	-62.06	-	-	-
Li-R062	$10/3\text{LiN} + \text{H}_2 = 2/9\text{Li}_{15}\text{H}_9\text{N}_8 + 7/9\text{N}_2$	-28.32	-	-	-
Li-R063	$4\text{LiN} + \text{H}_2 = 2\text{Li}_2\text{HN} + \text{N}_2$	-31.03	-	-	-
Li-R064	$3\text{LiN} + \text{H}_2 = \text{Li}_3(\text{HN})_2 + 1/2\text{N}_2$	-19.08	-	-	-
Li-R065	$2\text{LiN} + \text{H}_2 = 2/3\text{Li}_3\text{H}_3\text{N}_2 + 1/3\text{N}_2$	-17.48	-	-	-
Li-R066	$8\text{LiN} + \text{H}_2 = 2\text{Li}_4\text{HN} + 3\text{N}_2$	-48.95	-	-	-
Li-R067	$14/5\text{LiN} + \text{H}_2 = 2/5\text{Li}_7\text{H}_5\text{N}_4 + 3/5\text{N}_2$	-25.22	-	-	-
Li-R068	$\text{LiN} + \text{H}_2 = \text{LiH}_2\text{N}$	9.62	-	-	-
Li-R069	$2/3\text{LiN} + \text{H}_2 = 2/3\text{Li} + 2/3\text{NH}_3$	-66.87	-	-	-
Li-R070	$1/2\text{LiN} + \text{H}_2 = 1/2\text{LiH} + 1/2\text{NH}_3$	-62.06	-	-	-
Li-R071	$\text{LiN} + \text{H}_2 = 1/15\text{Li}_{15}\text{H}_9\text{N}_8 + 7/15\text{NH}_3$	-28.32	-	-	-
Li-R072	$\text{LiN} + \text{H}_2 = 1/2\text{Li}_2\text{HN} + 1/2\text{NH}_3$	-31.03	-	-	-
Li-R073	$6/5\text{LiN} + \text{H}_2 = 2/5\text{Li}_3(\text{HN})_2 + 2/5\text{NH}_3$	-19.08	-	-	-
Li-R074	$\text{LiN} + \text{H}_2 = 1/3\text{Li}_3\text{H}_3\text{N}_2 + 1/3\text{NH}_3$	-17.48	-	-	-
Li-R075	$4/5\text{LiN} + \text{H}_2 = 1/5\text{Li}_4\text{HN} + 3/5\text{NH}_3$	-48.95	-	-	-
Li-R076	$\text{LiN} + \text{H}_2 = 1/7\text{Li}_7\text{H}_5\text{N}_4 + 3/7\text{NH}_3$	-25.22	-	-	-
Li-R077	$4/3\text{LiN} + \text{H}_2 = 2/3\text{Li}_2\text{N} + 2/3\text{NH}_3$	-33.43	-	-	-
Li-R078	$\text{LiN} + \text{H}_2 = 1/3\text{Li}_3\text{N} + 2/3\text{NH}_3$	-44.58	-	-	-
Li-R079	$2\text{LiN} + \text{H}_2 = 2/3\text{Li}_3\text{N}_2 + 2/3\text{NH}_3$	-22.29	-	-	-
Li-R080	$2\text{LiN}_3 + \text{H}_2 = 2\text{LiH} + 3\text{N}_2$	-83.77	-22.23	-	exergonic
Li-R081	$10/3\text{LiN}_3 + \text{H}_2 = 2/9\text{Li}_{15}\text{H}_9\text{N}_8 + 37/9\text{N}_2$	-69.33	-	-	-
Li-R082	$4\text{LiN}_3 + \text{H}_2 = 2\text{Li}_2\text{HN} + 5\text{N}_2$	-70.49	-	-	-
Li-R083	$3\text{LiN}_3 + \text{H}_2 = \text{Li}_3(\text{HN})_2 + 7/2\text{N}_2$	-65.38	-	-	-
Li-R084	$2\text{LiN}_3 + \text{H}_2 = 2/3\text{Li}_3\text{H}_3\text{N}_2 + 7/3\text{N}_2$	-64.69	-	-	-
Li-R085	$8\text{LiN}_3 + \text{H}_2 = 2\text{Li}_4\text{HN} + 11\text{N}_2$	-78.16	-	-	-
Li-R086	$14/5\text{LiN}_3 + \text{H}_2 = 2/5\text{Li}_7\text{H}_5\text{N}_4 + 17/5\text{N}_2$	-68.01	-	-	-
Li-R087	$\text{LiN}_3 + \text{H}_2 = \text{LiH}_2\text{N} + \text{N}_2$	-53.1	-148.48	-	exergonic
Li-R088	$2/9\text{LiN}_3 + \text{H}_2 = 2/9\text{Li} + 2/3\text{NH}_3$	-85.83	-12.95	371	exergonic
Li-R089	$1/5\text{LiN}_3 + \text{H}_2 = 1/5\text{LiH} + 3/5\text{NH}_3$	-83.77	-29.76	557.2	exergonic
Li-R090	$1/4\text{LiN}_3 + \text{H}_2 = 1/60\text{Li}_{15}\text{H}_9\text{N}_8 + 37/60\text{NH}_3$	-69.33	-	-	-
Li-R091	$1/4\text{LiN}_3 + \text{H}_2 = 1/8\text{Li}_2\text{HN} + 5/8\text{NH}_3$	-70.49	-	-	-
Li-R092	$6/23\text{LiN}_3 + \text{H}_2 = 2/23\text{Li}_3(\text{HN})_2 + 14/23\text{NH}_3$	-65.38	-	-	-
Li-R093	$1/4\text{LiN}_3 + \text{H}_2 = 1/12\text{Li}_3\text{H}_3\text{N}_2 + 7/12\text{NH}_3$	-64.69	-	-	-
Li-R094	$4/17\text{LiN}_3 + \text{H}_2 = 1/17\text{Li}_4\text{HN} + 11/17\text{NH}_3$	-78.16	-	-	-
Li-R095	$1/4\text{LiN}_3 + \text{H}_2 = 1/28\text{Li}_7\text{H}_5\text{N}_4 + 17/28\text{NH}_3$	-68.01	-	-	-



Li-R096	$1/4\text{LiN}_3 + \text{H}_2 = 1/4\text{LiH}_2\text{N} + 1/2\text{NH}_3$	-53.1	-60.07	-	exergonic
Li-R097	$4/15\text{LiN}_3 + \text{H}_2 = 2/15\text{Li}_2\text{N} + 2/3\text{NH}_3$	-71.52	-	-	-
Li-R098	$1/4\text{LiN}_3 + \text{H}_2 = 1/12\text{Li}_3\text{N} + 2/3\text{NH}_3$	-76.29	-24.45	608.4	exergonic
Li-R099	$2/7\text{LiN}_3 + \text{H}_2 = 2/21\text{Li}_3\text{N}_2 + 2/3\text{NH}_3$	-66.75	-	-	-
Li-R100	$1/3\text{LiN}_3 + \text{H}_2 = 1/3\text{LiN} + 2/3\text{NH}_3$	-57.22	-	-	-
Li-R101	$4\text{Li} + \text{N}_2 = 2\text{Li}_2\text{N}$	100.91	-	-	-
Li-R102	$6\text{Li} + \text{N}_2 = 2\text{Li}_3\text{N}$	67.28	-329.11	-	exergonic
Li-R103	$3\text{Li} + \text{N}_2 = \text{Li}_3\text{N}_2$	134.55	-	-	-
Li-R104	$2\text{Li} + \text{N}_2 = 2\text{LiN}$	201.83	-	-	-
Li-R105	$2/3\text{Li} + \text{N}_2 = 2/3\text{LiN}_3$	605.49	-52.95	82.9	exergonic
Li-R106	$6\text{Li}(\text{H}_3\text{N})_4 + \text{N}_2 = 2/5\text{Li}_{15}\text{H}_9\text{N}_8 + 114/5\text{NH}_3$	-80	-	-	-
Li-R107	$6\text{Li}(\text{H}_3\text{N})_4 + \text{N}_2 = 3\text{Li}_2\text{HN} + 23\text{NH}_3$	-80.75	-	-	-
Li-R108	$9/2\text{Li}(\text{H}_3\text{N})_4 + \text{N}_2 = 3/2\text{Li}_3(\text{HN})_2 + 17\text{NH}_3$	-77.42	-	-	-
Li-R109	$6\text{Li}(\text{H}_3\text{N})_4 + \text{N}_2 = 2\text{Li}_3\text{H}_3\text{N}_2 + 22\text{NH}_3$	-76.97	-	-	-
Li-R110	$12\text{Li}(\text{H}_3\text{N})_4 + \text{N}_2 = 3\text{Li}_4\text{HN} + 47\text{NH}_3$	-85.75	-	-	-
Li-R111	$6\text{Li}(\text{H}_3\text{N})_4 + \text{N}_2 = 6/7\text{Li}_7\text{H}_5\text{N}_4 + 158/7\text{NH}_3$	-79.13	-	-	-
Li-R112	$6\text{Li}(\text{H}_3\text{N})_4 + \text{N}_2 = 6\text{LiH}_2\text{N} + 20\text{NH}_3$	-69.41	-	-	-
Li-R113	$4\text{Li}(\text{H}_3\text{N})_4 + \text{N}_2 = 2\text{Li}_2\text{N} + 16\text{NH}_3$	-81.42	-	-	-
Li-R114	$6\text{Li}(\text{H}_3\text{N})_4 + \text{N}_2 = 2\text{Li}_3\text{N} + 24\text{NH}_3$	-84.53	-	-	-
Li-R115	$3\text{Li}(\text{H}_3\text{N})_4 + \text{N}_2 = \text{Li}_3\text{N}_2 + 12\text{NH}_3$	-78.31	-	-	-
Li-R116	$2\text{Li}(\text{H}_3\text{N})_4 + \text{N}_2 = 2\text{LiN} + 8\text{NH}_3$	-72.09	-	-	-
Li-R117	$2/3\text{Li}(\text{H}_3\text{N})_4 + \text{N}_2 = 2/3\text{LiN}_3 + 8/3\text{NH}_3$	-34.77	-	-	-
Li-R118	$\text{Li}_{15}\text{H}_9\text{N}_8 + \text{N}_2 = 5\text{Li}_3\text{N}_2 + 9/2\text{H}_2$	8.41	-	-	-
Li-R119	$2/7\text{Li}_{15}\text{H}_9\text{N}_8 + \text{N}_2 = 30/7\text{LiN} + 9/7\text{H}_2$	39.51	-	-	-
Li-R120	$2/37\text{Li}_{15}\text{H}_9\text{N}_8 + \text{N}_2 = 30/37\text{LiN}_3 + 9/37\text{H}_2$	226.08	-	-	-
Li-R121	$4/5\text{Li}_{15}\text{H}_9\text{N}_8 + \text{N}_2 = 6\text{Li}_2\text{N} + 12/5\text{NH}_3$	-7.14	-	-	-
Li-R122	$2/5\text{Li}_{15}\text{H}_9\text{N}_8 + \text{N}_2 = 2\text{Li}_3\text{N}_2 + 6/5\text{NH}_3$	8.41	-	-	-
Li-R123	$1/5\text{Li}_{15}\text{H}_9\text{N}_8 + \text{N}_2 = 3\text{LiN} + 3/5\text{NH}_3$	39.51	-	-	-
Li-R124	$1/20\text{Li}_{15}\text{H}_9\text{N}_8 + \text{N}_2 = 3/4\text{LiN}_3 + 3/20\text{NH}_3$	226.08	-	-	-
Li-R125	$6\text{Li}_2\text{HN} + \text{N}_2 = 4\text{Li}_3\text{N}_2 + 3\text{H}_2$	12.67	-	-	-
Li-R126	$2\text{Li}_2\text{HN} + \text{N}_2 = 4\text{LiN} + \text{H}_2$	44.99	-	-	-
Li-R127	$2/5\text{Li}_2\text{HN} + \text{N}_2 = 4/5\text{LiN}_3 + 1/5\text{H}_2$	238.89	-	-	-
Li-R128	$6\text{Li}_2\text{HN} + \text{N}_2 = 6\text{Li}_2\text{N} + 2\text{NH}_3$	-3.49	-	-	-
Li-R129	$3\text{Li}_2\text{HN} + \text{N}_2 = 2\text{Li}_3\text{N}_2 + \text{NH}_3$	12.67	-	-	-
Li-R130	$3/2\text{Li}_2\text{HN} + \text{N}_2 = 3\text{LiN} + 1/2\text{NH}_3$	44.99	-	-	-
Li-R131	$3/8\text{Li}_2\text{HN} + \text{N}_2 = 3/4\text{LiN}_3 + 1/8\text{NH}_3$	238.89	-	-	-

Li-R132	$6\text{Li}_2\text{N} + \text{N}_2 = 4\text{Li}_3\text{N}_2$	16.74	-	-	-
Li-R133	$2\text{Li}_2\text{N} + \text{N}_2 = 4\text{LiN}$	50.23	-	-	-
Li-R134	$2/5\text{Li}_2\text{N} + \text{N}_2 = 4/5\text{LiN}_3$	251.14	-	-	-
Li-R135	$2\text{Li}_3(\text{HN})_2 + \text{N}_2 = 6\text{LiN} + 2\text{H}_2$	23.58	-	-	-
Li-R136	$2/7\text{Li}_3(\text{HN})_2 + \text{N}_2 = 6/7\text{LiN}_3 + 2/7\text{H}_2$	188.86	-	-	-
Li-R137	$12\text{Li}_3(\text{HN})_2 + \text{N}_2 = 18\text{Li}_2\text{N} + 8\text{NH}_3$	-17.74	-	-	-
Li-R138	$3\text{Li}_3(\text{HN})_2 + \text{N}_2 = 3\text{Li}_3\text{N}_2 + 2\text{NH}_3$	-3.96	-	-	-
Li-R139	$6/5\text{Li}_3(\text{HN})_2 + \text{N}_2 = 18/5\text{LiN} + 4/5\text{NH}_3$	23.58	-	-	-
Li-R140	$6/23\text{Li}_3(\text{HN})_2 + \text{N}_2 = 18/23\text{LiN}_3 + 4/23\text{NH}_3$	188.86	-	-	-
Li-R141	$2\text{Li}_3\text{H}_3\text{N}_2 + \text{N}_2 = 6\text{LiN} + 3\text{H}_2$	21.18	-	-	-
Li-R142	$2/7\text{Li}_3\text{H}_3\text{N}_2 + \text{N}_2 = 6/7\text{LiN}_3 + 3/7\text{H}_2$	183.24	-	-	-
Li-R143	Improbable stoichiometric coefficients	-16.42	-	-	-
Li-R144	$6\text{Li}_3\text{H}_3\text{N}_2 + \text{N}_2 = 6\text{Li}_3(\text{HN})_2 + 2\text{NH}_3$	-1.94	-	-	-
Li-R145	Improbable stoichiometric coefficients	-9.38	-	-	-
Li-R146	$4\text{Li}_3\text{H}_3\text{N}_2 + \text{N}_2 = 6\text{Li}_2\text{N} + 4\text{NH}_3$	-19.34	-	-	-
Li-R147	$2\text{Li}_3\text{H}_3\text{N}_2 + \text{N}_2 = 2\text{Li}_3\text{N}_2 + 2\text{NH}_3$	-5.83	-	-	-
Li-R148	$\text{Li}_3\text{H}_3\text{N}_2 + \text{N}_2 = 3\text{LiN} + \text{NH}_3$	21.18	-	-	-
Li-R149	$1/4\text{Li}_3\text{H}_3\text{N}_2 + \text{N}_2 = 3/4\text{LiN}_3 + 1/4\text{NH}_3$	183.24	-	-	-
Li-R150	$4\text{Li}_3\text{N} + \text{N}_2 = 6\text{Li}_2\text{N}$	20.11	-	-	-
Li-R151	$2\text{Li}_3\text{N} + \text{N}_2 = 2\text{Li}_3\text{N}_2$	40.22	-	-	-
Li-R152	$\text{Li}_3\text{N} + \text{N}_2 = 3\text{LiN}$	80.44	-	-	-
Li-R153	$1/4\text{Li}_3\text{N} + \text{N}_2 = 3/4\text{LiN}_3$	321.75	-18.43	-	endergonic
Li-R154	$2\text{Li}_3\text{N}_2 + \text{N}_2 = 6\text{LiN}$	28.68	-	-	-
Li-R155	$2/7\text{Li}_3\text{N}_2 + \text{N}_2 = 6/7\text{LiN}_3$	200.78	-	-	-
Li-R156	$2\text{Li}_4\text{HN} + \text{N}_2 = 4\text{Li}_2\text{N} + \text{H}_2$	30.39	-	-	-
Li-R157	$6\text{Li}_4\text{HN} + \text{N}_2 = 8\text{Li}_3\text{N} + 3\text{H}_2$	8.56	-	-	-
Li-R158	$6/5\text{Li}_4\text{HN} + \text{N}_2 = 8/5\text{Li}_3\text{N}_2 + 3/5\text{H}_2$	52.22	-	-	-
Li-R159	$2/3\text{Li}_4\text{HN} + \text{N}_2 = 8/3\text{LiN} + 1/3\text{H}_2$	95.88	-	-	-
Li-R160	$2/11\text{Li}_4\text{HN} + \text{N}_2 = 8/11\text{LiN}_3 + 1/11\text{H}_2$	357.85	-	-	-
Li-R161	$3/2\text{Li}_4\text{HN} + \text{N}_2 = 3\text{Li}_2\text{N} + 1/2\text{NH}_3$	30.39	-	-	-
Li-R162	$3\text{Li}_4\text{HN} + \text{N}_2 = 4\text{Li}_3\text{N} + \text{NH}_3$	8.56	-	-	-
Li-R163	$\text{Li}_4\text{HN} + \text{N}_2 = 4/3\text{Li}_3\text{N}_2 + 1/3\text{NH}_3$	52.22	-	-	-
Li-R164	$3/5\text{Li}_4\text{HN} + \text{N}_2 = 12/5\text{LiN} + 1/5\text{NH}_3$	95.88	-	-	-
Li-R165	$3/17\text{Li}_4\text{HN} + \text{N}_2 = 12/17\text{LiN}_3 + 1/17\text{NH}_3$	357.85	-	-	-
Li-R166	$3\text{Li}_7\text{H}_5\text{N}_4 + \text{N}_2 = 7\text{Li}_3(\text{HN})_2 + 1/2\text{H}_2$	8.21	-	-	-
Li-R167	$3\text{Li}_7\text{H}_5\text{N}_4 + \text{N}_2 = 7\text{Li}_3\text{N}_2 + 15/2\text{H}_2$	3.92	-	-	-

Li-R168	$2/3\text{Li}_7\text{H}_5\text{N}_4 + \text{N}_2 = 14/3\text{LiN} + 5/3\text{H}_2$	33.73	-	-	-
Li-R169	$2/17\text{Li}_7\text{H}_5\text{N}_4 + \text{N}_2 = 14/17\text{LiN}_3 + 5/17\text{H}_2$	212.57	-	-	-
Li-R170	$18/7\text{Li}_7\text{H}_5\text{N}_4 + \text{N}_2 = 6\text{Li}_3(\text{HN})_2 + 2/7\text{NH}_3$	8.21	-	-	-
Li-R171	$12/7\text{Li}_7\text{H}_5\text{N}_4 + \text{N}_2 = 6\text{Li}_2\text{N} + 20/7\text{NH}_3$	-10.98	-	-	-
Li-R172	$6/7\text{Li}_7\text{H}_5\text{N}_4 + \text{N}_2 = 2\text{Li}_3\text{N}_2 + 10/7\text{NH}_3$	3.92	-	-	-
Li-R173	$3/7\text{Li}_7\text{H}_5\text{N}_4 + \text{N}_2 = 3\text{LiN} + 5/7\text{NH}_3$	33.73	-	-	-
Li-R174	$3/28\text{Li}_7\text{H}_5\text{N}_4 + \text{N}_2 = 3/4\text{LiN}_3 + 5/28\text{NH}_3$	212.57	-	-	-
Li-R175	$15/4\text{LiH} + \text{N}_2 = 1/4\text{Li}_{15}\text{H}_9\text{N}_8 + 3/4\text{H}_2$	88.92	-	-	-
Li-R176	$4\text{LiH} + \text{N}_2 = 2\text{Li}_2\text{HN} + \text{H}_2$	81.78	-	-	-
Li-R177	$3\text{LiH} + \text{N}_2 = \text{Li}_3(\text{HN})_2 + 1/2\text{H}_2$	113.26	-	-	-
Li-R178	$3\text{LiH} + \text{N}_2 = \text{Li}_3\text{H}_3\text{N}_2$	117.49	-	-	-
Li-R179	$8\text{LiH} + \text{N}_2 = 2\text{Li}_4\text{HN} + 3\text{H}_2$	34.55	-	-	-
Li-R180	$7/2\text{LiH} + \text{N}_2 = 1/2\text{Li}_7\text{H}_5\text{N}_4 + 1/2\text{H}_2$	97.08	-	-	-
Li-R181	$4\text{LiH} + \text{N}_2 = 2\text{Li}_2\text{N} + 2\text{H}_2$	75.43	-	-	-
Li-R182	$6\text{LiH} + \text{N}_2 = 2\text{Li}_3\text{N} + 3\text{H}_2$	46.06	214.13	-	endergonic
Li-R183	$3\text{LiH} + \text{N}_2 = \text{Li}_3\text{N}_2 + 3/2\text{H}_2$	104.81	-	-	-
Li-R184	$2\text{LiH} + \text{N}_2 = 2\text{LiN} + \text{H}_2$	163.55	-	-	-
Li-R185	$2/3\text{LiH} + \text{N}_2 = 2/3\text{LiN}_3 + 1/3\text{H}_2$	516.02	7.41	-	endergonic
Li-R186	$6\text{LiH} + \text{N}_2 = 6\text{Li} + 2\text{NH}_3$	-12.68	451.45	-	endergonic
Li-R187	$3\text{LiH} + \text{N}_2 = 1/5\text{Li}_{15}\text{H}_9\text{N}_8 + 2/5\text{NH}_3$	88.92	-	-	-
Li-R188	$3\text{LiH} + \text{N}_2 = 3/2\text{Li}_2\text{HN} + 1/2\text{NH}_3$	81.78	-	-	-
Li-R189	$18/7\text{LiH} + \text{N}_2 = 6/7\text{Li}_3(\text{HN})_2 + 2/7\text{NH}_3$	113.26	-	-	-
Li-R190	$4\text{LiH} + \text{N}_2 = \text{Li}_4\text{HN} + \text{NH}_3$	34.55	-	-	-
Li-R191	$3\text{LiH} + \text{N}_2 = 3/7\text{Li}_7\text{H}_5\text{N}_4 + 2/7\text{NH}_3$	97.08	-	-	-
Li-R192	$12/5\text{LiH} + \text{N}_2 = 6/5\text{Li}_2\text{N} + 4/5\text{NH}_3$	75.43	-	-	-
Li-R193	$3\text{LiH} + \text{N}_2 = \text{Li}_3\text{N} + \text{NH}_3$	46.06	61.17	-	endergonic
Li-R194	$2\text{LiH} + \text{N}_2 = 2/3\text{Li}_3\text{N}_2 + 2/3\text{NH}_3$	104.81	-	-	-
Li-R195	$3/2\text{LiH} + \text{N}_2 = 3/2\text{LiN} + 1/2\text{NH}_3$	163.55	-	-	-
Li-R196	$3/5\text{LiH} + \text{N}_2 = 3/5\text{LiN}_3 + 1/5\text{NH}_3$	516.02	-2.51	-	endergonic
Li-R197	$\text{LiH}_2\text{N} + \text{N}_2 = \text{LiN}_3 + \text{H}_2$	113.22	148.48	-	endergonic
Li-R198	$18\text{LiH}_2\text{N} + \text{N}_2 = 6\text{Li}_3(\text{HN})_2 + 8\text{NH}_3$	-26.19	-	-	-
Li-R199	$12\text{LiH}_2\text{N} + \text{N}_2 = 6\text{Li}_2\text{N} + 8\text{NH}_3$	-39.28	-	-	-
Li-R200	$6\text{LiH}_2\text{N} + \text{N}_2 = 2\text{Li}_3\text{N}_2 + 4\text{NH}_3$	-29.11	-	-	-
Li-R201	$3\text{LiH}_2\text{N} + \text{N}_2 = 3\text{LiN} + 2\text{NH}_3$	-8.78	-	-	-
Li-R202	$3/4\text{LiH}_2\text{N} + \text{N}_2 = 3/4\text{LiN}_3 + 1/2\text{NH}_3$	113.22	88.41	-	endergonic
Li-R203	$\text{LiN} + \text{N}_2 = \text{LiN}_3$	133.74	-	-	-

Table S21: The Mn-based system

ID	Reaction	dm_stoich [%]	h298 [kJ/mol]	T_eq [°C]	Type
Mn-R01	$2\text{Mn} + \text{H}_2 = 2\text{MnH}$	1.83	-	-	-
Mn-R02	$1/9\text{Mn}(\text{H15N8})_2 + \text{H}_2 = 1/9\text{Mn} + 16/9\text{NH}_3$	-82.24	-	-	-
Mn-R03	$2/19\text{Mn}(\text{H15N8})_2 + \text{H}_2 = 2/19\text{MnH} + 32/19\text{NH}_3$	-81.91	-	-	-
Mn-R04	$1/8\text{Mn}(\text{H15N8})_2 + \text{H}_2 = 1/8\text{Mn}(\text{H}_2\text{N})_2 + 7/4\text{NH}_3$	-71.88	-	-	-
Mn-R05	$4/33\text{Mn}(\text{H15N8})_2 + \text{H}_2 = 2/33\text{Mn}_2\text{N} + 62/33\text{NH}_3$	-79.97	-	-	-
Mn-R06	$1/8\text{Mn}(\text{H15N8})_2 + \text{H}_2 = 1/24\text{Mn}_3\text{N}_2 + 23/12\text{NH}_3$	-79.22	-	-	-
Mn-R07	$1/7\text{Mn}(\text{H15N8})_2 + \text{H}_2 = 1/21\text{Mn}_3\text{N}_4 + 44/21\text{NH}_3$	-76.2	-	-	-
Mn-R08	$8/69\text{Mn}(\text{H15N8})_2 + \text{H}_2 = 2/69\text{Mn}_4\text{N} + 42/23\text{NH}_3$	-81.11	-	-	-
Mn-R09	$2/15\text{Mn}(\text{H15N8})_2 + \text{H}_2 = 2/15\text{MnN} + 2\text{NH}_3$	-77.71	-	-	-
Mn-R10	$5/42\text{Mn}(\text{H15N8})_2 + \text{H}_2 = 1/42\text{Mn}_5\text{N}_2 + 13/7\text{NH}_3$	-80.43	-	-	-
Mn-R11	$\text{Mn}(\text{H}_2\text{N})_2 + \text{H}_2 = \text{Mn} + 2\text{NH}_3$	-36.84	-	-	-
Mn-R12	$2/3\text{Mn}(\text{H}_2\text{N})_2 + \text{H}_2 = 2/3\text{MnH} + 4/3\text{NH}_3$	-35.68	-	-	-
Mn-R13	$4\text{Mn}(\text{H}_2\text{N})_2 + \text{H}_2 = 2\text{Mn}_2\text{N} + 6\text{NH}_3$	-28.79	-	-	-
Mn-R14	$8/5\text{Mn}(\text{H}_2\text{N})_2 + \text{H}_2 = 2/5\text{Mn}_4\text{N} + 14/5\text{NH}_3$	-32.82	-	-	-
Mn-R15	$5/2\text{Mn}(\text{H}_2\text{N})_2 + \text{H}_2 = 1/2\text{Mn}_5\text{N}_2 + 4\text{NH}_3$	-30.4	-	-	-
Mn-R16	$\text{Mn}_2\text{N} + \text{H}_2 = 2\text{MnH} + 1/2\text{N}_2$	-9.68	-	-	-
Mn-R17	$2/3\text{Mn}_2\text{N} + \text{H}_2 = 4/3\text{Mn} + 2/3\text{NH}_3$	-11.31	53.44	-	endergonic
Mn-R18	$2/5\text{Mn}_2\text{N} + \text{H}_2 = 4/5\text{MnH} + 2/5\text{NH}_3$	-9.68	-	-	-
Mn-R19	$4/3\text{Mn}_2\text{N} + \text{H}_2 = 2/3\text{Mn}_4\text{N} + 2/3\text{NH}_3$	-5.65	51.69	-	endergonic
Mn-R20	$10/3\text{Mn}_2\text{N} + \text{H}_2 = 4/3\text{Mn}_5\text{N}_2 + 2/3\text{NH}_3$	-2.26	117.28	-	endergonic
Mn-R21	$2/3\text{Mn}_3\text{N}_2 + \text{H}_2 = 2\text{MnH} + 2/3\text{N}_2$	-12.96	-	-	-
Mn-R22	$1/3\text{Mn}_3\text{N}_2 + \text{H}_2 = \text{Mn} + 2/3\text{NH}_3$	-14.53	33.28	-	endergonic
Mn-R23	$2/9\text{Mn}_3\text{N}_2 + \text{H}_2 = 2/3\text{MnH} + 4/9\text{NH}_3$	-12.96	-	-	-
Mn-R24	$4/3\text{Mn}_3\text{N}_2 + \text{H}_2 = 2\text{Mn}_2\text{N} + 2/3\text{NH}_3$	-3.63	-27.18	96.8	exergonic
Mn-R25	$8/15\text{Mn}_3\text{N}_2 + \text{H}_2 = 2/5\text{Mn}_4\text{N} + 2/3\text{NH}_3$	-9.08	20.15	-	endergonic
Mn-R26	$5/6\text{Mn}_3\text{N}_2 + \text{H}_2 = 1/2\text{Mn}_5\text{N}_2 + 2/3\text{NH}_3$	-5.81	26.99	-	endergonic
Mn-R27	$2/3\text{Mn}_3\text{N}_4 + \text{H}_2 = 2\text{MnH} + 4/3\text{N}_2$	-24	-	-	-
Mn-R28	$1/6\text{Mn}_3\text{N}_4 + \text{H}_2 = 1/2\text{Mn} + 2/3\text{NH}_3$	-25.37	-	-	-
Mn-R29	$2/15\text{Mn}_3\text{N}_4 + \text{H}_2 = 2/5\text{MnH} + 8/15\text{NH}_3$	-24	-	-	-
Mn-R30	$4/15\text{Mn}_3\text{N}_4 + \text{H}_2 = 2/5\text{Mn}_2\text{N} + 2/3\text{NH}_3$	-15.86	-	-	-
Mn-R31	$1/3\text{Mn}_3\text{N}_4 + \text{H}_2 = 1/3\text{Mn}_3\text{N}_2 + 2/3\text{NH}_3$	-12.69	-	-	-
Mn-R32	$8/39\text{Mn}_3\text{N}_4 + \text{H}_2 = 2/13\text{Mn}_4\text{N} + 2/3\text{NH}_3$	-20.61	-	-	-
Mn-R33	$2/3\text{Mn}_3\text{N}_4 + \text{H}_2 = 2\text{MnN} + 2/3\text{NH}_3$	-6.34	-	-	-

Mn-R34	$5/21\text{Mn}_3\text{N}_4 + \text{H}_2 = 1/7\text{Mn}_5\text{N}_2 + 2/3\text{NH}_3$	-17.76	-	-	-
Mn-R35	$1/2\text{Mn}_4\text{N} + \text{H}_2 = 2\text{MnH} + 1/4\text{N}_2$	-4.27	-	-	-
Mn-R36	$2/3\text{Mn}_4\text{N} + \text{H}_2 = 8/3\text{Mn} + 2/3\text{NH}_3$	-5.99	55.18	-	endergonic
Mn-R37	$2/7\text{Mn}_4\text{N} + \text{H}_2 = 8/7\text{MnH} + 2/7\text{NH}_3$	-4.27	-	-	-
Mn-R38	$2/5\text{Mn}_5\text{N}_2 + \text{H}_2 = 2\text{MnH} + 2/5\text{N}_2$	-7.59	-	-	-
Mn-R39	$1/3\text{Mn}_5\text{N}_2 + \text{H}_2 = 5/3\text{Mn} + 2/3\text{NH}_3$	-9.25	37.48	-	endergonic
Mn-R40	$2/11\text{Mn}_5\text{N}_2 + \text{H}_2 = 10/11\text{MnH} + 4/11\text{NH}_3$	-7.59	-	-	-
Mn-R41	$8/9\text{Mn}_5\text{N}_2 + \text{H}_2 = 10/9\text{Mn}_4\text{N} + 2/3\text{NH}_3$	-3.47	7.97	-	endergonic
Mn-R42	$2\text{MnN} + \text{H}_2 = 2\text{MnH} + \text{N}_2$	-18.85	-	-	-
Mn-R43	$2/3\text{MnN} + \text{H}_2 = 2/3\text{Mn} + 2/3\text{NH}_3$	-20.32	9.48	-	endergonic
Mn-R44	$1/2\text{MnN} + \text{H}_2 = 1/2\text{MnH} + 1/2\text{NH}_3$	-18.85	-	-	-
Mn-R45	$4/3\text{MnN} + \text{H}_2 = 2/3\text{Mn}_2\text{N} + 2/3\text{NH}_3$	-10.16	-34.48	624	exergonic
Mn-R46	$2\text{MnN} + \text{H}_2 = 2/3\text{Mn}_3\text{N}_2 + 2/3\text{NH}_3$	-6.77	-38.13	-	exergonic
Mn-R47	$8/9\text{MnN} + \text{H}_2 = 2/9\text{Mn}_4\text{N} + 2/3\text{NH}_3$	-15.24	-5.76	125.4	exergonic
Mn-R48	$10/9\text{MnN} + \text{H}_2 = 2/9\text{Mn}_5\text{N}_2 + 2/3\text{NH}_3$	-12.19	-9.19	272.6	exergonic
Mn-R49	$4\text{Mn} + \text{N}_2 = 2\text{Mn}_2\text{N}$	12.75	-252.1	-	exergonic
Mn-R50	$3\text{Mn} + \text{N}_2 = \text{Mn}_3\text{N}_2$	17	-191.64	-	exergonic
Mn-R51	$3/2\text{Mn} + \text{N}_2 = 1/2\text{Mn}_3\text{N}_4$	33.99	-	-	-
Mn-R52	$8\text{Mn} + \text{N}_2 = 2\text{Mn}_4\text{N}$	6.37	-257.33	-	exergonic
Mn-R53	$2\text{Mn} + \text{N}_2 = 2\text{MnN}$	25.5	-120.23	496.6	exergonic
Mn-R54	$5\text{Mn} + \text{N}_2 = \text{Mn}_5\text{N}_2$	10.2	-204.22	-	exergonic
Mn-R55	$3\text{Mn}(\text{H}_2\text{N})_2 + \text{N}_2 = \text{Mn}_3\text{N}_4 + 4\text{NH}_3$	-15.37	-	-	-
Mn-R56	$6\text{Mn}(\text{H}_2\text{N})_2 + \text{N}_2 = 6\text{MnN} + 8\text{NH}_3$	-20.74	-	-	-
Mn-R57	$6\text{Mn}_2\text{N} + \text{N}_2 = 4\text{Mn}_3\text{N}_2$	3.77	-10.26	-	exergonic
Mn-R58	$6/5\text{Mn}_2\text{N} + \text{N}_2 = 4/5\text{Mn}_3\text{N}_4$	18.84	-	-	-
Mn-R59	$2\text{Mn}_2\text{N} + \text{N}_2 = 4\text{MnN}$	11.31	11.65	-	endergonic
Mn-R60	$\text{Mn}_3\text{N}_2 + \text{N}_2 = \text{Mn}_3\text{N}_4$	14.53	-	-	-
Mn-R61	$2\text{Mn}_3\text{N}_2 + \text{N}_2 = 6\text{MnN}$	7.26	22.6	-	endergonic
Mn-R62	$2\text{Mn}_4\text{N} + \text{N}_2 = 4\text{Mn}_2\text{N}$	5.99	-246.87	639.4	exergonic
Mn-R63	$6/5\text{Mn}_4\text{N} + \text{N}_2 = 8/5\text{Mn}_3\text{N}_2$	9.99	-152.23	-	exergonic
Mn-R64	$6/13\text{Mn}_4\text{N} + \text{N}_2 = 8/13\text{Mn}_3\text{N}_4$	25.97	-	-	-
Mn-R65	$2/3\text{Mn}_4\text{N} + \text{N}_2 = 8/3\text{MnN}$	17.98	-74.52	204	exergonic
Mn-R66	$10/3\text{Mn}_4\text{N} + \text{N}_2 = 8/3\text{Mn}_5\text{N}_2$	3.6	-115.7	450.4	exergonic
Mn-R67	$4\text{Mn}_5\text{N}_2 + \text{N}_2 = 10\text{Mn}_2\text{N}$	2.31	-443.62	690.4	exergonic
Mn-R68	$3/2\text{Mn}_5\text{N}_2 + \text{N}_2 = 5/2\text{Mn}_3\text{N}_2$	6.17	-172.77	-	exergonic
Mn-R69	$3/7\text{Mn}_5\text{N}_2 + \text{N}_2 = 5/7\text{Mn}_3\text{N}_4$	21.59	-	-	-

Mn-R70	$2/3\text{Mn}_5\text{N}_2 + \text{N}_2 = 10/3\text{MnN}$	13.88	-64.23	144.9	exergonic
Mn-R71	$4\text{MnH} + \text{N}_2 = 2\text{Mn}_2\text{N} + 2\text{H}_2$	10.72	-	-	-
Mn-R72	$3\text{MnH} + \text{N}_2 = \text{Mn}_3\text{N}_2 + 3/2\text{H}_2$	14.89	-	-	-
Mn-R73	$3/2\text{MnH} + \text{N}_2 = 1/2\text{Mn}_3\text{N}_4 + 3/4\text{H}_2$	31.58	-	-	-
Mn-R74	$8\text{MnH} + \text{N}_2 = 2\text{Mn}_4\text{N} + 4\text{H}_2$	4.46	-	-	-
Mn-R75	$2\text{MnH} + \text{N}_2 = 2\text{MnN} + \text{H}_2$	23.23	-	-	-
Mn-R76	$5\text{MnH} + \text{N}_2 = \text{Mn}_5\text{N}_2 + 5/2\text{H}_2$	8.21	-	-	-
Mn-R77	$6\text{MnH} + \text{N}_2 = 6\text{Mn} + 2\text{NH}_3$	-1.8	-	-	-
Mn-R78	$12/5\text{MnH} + \text{N}_2 = 6/5\text{Mn}_2\text{N} + 4/5\text{NH}_3$	10.72	-	-	-
Mn-R79	$2\text{MnH} + \text{N}_2 = 2/3\text{Mn}_3\text{N}_2 + 2/3\text{NH}_3$	14.89	-	-	-
Mn-R80	$6/5\text{MnH} + \text{N}_2 = 2/5\text{Mn}_3\text{N}_4 + 2/5\text{NH}_3$	31.58	-	-	-
Mn-R81	$24/7\text{MnH} + \text{N}_2 = 6/7\text{Mn}_4\text{N} + 8/7\text{NH}_3$	4.46	-	-	-
Mn-R82	$3/2\text{MnH} + \text{N}_2 = 3/2\text{MnN} + 1/2\text{NH}_3$	23.23	-	-	-
Mn-R83	$30/11\text{MnH} + \text{N}_2 = 6/11\text{Mn}_5\text{N}_2 + 10/11\text{NH}_3$	8.21	-	-	-
Mn-R84	$6\text{MnN} + \text{N}_2 = 2\text{Mn}_3\text{N}_4$	6.77	-	-	-

Table S22: The Mo-based system

ID	Reaction	dm_stoich [%]	h298 [kJ/mol]	T_eq [°C]	Type
Mo-R001	$6\text{Mo} + \text{H}_2 = 2\text{Mo}_3\text{H}$	0.35	656.27	-	endergonic
Mo-R002	$2\text{Mo} + \text{H}_2 = 2\text{MoH}$	1.05	152.06	-	endergonic
Mo-R003	$2/5\text{Mo}_{15}\text{N}_{16} + \text{H}_2 = 2\text{Mo}_3\text{H} + 16/5\text{N}_2$	-13.17	-	-	-
Mo-R004	$2/15\text{Mo}_{15}\text{N}_{16} + \text{H}_2 = 2\text{MoH} + 16/15\text{N}_2$	-12.56	-	-	-
Mo-R005	$1/24\text{Mo}_{15}\text{N}_{16} + \text{H}_2 = 5/8\text{Mo} + 2/3\text{NH}_3$	-13.47	-	-	-
Mo-R006	$2/53\text{Mo}_{15}\text{N}_{16} + \text{H}_2 = 10/53\text{Mo}_3\text{H} + 32/53\text{NH}_3$	-13.17	-	-	-
Mo-R007	$2/63\text{Mo}_{15}\text{N}_{16} + \text{H}_2 = 10/21\text{MoH} + 32/63\text{NH}_3$	-12.56	-	-	-
Mo-R008	$4/51\text{Mo}_{15}\text{N}_{16} + \text{H}_2 = 10/17\text{Mo}_2\text{N} + 2/3\text{NH}_3$	-7.16	-	-	-
Mo-R009	$1/9\text{Mo}_{15}\text{N}_{16} + \text{H}_2 = 5/9\text{Mo}_3\text{N}_2 + 2/3\text{NH}_3$	-5.05	-	-	-
Mo-R010	$2/3\text{Mo}_{15}\text{N}_{16} + \text{H}_2 = 10\text{MoN} + 2/3\text{NH}_3$	-0.84	-	-	-
Mo-R011	$1/24\text{Mo}_{15}\text{N}_{16} + \text{H}_2 = 5/16\text{Mo}_2 + 2/3\text{NH}_3$	-13.47	-	-	-
Mo-R012	$3\text{Mo}_2 + \text{H}_2 = 2\text{Mo}_3\text{H}$	0.35	-446.23	389.5	exergonic
Mo-R013	$\text{Mo}_2 + \text{H}_2 = 2\text{MoH}$	1.05	-215.44	416.4	exergonic
Mo-R014	$3\text{Mo}_2\text{N} + \text{H}_2 = 2\text{Mo}_3\text{H} + 3/2\text{N}_2$	-6.48	901.03	-	endergonic
Mo-R015	$\text{Mo}_2\text{N} + \text{H}_2 = 2\text{MoH} + 1/2\text{N}_2$	-5.82	233.64	-	endergonic
Mo-R016	$2/3\text{Mo}_2\text{N} + \text{H}_2 = 4/3\text{Mo} + 2/3\text{NH}_3$	-6.8	23.79	-	endergonic
Mo-R017	$6/11\text{Mo}_2\text{N} + \text{H}_2 = 4/11\text{Mo}_3\text{H} + 6/11\text{NH}_3$	-6.48	138.79	-	endergonic
Mo-R018	$2/5\text{Mo}_2\text{N} + \text{H}_2 = 4/5\text{MoH} + 2/5\text{NH}_3$	-5.82	75.1	-	endergonic
Mo-R019	$2/3\text{Mo}_2\text{N} + \text{H}_2 = 2/3\text{Mo}_2 + 2/3\text{NH}_3$	-6.8	268.79	-	endergonic
Mo-R020	$3\text{Mo}_2\text{N}_3 + \text{H}_2 = 2\text{Mo}_3\text{H} + 9/2\text{N}_2$	-17.68	-	-	-
Mo-R021	$\text{Mo}_2\text{N}_3 + \text{H}_2 = 2\text{MoH} + 3/2\text{N}_2$	-17.1	-	-	-
Mo-R022	$2/9\text{Mo}_2\text{N}_3 + \text{H}_2 = 4/9\text{Mo} + 2/3\text{NH}_3$	-17.96	-	-	-
Mo-R023	$6/29\text{Mo}_2\text{N}_3 + \text{H}_2 = 4/29\text{Mo}_3\text{H} + 18/29\text{NH}_3$	-17.68	-	-	-
Mo-R024	$2/11\text{Mo}_2\text{N}_3 + \text{H}_2 = 4/11\text{MoH} + 6/11\text{NH}_3$	-17.1	-	-	-
Mo-R025	$10/13\text{Mo}_2\text{N}_3 + \text{H}_2 = 4/39\text{Mo}_{15}\text{N}_{16} + 2/3\text{NH}_3$	-5.19	-	-	-

Mo-R026	$1/3\text{Mo}_2\text{N}_3 + \text{H}_2 = 1/3\text{Mo}_2\text{N} + 2/3\text{NH}_3$	-11.98	-	-	-
Mo-R027	$2/5\text{Mo}_2\text{N}_3 + \text{H}_2 = 4/15\text{Mo}_3\text{N}_2 + 2/3\text{NH}_3$	-9.98	-	-	-
Mo-R028	$2/3\text{Mo}_2\text{N}_3 + \text{H}_2 = 4/3\text{MoN} + 2/3\text{NH}_3$	-5.99	-	-	-
Mo-R029	$2/9\text{Mo}_2\text{N}_3 + \text{H}_2 = 2/9\text{Mo}_2 + 2/3\text{NH}_3$	-17.96	-	-	-
Mo-R030	$\text{Mo}_3\text{H} + \text{H}_2 = 3\text{MoH}$	0.7	-100.05	485.6	exergonic
Mo-R031	$2\text{Mo}_3\text{N}_2 + \text{H}_2 = 2\text{Mo}_3\text{H} + 2\text{N}_2$	-8.55	-	-	-
Mo-R032	$2/3\text{Mo}_3\text{N}_2 + \text{H}_2 = 2\text{MoH} + 2/3\text{N}_2$	-7.91	-	-	-
Mo-R033	$1/3\text{Mo}_3\text{N}_2 + \text{H}_2 = \text{Mo} + 2/3\text{NH}_3$	-8.87	-	-	-
Mo-R034	$2/7\text{Mo}_3\text{N}_2 + \text{H}_2 = 2/7\text{Mo}_3\text{H} + 4/7\text{NH}_3$	-8.55	-	-	-
Mo-R035	$2/9\text{Mo}_3\text{N}_2 + \text{H}_2 = 2/3\text{MoH} + 4/9\text{NH}_3$	-7.91	-	-	-
Mo-R036	$4/3\text{Mo}_3\text{N}_2 + \text{H}_2 = 2\text{Mo}_2\text{N} + 2/3\text{NH}_3$	-2.22	-	-	-
Mo-R037	$1/3\text{Mo}_3\text{N}_2 + \text{H}_2 = 1/2\text{Mo}_2 + 2/3\text{NH}_3$	-8.87	-	-	-
Mo-R038	$6\text{MoN} + \text{H}_2 = 2\text{Mo}_3\text{H} + 3\text{N}_2$	-12.43	901.02	-	endergonic
Mo-R039	$2\text{MoN} + \text{H}_2 = 2\text{MoH} + \text{N}_2$	-11.82	233.64	-	endergonic
Mo-R040	$2/3\text{MoN} + \text{H}_2 = 2/3\text{Mo} + 2/3\text{NH}_3$	-12.74	-3.4	293	exergonic
Mo-R041	$3/5\text{MoN} + \text{H}_2 = 1/5\text{Mo}_3\text{H} + 3/5\text{NH}_3$	-12.43	62.56	-	endergonic
Mo-R042	$1/2\text{MoN} + \text{H}_2 = 1/2\text{MoH} + 1/2\text{NH}_3$	-11.82	35.46	-	endergonic
Mo-R043	$4/3\text{MoN} + \text{H}_2 = 2/3\text{Mo}_2\text{N} + 2/3\text{NH}_3$	-6.37	-30.6	-	exergonic
Mo-R044	$2\text{MoN} + \text{H}_2 = 2/3\text{Mo}_3\text{N}_2 + 2/3\text{NH}_3$	-4.25	-	-	-
Mo-R045	$2/3\text{MoN} + \text{H}_2 = 1/3\text{Mo}_2 + 2/3\text{NH}_3$	-12.74	119.1	-	endergonic
Mo-R046	$6\text{MoN}_2 + \text{H}_2 = 2\text{Mo}_3\text{H} + 6\text{N}_2$	-22.33	822.74	-	endergonic
Mo-R047	$2\text{MoN}_2 + \text{H}_2 = 2\text{MoH} + 2\text{N}_2$	-21.79	207.55	-	endergonic
Mo-R048	$1/3\text{MoN}_2 + \text{H}_2 = 1/3\text{Mo} + 2/3\text{NH}_3$	-22.6	-21.35	520.4	exergonic
Mo-R049	$6/19\text{MoN}_2 + \text{H}_2 = 2/19\text{Mo}_3\text{H} + 12/19\text{NH}_3$	-22.33	14.31	-	endergonic
Mo-R050	$2/7\text{MoN}_2 + \text{H}_2 = 2/7\text{MoH} + 4/7\text{NH}_3$	-21.79	3.42	-	endergonic
Mo-R051	$5/7\text{MoN}_2 + \text{H}_2 = 1/21\text{Mo}_{15}\text{N}_{16} + 2/3\text{NH}_3$	-10.55	-	-	-
Mo-R052	$4/9\text{MoN}_2 + \text{H}_2 = 2/9\text{Mo}_2\text{N} + 2/3\text{NH}_3$	-16.95	-36.4	788.7	exergonic
Mo-R053	$4/3\text{MoN}_2 + \text{H}_2 = 2/3\text{Mo}_2\text{N}_3 + 2/3\text{NH}_3$	-5.65	-	-	-
Mo-R054	$1/2\text{MoN}_2 + \text{H}_2 = 1/6\text{Mo}_3\text{N}_2 + 2/3\text{NH}_3$	-15.07	-	-	-
Mo-R055	$2/3\text{MoN}_2 + \text{H}_2 = 2/3\text{MoN} + 2/3\text{NH}_3$	-11.3	-39.3	568	exergonic
Mo-R056	$1/3\text{MoN}_2 + \text{H}_2 = 1/6\text{Mo}_2 + 2/3\text{NH}_3$	-22.6	39.9	-	endergonic
Mo-R057	$15/8\text{Mo} + \text{N}_2 = 1/8\text{Mo}_{15}\text{N}_{16}$	15.57	-	-	-
Mo-R058	$4\text{Mo} + \text{N}_2 = 2\text{Mo}_2\text{N}$	7.3	-163.18	686.8	exergonic
Mo-R059	$4/3\text{Mo} + \text{N}_2 = 2/3\text{Mo}_2\text{N}_3$	21.9	-	-	-
Mo-R060	$3\text{Mo} + \text{N}_2 = \text{Mo}_3\text{N}_2$	9.73	-	-	-
Mo-R061	$2\text{Mo} + \text{N}_2 = 2\text{MoN}$	14.6	-81.59	165.1	exergonic
Mo-R062	$\text{Mo} + \text{N}_2 = \text{MoN}_2$	29.2	-27.75	-	endergonic
Mo-R063	$4/13\text{Mo}_{15}\text{N}_{16} + \text{N}_2 = 30/13\text{Mo}_2\text{N}_3$	5.47	-	-	-
Mo-R064	$1/7\text{Mo}_{15}\text{N}_{16} + \text{N}_2 = 15/7\text{MoN}_2$	11.79	-	-	-
Mo-R065	$15/16\text{Mo}_2 + \text{N}_2 = 1/8\text{Mo}_{15}\text{N}_{16}$	15.57	-	-	-
Mo-R066	$2\text{Mo}_2 + \text{N}_2 = 2\text{Mo}_2\text{N}$	7.3	-898.18	-	exergonic
Mo-R067	$2/3\text{Mo}_2 + \text{N}_2 = 2/3\text{Mo}_2\text{N}_3$	21.9	-	-	-
Mo-R068	$3/2\text{Mo}_2 + \text{N}_2 = \text{Mo}_3\text{N}_2$	9.73	-	-	-
Mo-R069	$\text{Mo}_2 + \text{N}_2 = 2\text{MoN}$	14.6	-449.09	-	exergonic
Mo-R070	$1/2\text{Mo}_2 + \text{N}_2 = \text{MoN}_2$	29.2	-211.5	656.9	exergonic
Mo-R071	$30/17\text{Mo}_2\text{N} + \text{N}_2 = 4/17\text{Mo}_{15}\text{N}_{16}$	7.71	-	-	-
Mo-R072	$\text{Mo}_2\text{N} + \text{N}_2 = \text{Mo}_2\text{N}_3$	13.61	-	-	-
Mo-R073	$6\text{Mo}_2\text{N} + \text{N}_2 = 4\text{Mo}_3\text{N}_2$	2.27	-	-	-
Mo-R074	$2\text{Mo}_2\text{N} + \text{N}_2 = 4\text{MoN}$	6.8	0	-	endergonic

Mo-R075	$2/3\text{Mo}_2\text{N} + \text{N}_2 = 4/3\text{MoN}_2$	20.41	17.4	-	endergonic
Mo-R076	$2\text{Mo}_2\text{N}_3 + \text{N}_2 = 4\text{MoN}_2$	5.99	-	-	-
Mo-R077	$5/8\text{Mo}_3\text{H} + \text{N}_2 = 1/8\text{Mo}_{15}\text{N}_{16} + 5/16\text{H}_2$	15.17	-	-	-
Mo-R078	$4/3\text{Mo}_3\text{H} + \text{N}_2 = 2\text{Mo}_2\text{N} + 2/3\text{H}_2$	6.92	-600.69	-	exergonic
Mo-R079	$4/9\text{Mo}_3\text{H} + \text{N}_2 = 2/3\text{Mo}_2\text{N}_3 + 2/9\text{H}_2$	21.47	-	-	-
Mo-R080	$\text{Mo}_3\text{H} + \text{N}_2 = \text{Mo}_3\text{N}_2 + 1/2\text{H}_2$	9.35	-	-	-
Mo-R081	$2/3\text{Mo}_3\text{H} + \text{N}_2 = 2\text{MoN} + 1/3\text{H}_2$	14.2	-300.34	-	exergonic
Mo-R082	$1/3\text{Mo}_3\text{H} + \text{N}_2 = \text{MoN}_2 + 1/6\text{H}_2$	28.75	-137.12	-	exergonic
Mo-R083	$6\text{Mo}_3\text{H} + \text{N}_2 = 18\text{Mo} + 2\text{NH}_3$	-0.35	-2060.59	-	exergonic
Mo-R084	$30/53\text{Mo}_3\text{H} + \text{N}_2 = 6/53\text{Mo}_{15}\text{N}_{16} + 10/53\text{NH}_3$	15.17	-	-	-
Mo-R085	$12/11\text{Mo}_3\text{H} + \text{N}_2 = 18/11\text{Mo}_2\text{N} + 4/11\text{NH}_3$	6.92	-508.16	-	exergonic
Mo-R086	$12/29\text{Mo}_3\text{H} + \text{N}_2 = 18/29\text{Mo}_2\text{N}_3 + 4/29\text{NH}_3$	21.47	-	-	-
Mo-R087	$6/7\text{Mo}_3\text{H} + \text{N}_2 = 6/7\text{Mo}_3\text{N}_2 + 2/7\text{NH}_3$	9.35	-	-	-
Mo-R088	$3/5\text{Mo}_3\text{H} + \text{N}_2 = 9/5\text{MoN} + 1/5\text{NH}_3$	14.2	-279.49	-	exergonic
Mo-R089	$6/19\text{Mo}_3\text{H} + \text{N}_2 = 18/19\text{MoN}_2 + 2/19\text{NH}_3$	28.75	-134.74	-	exergonic
Mo-R090	$6\text{Mo}_3\text{H} + \text{N}_2 = 9\text{Mo}_2 + 2\text{NH}_3$	-0.35	1246.91	416.5	exergonic
Mo-R091	$5/3\text{Mo}_3\text{N}_2 + \text{N}_2 = 1/3\text{Mo}_{15}\text{N}_{16}$	5.32	-	-	-
Mo-R092	$4/5\text{Mo}_3\text{N}_2 + \text{N}_2 = 6/5\text{Mo}_2\text{N}_3$	11.09	-	-	-
Mo-R093	$2\text{Mo}_3\text{N}_2 + \text{N}_2 = 6\text{MoN}$	4.43	-	-	-
Mo-R094	$1/2\text{Mo}_3\text{N}_2 + \text{N}_2 = 3/2\text{MoN}_2$	17.74	-	-	-
Mo-R095	$15/8\text{MoH} + \text{N}_2 = 1/8\text{Mo}_{15}\text{N}_{16} + 15/16\text{H}_2$	14.37	-	-	-
Mo-R096	$4\text{MoH} + \text{N}_2 = 2\text{Mo}_2\text{N} + 2\text{H}_2$	6.18	-467.29	-	exergonic
Mo-R097	$4/3\text{MoH} + \text{N}_2 = 2/3\text{Mo}_2\text{N}_3 + 2/3\text{H}_2$	20.63	-	-	-
Mo-R098	$3\text{MoH} + \text{N}_2 = \text{Mo}_3\text{N}_2 + 3/2\text{H}_2$	8.59	-	-	-
Mo-R099	$2\text{MoH} + \text{N}_2 = 2\text{MoN} + \text{H}_2$	13.41	-233.64	-	exergonic
Mo-R100	$\text{MoH} + \text{N}_2 = \text{MoN}_2 + 1/2\text{H}_2$	27.85	-103.77	-	exergonic
Mo-R101	$6\text{MoH} + \text{N}_2 = 6\text{Mo} + 2\text{NH}_3$	-1.04	-547.96	-	exergonic
Mo-R102	$9\text{MoH} + \text{N}_2 = 3\text{Mo}_3\text{H} + 2\text{NH}_3$	-0.69	208.35	-	endergonic
Mo-R103	$10/7\text{MoH} + \text{N}_2 = 2/21\text{Mo}_{15}\text{N}_{16} + 10/21\text{NH}_3$	14.37	-	-	-
Mo-R104	$12/5\text{MoH} + \text{N}_2 = 6/5\text{Mo}_2\text{N} + 4/5\text{NH}_3$	6.18	-317.09	-	exergonic
Mo-R105	$12/11\text{MoH} + \text{N}_2 = 6/11\text{Mo}_2\text{N}_3 + 4/11\text{NH}_3$	20.63	-	-	-
Mo-R106	$2\text{MoH} + \text{N}_2 = 2/3\text{Mo}_3\text{N}_2 + 2/3\text{NH}_3$	8.59	-	-	-
Mo-R107	$3/2\text{MoH} + \text{N}_2 = 3/2\text{MoN} + 1/2\text{NH}_3$	13.41	-198.18	-	exergonic
Mo-R108	$6/7\text{MoH} + \text{N}_2 = 6/7\text{MoN}_2 + 2/7\text{NH}_3$	27.85	-102.06	-	exergonic
Mo-R109	$6\text{MoH} + \text{N}_2 = 3\text{Mo}_2 + 2\text{NH}_3$	-1.04	554.54	495.3	exergonic
Mo-R110	$30\text{MoN} + \text{N}_2 = 2\text{Mo}_{15}\text{N}_{16}$	0.85	-	-	-
Mo-R111	$4\text{MoN} + \text{N}_2 = 2\text{Mo}_2\text{N}_3$	6.37	-	-	-
Mo-R112	$2\text{MoN} + \text{N}_2 = 2\text{MoN}_2$	12.74	26.09	-	endergonic

Table S23: The Ni-based system

ID	Reaction	dm_stoich [%]	h298 [kJ/mol]	T_eq [°C]	Type
Ni-R001	$4\text{Ni} + \text{H}_2 = 2\text{Ni}_2\text{H}$	0.86	22.53	-	endergonic
Ni-R002	$6\text{Ni} + \text{H}_2 = 2\text{Ni}_3\text{H}$	0.57	-	-	-
Ni-R003	$2\text{Ni} + \text{H}_2 = 2\text{NiH}$	1.72	-4.28	-	endergonic
Ni-R004	$2/3\text{Ni} + \text{H}_2 = 2/3\text{NiH}_3$	5.15	-	-	-
Ni-R005	$4\text{Ni} + \text{H}_2 = 4\text{NiH}_{0.5}$	0.86	-7.58	-	endergonic



Ni-R006	$200/59\text{Ni} + \text{H}_2 = 200/59\text{NiH}_{0.59}$	1.01	-7.84	-	endergonic
Ni-R007	$50/17\text{Ni} + \text{H}_2 = 50/17\text{NiH}_{0.68}$	1.17	-8.43	-	endergonic
Ni-R008	$\text{Ni}(\text{H}_2\text{N})_2 + \text{H}_2 = \text{Ni} + 2\text{NH}_3$	-35.32	-	-	-
Ni-R009	$4/5\text{Ni}(\text{H}_2\text{N})_2 + \text{H}_2 = 2/5\text{Ni}_2\text{H} + 8/5\text{NH}_3$	-34.76	-	-	-
Ni-R010	$6/7\text{Ni}(\text{H}_2\text{N})_2 + \text{H}_2 = 2/7\text{Ni}_3\text{H} + 12/7\text{NH}_3$	-34.95	-	-	-
Ni-R011	$2/3\text{Ni}(\text{H}_2\text{N})_2 + \text{H}_2 = 2/3\text{NiH} + 4/3\text{NH}_3$	-34.21	-	-	-
Ni-R012	$2/5\text{Ni}(\text{H}_2\text{N})_2 + \text{H}_2 = 2/5\text{NiH}_3 + 4/5\text{NH}_3$	-31.98	-	-	-
Ni-R013	$2\text{Ni}(\text{H}_2\text{N})_2 + \text{H}_2 = 2/3\text{Ni}_3\text{N} + 10/3\text{NH}_3$	-30.17	-	-	-
Ni-R014	$8/5\text{Ni}(\text{H}_2\text{N})_2 + \text{H}_2 = 2/5\text{Ni}_4\text{N} + 14/5\text{NH}_3$	-31.46	-	-	-
Ni-R015	$4/5\text{Ni}(\text{H}_2\text{N})_2 + \text{H}_2 = 4/5\text{NiH}_{0.5} + 8/5\text{NH}_3$	-34.76	-	-	-
Ni-R016	$200/259\text{Ni}(\text{H}_2\text{N})_2 + \text{H}_2 = 200/259\text{NiH}_{0.59} + 400/259\text{NH}_3$	-34.66	-	-	-
Ni-R017	$50/67\text{Ni}(\text{H}_2\text{N})_2 + \text{H}_2 = 50/67\text{NiH}_{0.68} + 100/67\text{NH}_3$	-34.56	-	-	-
Ni-R018	$2\text{Ni}_2\text{H} + \text{H}_2 = 4\text{NiH}$	0.85	-31.09	55.9	exergonic
Ni-R019	$2/5\text{Ni}_2\text{H} + \text{H}_2 = 4/5\text{NiH}_3$	4.26	-	-	-
Ni-R020	$100/9\text{Ni}_2\text{H} + \text{H}_2 = 200/9\text{NiH}_{0.59}$	0.15	-176.57	-	exergonic
Ni-R021	$50/9\text{Ni}_2\text{H} + \text{H}_2 = 100/9\text{NiH}_{0.68}$	0.31	-94.42	675.3	exergonic
Ni-R022	$4\text{Ni}_3\text{H} + \text{H}_2 = 6\text{Ni}_2\text{H}$	0.28	-	-	-
Ni-R023	$\text{Ni}_3\text{H} + \text{H}_2 = 3\text{NiH}$	1.14	-	-	-
Ni-R024	$1/4\text{Ni}_3\text{H} + \text{H}_2 = 3/4\text{NiH}_3$	4.55	-	-	-
Ni-R025	$4\text{Ni}_3\text{H} + \text{H}_2 = 12\text{NiH}_{0.5}$	0.28	-	-	-
Ni-R026	$200/77\text{Ni}_3\text{H} + \text{H}_2 = 600/77\text{NiH}_{0.59}$	0.44	-	-	-
Ni-R027	$25/13\text{Ni}_3\text{H} + \text{H}_2 = 75/13\text{NiH}_{0.68}$	0.59	-	-	-
Ni-R028	$4/3\text{Ni}_3\text{N} + \text{H}_2 = 2\text{Ni}_2\text{H} + 2/3\text{N}_2$	-6.57	21.41	-	endergonic
Ni-R029	$2\text{Ni}_3\text{N} + \text{H}_2 = 2\text{Ni}_3\text{H} + \text{N}_2$	-6.84	-	-	-
Ni-R030	$2/3\text{Ni}_3\text{N} + \text{H}_2 = 2\text{NiH} + 1/3\text{N}_2$	-5.78	-4.84	-	endergonic
Ni-R031	$2/9\text{Ni}_3\text{N} + \text{H}_2 = 2/3\text{NiH}_3 + 1/9\text{N}_2$	-2.6	-	-	-
Ni-R032	$4/3\text{Ni}_3\text{N} + \text{H}_2 = 4\text{NiH}_{0.5} + 2/3\text{N}_2$	-6.57	-8.7	-	exergonic
Ni-R033	$200/177\text{Ni}_3\text{N} + \text{H}_2 = 200/59\text{NiH}_{0.59} + 100/177\text{N}_2$	-6.43	-8.79	500.5	exergonic
Ni-R034	$50/51\text{Ni}_3\text{N} + \text{H}_2 = 50/17\text{NiH}_{0.68} + 25/51\text{N}_2$	-6.29	-9.25	141.6	exergonic
Ni-R035	$2/3\text{Ni}_3\text{N} + \text{H}_2 = 2\text{Ni} + 2/3\text{NH}_3$	-7.37	-31.16	-	exergonic
Ni-R036	$4/9\text{Ni}_3\text{N} + \text{H}_2 = 2/3\text{Ni}_2\text{H} + 4/9\text{NH}_3$	-6.57	-13.26	24.1	exergonic
Ni-R037	$1/2\text{Ni}_3\text{N} + \text{H}_2 = 1/2\text{Ni}_3\text{H} + 1/2\text{NH}_3$	-6.84	-	-	-
Ni-R038	$1/3\text{Ni}_3\text{N} + \text{H}_2 = \text{NiH} + 1/3\text{NH}_3$	-5.78	-17.72	37.2	exergonic
Ni-R039	$1/6\text{Ni}_3\text{N} + \text{H}_2 = 1/2\text{NiH}_3 + 1/6\text{NH}_3$	-2.6	-	-	-
Ni-R040	$8/3\text{Ni}_3\text{N} + \text{H}_2 = 2\text{Ni}_4\text{N} + 2/3\text{NH}_3$	-1.84	-	-	-
Ni-R041	$4/9\text{Ni}_3\text{N} + \text{H}_2 = 4/3\text{NiH}_{0.5} + 4/9\text{NH}_3$	-6.57	-23.3	282.4	exergonic

Ni-R042	$200/477\text{Ni}_3\text{N} + \text{H}_2 = 200/159\text{NiH}_0.59 + 200/477\text{NH}_3$	-6.43	-22.51	223.7	exergonic
Ni-R043	$25/63\text{Ni}_3\text{N} + \text{H}_2 = 25/21\text{NiH}_0.68 + 25/63\text{NH}_3$	-6.29	-21.96	174.6	exergonic
Ni-R044	$\text{Ni}_4\text{N} + \text{H}_2 = 2\text{Ni}_2\text{H} + 1/2\text{N}_2$	-4.82	-	-	-
Ni-R045	$3/2\text{Ni}_4\text{N} + \text{H}_2 = 2\text{Ni}_3\text{H} + 3/4\text{N}_2$	-5.09	-	-	-
Ni-R046	$1/2\text{Ni}_4\text{N} + \text{H}_2 = 2\text{NiH} + 1/4\text{N}_2$	-4.01	-	-	-
Ni-R047	$1/6\text{Ni}_4\text{N} + \text{H}_2 = 2/3\text{NiH}_3 + 1/12\text{N}_2$	-0.77	-	-	-
Ni-R048	$\text{Ni}_4\text{N} + \text{H}_2 = 4\text{NiH}_0.5 + 1/2\text{N}_2$	-4.82	-	-	-
Ni-R049	$50/59\text{Ni}_4\text{N} + \text{H}_2 = 200/59\text{NiH}_0.59 + 25/59\text{N}_2$	-4.67	-	-	-
Ni-R050	$25/34\text{Ni}_4\text{N} + \text{H}_2 = 50/17\text{NiH}_0.68 + 25/68\text{N}_2$	-4.53	-	-	-
Ni-R051	$2/3\text{Ni}_4\text{N} + \text{H}_2 = 8/3\text{Ni} + 2/3\text{NH}_3$	-5.63	-	-	-
Ni-R052	$2/5\text{Ni}_4\text{N} + \text{H}_2 = 4/5\text{Ni}_2\text{H} + 2/5\text{NH}_3$	-4.82	-	-	-
Ni-R053	$6/13\text{Ni}_4\text{N} + \text{H}_2 = 8/13\text{Ni}_3\text{H} + 6/13\text{NH}_3$	-5.09	-	-	-
Ni-R054	$2/7\text{Ni}_4\text{N} + \text{H}_2 = 8/7\text{NiH} + 2/7\text{NH}_3$	-4.01	-	-	-
Ni-R055	$2/15\text{Ni}_4\text{N} + \text{H}_2 = 8/15\text{NiH}_3 + 2/15\text{NH}_3$	-0.77	-	-	-
Ni-R056	$2/5\text{Ni}_4\text{N} + \text{H}_2 = 8/5\text{NiH}_0.5 + 2/5\text{NH}_3$	-4.82	-	-	-
Ni-R057	$25/67\text{Ni}_4\text{N} + \text{H}_2 = 100/67\text{NiH}_0.59 + 25/67\text{NH}_3$	-4.67	-	-	-
Ni-R058	$50/143\text{Ni}_4\text{N} + \text{H}_2 = 200/143\text{NiH}_0.68 + 50/143\text{NH}_3$	-4.53	-	-	-
Ni-R059	$\text{Ni}_4\text{N}_3 + \text{H}_2 = 2\text{Ni}_2\text{H} + 3/2\text{N}_2$	-14.45	-	-	-
Ni-R060	$3/2\text{Ni}_4\text{N}_3 + \text{H}_2 = 2\text{Ni}_3\text{H} + 9/4\text{N}_2$	-14.7	-	-	-
Ni-R061	$1/2\text{Ni}_4\text{N}_3 + \text{H}_2 = 2\text{NiH} + 3/4\text{N}_2$	-13.72	-	-	-
Ni-R062	$1/6\text{Ni}_4\text{N}_3 + \text{H}_2 = 2/3\text{NiH}_3 + 1/4\text{N}_2$	-10.81	-	-	-
Ni-R063	$\text{Ni}_4\text{N}_3 + \text{H}_2 = 4\text{NiH}_0.5 + 3/2\text{N}_2$	-14.45	-	-	-
Ni-R064	$50/59\text{Ni}_4\text{N}_3 + \text{H}_2 = 200/59\text{NiH}_0.59 + 75/59\text{N}_2$	-14.32	-	-	-
Ni-R065	$25/34\text{Ni}_4\text{N}_3 + \text{H}_2 = 50/17\text{NiH}_0.68 + 75/68\text{N}_2$	-14.19	-	-	-
Ni-R066	$2/9\text{Ni}_4\text{N}_3 + \text{H}_2 = 8/9\text{Ni} + 2/3\text{NH}_3$	-15.18	-	-	-
Ni-R067	$2/11\text{Ni}_4\text{N}_3 + \text{H}_2 = 4/11\text{Ni}_2\text{H} + 6/11\text{NH}_3$	-14.45	-	-	-
Ni-R068	$6/31\text{Ni}_4\text{N}_3 + \text{H}_2 = 8/31\text{Ni}_3\text{H} + 18/31\text{NH}_3$	-14.7	-	-	-
Ni-R069	$2/13\text{Ni}_4\text{N}_3 + \text{H}_2 = 8/13\text{NiH} + 6/13\text{NH}_3$	-13.72	-	-	-
Ni-R070	$2/21\text{Ni}_4\text{N}_3 + \text{H}_2 = 8/21\text{NiH}_3 + 2/7\text{NH}_3$	-10.81	-	-	-
Ni-R071	$2/5\text{Ni}_4\text{N}_3 + \text{H}_2 = 8/15\text{Ni}_3\text{N} + 2/3\text{NH}_3$	-8.43	-	-	-
Ni-R072	$1/3\text{Ni}_4\text{N}_3 + \text{H}_2 = 1/3\text{Ni}_4\text{N} + 2/3\text{NH}_3$	-10.12	-	-	-
Ni-R073	$2/11\text{Ni}_4\text{N}_3 + \text{H}_2 = 8/11\text{NiH}_0.5 + 6/11\text{NH}_3$	-14.45	-	-	-
Ni-R074	$25/142\text{Ni}_4\text{N}_3 + \text{H}_2 = 50/71\text{NiH}_0.59 + 75/142\text{NH}_3$	-14.32	-	-	-
Ni-R075	$50/293\text{Ni}_4\text{N}_3 + \text{H}_2 = 200/293\text{NiH}_0.68 + 150/293\text{NH}_3$	-14.19	-	-	-
Ni-R076	$\text{NiH} + \text{H}_2 = \text{NiH}_3$	3.38	-	-	-
Ni-R077	$4\text{NiH}_0.5 + \text{H}_2 = 4\text{NiH}$	0.85	-0.98	-	endergonic

Ni-R078	$4/5\text{NiH}0.5 + \text{H}_2 = 4/5\text{NiH}_3$	4.26	-	-	-
Ni-R079	$200/9\text{NiH}0.5 + \text{H}_2 = 200/9\text{NiH}0.59$	0.15	-9.31	-	endergonic
Ni-R080	$100/9\text{NiH}0.5 + \text{H}_2 = 100/9\text{NiH}0.68$	0.31	-10.78	-	endergonic
Ni-R081	$200/41\text{NiH}0.59 + \text{H}_2 = 200/41\text{NiH}$	0.7	0.84	-	endergonic
Ni-R082	$200/241\text{NiH}0.59 + \text{H}_2 = 200/241\text{NiH}_3$	4.1	-	-	-
Ni-R083	$200/9\text{NiH}0.59 + \text{H}_2 = 200/9\text{NiH}0.68$	0.15	-12.26	-	endergonic
Ni-R084	$25/4\text{NiH}0.68 + \text{H}_2 = 25/4\text{NiH}$	0.54	4.53	-	endergonic
Ni-R085	$25/29\text{NiH}0.68 + \text{H}_2 = 25/29\text{NiH}_3$	3.94	-	-	-
Ni-R086	$4\text{NiN} + \text{H}_2 = 2\text{Ni}_2\text{H} + 2\text{N}_2$	-18.57	-218.73	-	exergonic
Ni-R087	$6\text{NiN} + \text{H}_2 = 2\text{Ni}_3\text{H} + 3\text{N}_2$	-18.8	-	-	-
Ni-R088	$2\text{NiN} + \text{H}_2 = 2\text{NiH} + \text{N}_2$	-17.88	-124.91	-	exergonic
Ni-R089	$2/3\text{NiN} + \text{H}_2 = 2/3\text{NiH}_3 + 1/3\text{N}_2$	-15.11	-	-	-
Ni-R090	$4\text{NiN} + \text{H}_2 = 4\text{NiH}0.5 + 2\text{N}_2$	-18.57	-248.84	-	exergonic
Ni-R091	$200/59\text{NiN} + \text{H}_2 = 200/59\text{NiH}0.59 + 100/59\text{N}_2$	-18.45	-212.3	-	exergonic
Ni-R092	$50/17\text{NiN} + \text{H}_2 = 50/17\text{NiH}0.68 + 25/17\text{N}_2$	-18.32	-185.83	-	exergonic
Ni-R093	$2/3\text{NiN} + \text{H}_2 = 2/3\text{Ni} + 2/3\text{NH}_3$	-19.27	-70.81	-	exergonic
Ni-R094	$4/7\text{NiN} + \text{H}_2 = 2/7\text{Ni}_2\text{H} + 4/7\text{NH}_3$	-18.57	-57.47	-	exergonic
Ni-R095	$3/5\text{NiN} + \text{H}_2 = 1/5\text{Ni}_3\text{H} + 3/5\text{NH}_3$	-18.8	-	-	-
Ni-R096	$1/2\text{NiN} + \text{H}_2 = 1/2\text{NiH} + 1/2\text{NH}_3$	-17.88	-54.18	-	exergonic
Ni-R097	$1/3\text{NiN} + \text{H}_2 = 1/3\text{NiH}_3 + 1/3\text{NH}_3$	-15.11	-	-	-
Ni-R098	$\text{NiN} + \text{H}_2 = 1/3\text{Ni}_3\text{N} + 2/3\text{NH}_3$	-12.84	-90.63	-	exergonic
Ni-R099	$8/9\text{NiN} + \text{H}_2 = 2/9\text{Ni}_4\text{N} + 2/3\text{NH}_3$	-14.45	-	-	-
Ni-R100	$8/3\text{NiN} + \text{H}_2 = 2/3\text{Ni}_4\text{N}_3 + 2/3\text{NH}_3$	-4.82	-	-	-
Ni-R101	$4/7\text{NiN} + \text{H}_2 = 4/7\text{NiH}0.5 + 4/7\text{NH}_3$	-18.57	-61.78	-	exergonic
Ni-R102	$200/359\text{NiN} + \text{H}_2 = 200/359\text{NiH}0.59 + 200/359\text{NH}_3$	-18.45	-60.46	-	exergonic
Ni-R103	$25/46\text{NiN} + \text{H}_2 = 25/46\text{NiH}0.68 + 25/46\text{NH}_3$	-18.32	-59.28	-	exergonic
Ni-R104	$6\text{Ni} + \text{N}_2 = 2\text{Ni}_3\text{N}$	7.95	1.67	-	endergonic
Ni-R105	$8\text{Ni} + \text{N}_2 = 2\text{Ni}_4\text{N}$	5.97	-	-	-
Ni-R106	$8/3\text{Ni} + \text{N}_2 = 2/3\text{Ni}_4\text{N}_3$	17.9	-	-	-
Ni-R107	$2\text{Ni} + \text{N}_2 = 2\text{NiN}$	23.86	120.63	-	endergonic
Ni-R108	$24\text{Ni}(\text{H}_2\text{N})_2 + \text{N}_2 = 6\text{Ni}_4\text{N}_3 + 32\text{NH}_3$	-23.74	-	-	-
Ni-R109	$6\text{Ni}(\text{H}_2\text{N})_2 + \text{N}_2 = 6\text{NiN} + 8\text{NH}_3$	-19.88	-	-	-
Ni-R110	$3\text{Ni}_2\text{H} + \text{N}_2 = 2\text{Ni}_3\text{N} + 3/2\text{H}_2$	7.04	-32.12	-	exergonic
Ni-R111	$4\text{Ni}_2\text{H} + \text{N}_2 = 2\text{Ni}_4\text{N} + 2\text{H}_2$	5.06	-	-	-
Ni-R112	$4/3\text{Ni}_2\text{H} + \text{N}_2 = 2/3\text{Ni}_4\text{N}_3 + 2/3\text{H}_2$	16.89	-	-	-
Ni-R113	$\text{Ni}_2\text{H} + \text{N}_2 = 2\text{NiN} + 1/2\text{H}_2$	22.81	109.37	-	endergonic

Ni-R114	$6\text{Ni}_2\text{H} + \text{N}_2 = 12\text{Ni} + 2\text{NH}_3$	-0.85	-159.38	-	exergonic
Ni-R115	$18\text{Ni}_2\text{H} + \text{N}_2 = 12\text{Ni}_3\text{H} + 2\text{NH}_3$	-0.28	-	-	-
Ni-R116	$2\text{Ni}_2\text{H} + \text{N}_2 = 4/3\text{Ni}_3\text{N} + 2/3\text{NH}_3$	7.04	-52.01	504.2	exergonic
Ni-R117	$12/5\text{Ni}_2\text{H} + \text{N}_2 = 6/5\text{Ni}_4\text{N} + 4/5\text{NH}_3$	5.06	-	-	-
Ni-R118	$12/11\text{Ni}_2\text{H} + \text{N}_2 = 6/11\text{Ni}_4\text{N}_3 + 4/11\text{NH}_3$	16.89	-	-	-
Ni-R119	$6/7\text{Ni}_2\text{H} + \text{N}_2 = 12/7\text{NiN} + 2/7\text{NH}_3$	22.81	80.63	-	endergonic
Ni-R120	$2\text{Ni}_3\text{H} + \text{N}_2 = 2\text{Ni}_3\text{N} + \text{H}_2$	7.34	-	-	-
Ni-R121	$8/3\text{Ni}_3\text{H} + \text{N}_2 = 2\text{Ni}_4\text{N} + 4/3\text{H}_2$	5.36	-	-	-
Ni-R122	$8/9\text{Ni}_3\text{H} + \text{N}_2 = 2/3\text{Ni}_4\text{N}_3 + 4/9\text{H}_2$	17.23	-	-	-
Ni-R123	$2/3\text{Ni}_3\text{H} + \text{N}_2 = 2\text{NiN} + 1/3\text{H}_2$	23.16	-	-	-
Ni-R124	$6\text{Ni}_3\text{H} + \text{N}_2 = 18\text{Ni} + 2\text{NH}_3$	-0.57	-	-	-
Ni-R125	$3/2\text{Ni}_3\text{H} + \text{N}_2 = 3/2\text{Ni}_3\text{N} + 1/2\text{NH}_3$	7.34	-	-	-
Ni-R126	$24/13\text{Ni}_3\text{H} + \text{N}_2 = 18/13\text{Ni}_4\text{N} + 8/13\text{NH}_3$	5.36	-	-	-
Ni-R127	$24/31\text{Ni}_3\text{H} + \text{N}_2 = 18/31\text{Ni}_4\text{N}_3 + 8/31\text{NH}_3$	17.23	-	-	-
Ni-R128	$3/5\text{Ni}_3\text{H} + \text{N}_2 = 9/5\text{NiN} + 1/5\text{NH}_3$	23.16	-	-	-
Ni-R129	$8/5\text{Ni}_3\text{N} + \text{N}_2 = 6/5\text{Ni}_4\text{N}_3$	9.21	-	-	-
Ni-R130	$\text{Ni}_3\text{N} + \text{N}_2 = 3\text{NiN}$	14.74	180.11	-	endergonic
Ni-R131	$6\text{Ni}_4\text{N} + \text{N}_2 = 8\text{Ni}_3\text{N}$	1.88	-	-	-
Ni-R132	$\text{Ni}_4\text{N} + \text{N}_2 = \text{Ni}_4\text{N}_3$	11.26	-	-	-
Ni-R133	$2/3\text{Ni}_4\text{N} + \text{N}_2 = 8/3\text{NiN}$	16.89	-	-	-
Ni-R134	$2\text{Ni}_4\text{N}_3 + \text{N}_2 = 8\text{NiN}$	5.06	-	-	-
Ni-R135	$6\text{NiH} + \text{N}_2 = 2\text{Ni}_3\text{N} + 3\text{H}_2$	6.13	14.52	-	exergonic
Ni-R136	$8\text{NiH} + \text{N}_2 = 2\text{Ni}_4\text{N} + 4\text{H}_2$	4.18	-	-	-
Ni-R137	$8/3\text{NiH} + \text{N}_2 = 2/3\text{Ni}_4\text{N}_3 + 4/3\text{H}_2$	15.91	-	-	-
Ni-R138	$2\text{NiH} + \text{N}_2 = 2\text{NiN} + \text{H}_2$	21.77	124.91	-	endergonic
Ni-R139	$6\text{NiH} + \text{N}_2 = 6\text{Ni} + 2\text{NH}_3$	-1.69	-78.95	-	exergonic
Ni-R140	$12\text{NiH} + \text{N}_2 = 6\text{Ni}_2\text{H} + 2\text{NH}_3$	-0.84	1.49	-	exergonic
Ni-R141	$9\text{NiH} + \text{N}_2 = 3\text{Ni}_3\text{H} + 2\text{NH}_3$	-1.13	-	-	-
Ni-R142	$3\text{NiH} + \text{N}_2 = \text{Ni}_3\text{N} + \text{NH}_3$	6.13	-38.64	721.7	exergonic
Ni-R143	$24/7\text{NiH} + \text{N}_2 = 6/7\text{Ni}_4\text{N} + 8/7\text{NH}_3$	4.18	-	-	-
Ni-R144	$24/13\text{NiH} + \text{N}_2 = 6/13\text{Ni}_4\text{N}_3 + 8/13\text{NH}_3$	15.91	-	-	-
Ni-R145	$3/2\text{NiH} + \text{N}_2 = 3/2\text{NiN} + 1/2\text{NH}_3$	21.77	70.74	-	endergonic
Ni-R146	$12\text{NiH} + \text{N}_2 = 12\text{NiH}_{0.5} + 2\text{NH}_3$	-0.84	-88.84	-	exergonic
Ni-R147	$600/41\text{NiH} + \text{N}_2 = 600/41\text{NiH}_{0.59} + 2\text{NH}_3$	-0.69	-94.32	-	exergonic
Ni-R148	$75/4\text{NiH} + \text{N}_2 = 75/4\text{NiH}_{0.68} + 2\text{NH}_3$	-0.54	-105.38	-	exergonic
Ni-R149	$6\text{NiH}_{0.5} + \text{N}_2 = 2\text{Ni}_3\text{N} + 3/2\text{H}_2$	7.04	13.04	-	endergonic

Ni-R150	$8\text{NiH}0.5 + \text{N}_2 = 2\text{Ni}_4\text{N} + 2\text{H}_2$	5.06	-	-	-
Ni-R151	$8/3\text{NiH}0.5 + \text{N}_2 = 2/3\text{Ni}_4\text{N}_3 + 2/3\text{H}_2$	16.89	-	-	-
Ni-R152	$2\text{NiH}0.5 + \text{N}_2 = 2\text{NiN} + 1/2\text{H}_2$	22.81	124.42	-	endergonic
Ni-R153	$12\text{NiH}0.5 + \text{N}_2 = 12\text{Ni} + 2\text{NH}_3$	-0.85	-69.05	-	exergonic
Ni-R154	$36\text{NiH}0.5 + \text{N}_2 = 12\text{Ni}_3\text{H} + 2\text{NH}_3$	-0.28	-	-	-
Ni-R155	$4\text{NiH}0.5 + \text{N}_2 = 4/3\text{Ni}_3\text{N} + 2/3\text{NH}_3$	7.04	-21.9	7.6	exergonic
Ni-R156	$24/5\text{NiH}0.5 + \text{N}_2 = 6/5\text{Ni}_4\text{N} + 4/5\text{NH}_3$	5.06	-	-	-
Ni-R157	$24/11\text{NiH}0.5 + \text{N}_2 = 6/11\text{Ni}_4\text{N}_3 + 4/11\text{NH}_3$	16.89	-	-	-
Ni-R158	$12/7\text{NiH}0.5 + \text{N}_2 = 12/7\text{NiN} + 2/7\text{NH}_3$	22.81	93.53	-	endergonic
Ni-R159	$6\text{NiH}0.59 + \text{N}_2 = 2\text{Ni}_3\text{N} + 177/100\text{H}_2$	6.87	15.56	500.5	exergonic
Ni-R160	$8\text{NiH}0.59 + \text{N}_2 = 2\text{Ni}_4\text{N} + 59/25\text{H}_2$	4.9	-	-	-
Ni-R161	$8/3\text{NiH}0.59 + \text{N}_2 = 2/3\text{Ni}_4\text{N}_3 + 59/75\text{H}_2$	16.72	-	-	-
Ni-R162	$2\text{NiH}0.59 + \text{N}_2 = 2\text{NiN} + 59/100\text{H}_2$	22.62	125.26	-	endergonic
Ni-R163	$600/59\text{NiH}0.59 + \text{N}_2 = 600/59\text{Ni} + 2\text{NH}_3$	-1	-68.26	-	exergonic
Ni-R164	$200/3\text{NiH}0.59 + \text{N}_2 = 100/3\text{Ni}_2\text{H} + 2\text{NH}_3$	-0.15	437.93	-	endergonic
Ni-R165	$1800/77\text{NiH}0.59 + \text{N}_2 = 600/77\text{Ni}_3\text{H} + 2\text{NH}_3$	-0.44	-	-	-
Ni-R166	$200/53\text{NiH}0.59 + \text{N}_2 = 200/159\text{Ni}_3\text{N} + 118/159\text{NH}_3$	6.87	-24.28	92.5	exergonic
Ni-R167	$300/67\text{NiH}0.59 + \text{N}_2 = 75/67\text{Ni}_4\text{N} + 59/67\text{NH}_3$	4.9	-	-	-
Ni-R168	$150/71\text{NiH}0.59 + \text{N}_2 = 75/142\text{Ni}_4\text{N}_3 + 59/142\text{NH}_3$	16.72	-	-	-
Ni-R169	$600/359\text{NiH}0.59 + \text{N}_2 = 600/359\text{NiN} + 118/359\text{NH}_3$	22.62	89.59	-	endergonic
Ni-R170	$200/3\text{NiH}0.59 + \text{N}_2 = 200/3\text{NiH}0.5 + 2\text{NH}_3$	-0.15	-63.87	-	exergonic
Ni-R171	$6\text{NiH}0.68 + \text{N}_2 = 2\text{Ni}_3\text{N} + 51/25\text{H}_2$	6.71	18.87	141.6	exergonic
Ni-R172	$8\text{NiH}0.68 + \text{N}_2 = 2\text{Ni}_4\text{N} + 68/25\text{H}_2$	4.74	-	-	-
Ni-R173	$8/3\text{NiH}0.68 + \text{N}_2 = 2/3\text{Ni}_4\text{N}_3 + 68/75\text{H}_2$	16.54	-	-	-
Ni-R174	$2\text{NiH}0.68 + \text{N}_2 = 2\text{NiN} + 17/25\text{H}_2$	22.44	126.36	-	endergonic
Ni-R175	$150/17\text{NiH}0.68 + \text{N}_2 = 150/17\text{Ni} + 2\text{NH}_3$	-1.15	-66.51	-	exergonic
Ni-R176	$100/3\text{NiH}0.68 + \text{N}_2 = 50/3\text{Ni}_2\text{H} + 2\text{NH}_3$	-0.31	191.46	-	endergonic
Ni-R177	$225/13\text{NiH}0.68 + \text{N}_2 = 75/13\text{Ni}_3\text{H} + 2\text{NH}_3$	-0.59	-	-	-
Ni-R178	$25/7\text{NiH}0.68 + \text{N}_2 = 25/21\text{Ni}_3\text{N} + 17/21\text{NH}_3$	6.71	-25.92	206.2	exergonic
Ni-R179	$600/143\text{NiH}0.68 + \text{N}_2 = 150/143\text{Ni}_4\text{N} + 136/143\text{NH}_3$	4.74	-	-	-
Ni-R180	$600/293\text{NiH}0.68 + \text{N}_2 = 150/293\text{Ni}_4\text{N}_3 + 136/293\text{NH}_3$	16.54	-	-	-
Ni-R181	$75/46\text{NiH}0.68 + \text{N}_2 = 75/46\text{NiN} + 17/46\text{NH}_3$	22.44	86.05	-	endergonic
Ni-R182	$100/3\text{NiH}0.68 + \text{N}_2 = 100/3\text{NiH}0.5 + 2\text{NH}_3$	-0.31	-59.44	-	exergonic
Ni-R183	$200/3\text{NiH}0.68 + \text{N}_2 = 200/3\text{NiH}0.59 + 2\text{NH}_3$	-0.15	-55.01	-	exergonic
Ni-R184	$6\text{NiH}_3 + \text{N}_2 = 2\text{Ni}_3\text{N} + 9\text{H}_2$	2.67	-	-	-
Ni-R185	$8\text{NiH}_3 + \text{N}_2 = 2\text{Ni}_4\text{N} + 12\text{H}_2$	0.77	-	-	-

Ni-R186	$8/3\text{NiH}_3 + \text{N}_2 = 2/3\text{Ni}_4\text{N}_3 + 4\text{H}_2$	12.12	-	-	-
Ni-R187	$2\text{NiH}_3 + \text{N}_2 = 2\text{NiN} + 3\text{H}_2$	17.8	-	-	-
Ni-R188	$2\text{NiH}_3 + \text{N}_2 = 2\text{Ni} + 2\text{NH}_3$	-4.9	-	-	-
Ni-R189	$12/5\text{NiH}_3 + \text{N}_2 = 6/5\text{Ni}_2\text{H} + 2\text{NH}_3$	-4.08	-	-	-
Ni-R190	$9/4\text{NiH}_3 + \text{N}_2 = 3/4\text{Ni}_3\text{H} + 2\text{NH}_3$	-4.36	-	-	-
Ni-R191	$3\text{NiH}_3 + \text{N}_2 = 3\text{NiH} + 2\text{NH}_3$	-3.27	-	-	-
Ni-R192	$3/2\text{NiH}_3 + \text{N}_2 = 1/2\text{Ni}_3\text{N} + 3/2\text{NH}_3$	2.67	-	-	-
Ni-R193	$8/5\text{NiH}_3 + \text{N}_2 = 2/5\text{Ni}_4\text{N} + 8/5\text{NH}_3$	0.77	-	-	-
Ni-R194	$8/7\text{NiH}_3 + \text{N}_2 = 2/7\text{Ni}_4\text{N}_3 + 8/7\text{NH}_3$	12.12	-	-	-
Ni-R195	$\text{NiH}_3 + \text{N}_2 = \text{NiN} + \text{NH}_3$	17.8	-	-	-
Ni-R196	$12/5\text{NiH}_3 + \text{N}_2 = 12/5\text{NiH}_{0.5} + 2\text{NH}_3$	-4.08	-	-	-
Ni-R197	$600/241\text{NiH}_3 + \text{N}_2 = 600/241\text{NiH}_{0.59} + 2\text{NH}_3$	-3.94	-	-	-
Ni-R198	$75/29\text{NiH}_3 + \text{N}_2 = 75/29\text{NiH}_{0.68} + 2\text{NH}_3$	-3.79	-	-	-

Table S24: The Sr-based system

ID	Reaction	dm_stoich [%]	h298 [kJ/mol]	T_eq [°C]	Type
Sr-R001	$6\text{Sr} + \text{H}_2 = 2\text{Sr}_3\text{H}$	0.38	-	-	-
Sr-R002	$\text{Sr} + \text{H}_2 = \text{SrH}_2$	2.3	-180	-	exergonic
Sr-R003	$2/3\text{Sr} + \text{H}_2 = 2/3\text{SrH}_3$	3.45	-37.33	99.1	exergonic
Sr-R004	$\text{Sr}(\text{H}_2\text{N})_2 + \text{H}_2 = \text{Sr} + 2\text{NH}_3$	-26.78	-	-	-
Sr-R005	$6/7\text{Sr}(\text{H}_2\text{N})_2 + \text{H}_2 = 2/7\text{Sr}_3\text{H} + 12/7\text{NH}_3$	-26.5	-	-	-
Sr-R006	$1/2\text{Sr}(\text{H}_2\text{N})_2 + \text{H}_2 = 1/2\text{SrH}_2 + \text{NH}_3$	-25.09	-	-	-
Sr-R007	$2/5\text{Sr}(\text{H}_2\text{N})_2 + \text{H}_2 = 2/5\text{SrH}_3 + 4/5\text{NH}_3$	-24.25	-	-	-
Sr-R008	$2\text{Sr}(\text{H}_2\text{N})_2 + \text{H}_2 = \text{Sr}_2\text{HN} + 3\text{NH}_3$	-20.51	-	-	-
Sr-R009	$4\text{Sr}(\text{H}_2\text{N})_2 + \text{H}_2 = 2\text{Sr}_2\text{N} + 6\text{NH}_3$	-20.93	-	-	-
Sr-R010	$2/3\text{Sr}_2\text{HN} + \text{H}_2 = 4/3\text{SrH}_2 + 1/3\text{N}_2$	-5.77	-44.91	244.9	exergonic
Sr-R011	$2/5\text{Sr}_2\text{HN} + \text{H}_2 = 4/5\text{SrH}_3 + 1/5\text{N}_2$	-4.71	72.26	-	endergonic
Sr-R012	$\text{Sr}_2\text{HN} + \text{H}_2 = 2\text{Sr} + \text{NH}_3$	-7.89	246.74	-	endergonic
Sr-R013	$3/4\text{Sr}_2\text{HN} + \text{H}_2 = 1/2\text{Sr}_3\text{H} + 3/4\text{NH}_3$	-7.54	-	-	-
Sr-R014	$1/3\text{Sr}_2\text{HN} + \text{H}_2 = 2/3\text{SrH}_2 + 1/3\text{NH}_3$	-5.77	-37.75	218	exergonic
Sr-R015	$1/4\text{Sr}_2\text{HN} + \text{H}_2 = 1/2\text{SrH}_3 + 1/4\text{NH}_3$	-4.71	33.69	-	endergonic
Sr-R016	$3\text{Sr}_2\text{N} + \text{H}_2 = 2\text{Sr}_3\text{H} + 3/2\text{N}_2$	-7.05	-	-	-
Sr-R017	$1/2\text{Sr}_2\text{N} + \text{H}_2 = \text{SrH}_2 + 1/4\text{N}_2$	-5.27	-82.75	523.4	exergonic
Sr-R018	$1/3\text{Sr}_2\text{N} + \text{H}_2 = 2/3\text{SrH}_3 + 1/6\text{N}_2$	-4.21	27.5	-	endergonic
Sr-R019	$2\text{Sr}_2\text{N} + \text{H}_2 = 2\text{Sr}_2\text{HN}$	0.53	-196.29	-	exergonic
Sr-R020	$2/3\text{Sr}_2\text{N} + \text{H}_2 = 4/3\text{Sr} + 2/3\text{NH}_3$	-7.4	99.07	-	endergonic
Sr-R021	$6/11\text{Sr}_2\text{N} + \text{H}_2 = 4/11\text{Sr}_3\text{H} + 6/11\text{NH}_3$	-7.05	-	-	-
Sr-R022	$2/7\text{Sr}_2\text{N} + \text{H}_2 = 4/7\text{SrH}_2 + 2/7\text{NH}_3$	-5.27	-60.4	407.8	exergonic
Sr-R023	$2/9\text{Sr}_2\text{N} + \text{H}_2 = 4/9\text{SrH}_3 + 2/9\text{NH}_3$	-4.21	8.13	-	endergonic
Sr-R024	$2/5\text{Sr}_3\text{H} + \text{H}_2 = 6/5\text{SrH}_2$	1.91	-	-	-
Sr-R025	$1/4\text{Sr}_3\text{H} + \text{H}_2 = 3/4\text{SrH}_3$	3.06	-	-	-
Sr-R026	$2\text{Sr}_3\text{N}_2 + \text{H}_2 = 2\text{Sr}_3\text{H} + 2\text{N}_2$	-9.28	-	-	-
Sr-R027	$1/3\text{Sr}_3\text{N}_2 + \text{H}_2 = \text{SrH}_2 + 1/3\text{N}_2$	-7.55	-49.6	533.1	exergonic

Sr-R028	$2/9\text{Sr}_3\text{N}_2 + \text{H}_2 = 2/3\text{SrH}_3 + 2/9\text{N}_2$	-6.51	49.6	-	endergonic
Sr-R029	$4/3\text{Sr}_3\text{N}_2 + \text{H}_2 = 2\text{Sr}_2\text{HN} + 1/3\text{N}_2$	-1.89	-63.67	-	exergonic
Sr-R030	$1/3\text{Sr}_3\text{N}_2 + \text{H}_2 = \text{Sr} + 2/3\text{NH}_3$	-9.63	99.8	-	endergonic
Sr-R031	$2/7\text{Sr}_3\text{N}_2 + \text{H}_2 = 2/7\text{Sr}_3\text{H} + 4/7\text{NH}_3$	-9.28	-	-	-
Sr-R032	$1/6\text{Sr}_3\text{N}_2 + \text{H}_2 = 1/2\text{SrH}_2 + 1/3\text{NH}_3$	-7.55	-40.1	351.5	exergonic
Sr-R033	$2/15\text{Sr}_3\text{N}_2 + \text{H}_2 = 2/5\text{SrH}_3 + 4/15\text{NH}_3$	-6.51	17.52	-	endergonic
Sr-R034	$2/3\text{Sr}_3\text{N}_2 + \text{H}_2 = \text{Sr}_2\text{HN} + 1/3\text{NH}_3$	-1.89	-47.13	-	exergonic
Sr-R035	$4/3\text{Sr}_3\text{N}_2 + \text{H}_2 = 2\text{Sr}_2\text{N} + 2/3\text{NH}_3$	-2.41	102.02	-	endergonic
Sr-R036	$3/2\text{Sr}_4\text{N}_3 + \text{H}_2 = 2\text{Sr}_3\text{H} + 9/4\text{N}_2$	-10.36	-	-	-
Sr-R037	$1/4\text{Sr}_4\text{N}_3 + \text{H}_2 = \text{SrH}_2 + 3/8\text{N}_2$	-8.65	-	-	-
Sr-R038	$1/6\text{Sr}_4\text{N}_3 + \text{H}_2 = 2/3\text{SrH}_3 + 1/4\text{N}_2$	-7.62	-	-	-
Sr-R039	$\text{Sr}_4\text{N}_3 + \text{H}_2 = 2\text{Sr}_2\text{HN} + 1/2\text{N}_2$	-3.06	-	-	-
Sr-R040	$2/9\text{Sr}_4\text{N}_3 + \text{H}_2 = 8/9\text{Sr} + 2/3\text{NH}_3$	-10.71	-	-	-
Sr-R041	$6/31\text{Sr}_4\text{N}_3 + \text{H}_2 = 8/31\text{Sr}_3\text{H} + 18/31\text{NH}_3$	-10.36	-	-	-
Sr-R042	$2/17\text{Sr}_4\text{N}_3 + \text{H}_2 = 8/17\text{SrH}_2 + 6/17\text{NH}_3$	-8.65	-	-	-
Sr-R043	$2/21\text{Sr}_4\text{N}_3 + \text{H}_2 = 8/21\text{SrH}_3 + 2/7\text{NH}_3$	-7.62	-	-	-
Sr-R044	$2/5\text{Sr}_4\text{N}_3 + \text{H}_2 = 4/5\text{Sr}_2\text{HN} + 2/5\text{NH}_3$	-3.06	-	-	-
Sr-R045	$2/3\text{Sr}_4\text{N}_3 + \text{H}_2 = 4/3\text{Sr}_2\text{N} + 2/3\text{NH}_3$	-3.57	-	-	-
Sr-R046	$2\text{Sr}_4\text{N}_3 + \text{H}_2 = 8/3\text{Sr}_3\text{N}_2 + 2/3\text{NH}_3$	-1.19	-	-	-
Sr-R047	$2\text{SrH}_2 + \text{H}_2 = 2\text{SrH}_3$	1.12	248.01	-	endergonic
Sr-R048	$2\text{SrHN} + \text{H}_2 = 2\text{SrH}_2 + \text{N}_2$	-12.67	-	-	-
Sr-R049	$\text{SrHN} + \text{H}_2 = \text{SrH}_3 + 1/2\text{N}_2$	-11.68	-	-	-
Sr-R050	$\text{SrHN} + \text{H}_2 = \text{Sr} + \text{NH}_3$	-14.63	-	-	-
Sr-R051	$6/7\text{SrHN} + \text{H}_2 = 2/7\text{Sr}_3\text{H} + 6/7\text{NH}_3$	-14.3	-	-	-
Sr-R052	$1/2\text{SrHN} + \text{H}_2 = 1/2\text{SrH}_2 + 1/2\text{NH}_3$	-12.67	-	-	-
Sr-R053	$2/5\text{SrHN} + \text{H}_2 = 2/5\text{SrH}_3 + 2/5\text{NH}_3$	-11.68	-	-	-
Sr-R054	$2\text{SrHN} + \text{H}_2 = \text{Sr}_2\text{HN} + \text{NH}_3$	-7.31	-	-	-
Sr-R055	$4\text{SrHN} + \text{H}_2 = 2\text{Sr}_2\text{N} + 2\text{NH}_3$	-7.81	-	-	-
Sr-R056	$6\text{SrN} + \text{H}_2 = 2\text{Sr}_3\text{H} + 3\text{N}_2$	-13.45	-	-	-
Sr-R057	$\text{SrN} + \text{H}_2 = \text{SrH}_2 + 1/2\text{N}_2$	-11.8	-50.94	640.5	exergonic
Sr-R058	$2/3\text{SrN} + \text{H}_2 = 2/3\text{SrH}_3 + 1/3\text{N}_2$	-10.81	48.71	-	endergonic
Sr-R059	$4\text{SrN} + \text{H}_2 = 2\text{Sr}_2\text{HN} + \text{N}_2$	-6.4	-69.05	-	exergonic
Sr-R060	$2\text{SrN} + \text{H}_2 = 2\text{SrHN}$	0.99	-	-	-
Sr-R061	$2/3\text{SrN} + \text{H}_2 = 2/3\text{Sr} + 2/3\text{NH}_3$	-13.78	55.44	-	endergonic
Sr-R062	$3/5\text{SrN} + \text{H}_2 = 1/5\text{Sr}_3\text{H} + 3/5\text{NH}_3$	-13.45	-	-	-
Sr-R063	$2/5\text{SrN} + \text{H}_2 = 2/5\text{SrH}_2 + 2/5\text{NH}_3$	-11.8	-38.73	346.4	exergonic
Sr-R064	$1/3\text{SrN} + \text{H}_2 = 1/3\text{SrH}_3 + 1/3\text{NH}_3$	-10.81	9.06	-	endergonic
Sr-R065	$\text{SrN} + \text{H}_2 = 1/2\text{Sr}_2\text{HN} + 1/2\text{NH}_3$	-6.4	-40.21	716.8	exergonic
Sr-R066	$4/3\text{SrN} + \text{H}_2 = 2/3\text{Sr}_2\text{N} + 2/3\text{NH}_3$	-6.89	11.82	-	endergonic
Sr-R067	$2\text{SrN} + \text{H}_2 = 2/3\text{Sr}_3\text{N}_2 + 2/3\text{NH}_3$	-4.59	-33.29	322.9	exergonic
Sr-R068	$8/3\text{SrN} + \text{H}_2 = 2/3\text{Sr}_4\text{N}_3 + 2/3\text{NH}_3$	-3.45	-	-	-
Sr-R069	$6\text{SrN}_2 + \text{H}_2 = 2\text{Sr}_3\text{H} + 6\text{N}_2$	-23.94	-	-	-
Sr-R070	$\text{SrN}_2 + \text{H}_2 = \text{SrH}_2 + \text{N}_2$	-22.48	0.39	-	exergonic
Sr-R071	$2/3\text{SrN}_2 + \text{H}_2 = 2/3\text{SrH}_3 + 2/3\text{N}_2$	-21.61	82.93	-	endergonic
Sr-R072	$1/2\text{SrN}_2 + \text{H}_2 = 1/2\text{Sr}(\text{H}_2\text{N})_2$	3.49	-	-	-
Sr-R073	$4\text{SrN}_2 + \text{H}_2 = 2\text{Sr}_2\text{HN} + 3\text{N}_2$	-17.73	136.29	99.7	exergonic
Sr-R074	$2\text{SrN}_2 + \text{H}_2 = 2\text{SrHN} + \text{N}_2$	-11.24	-	-	-
Sr-R075	$1/3\text{SrN}_2 + \text{H}_2 = 1/3\text{Sr} + 2/3\text{NH}_3$	-24.23	29.53	-	endergonic
Sr-R076	$6/19\text{SrN}_2 + \text{H}_2 = 2/19\text{Sr}_3\text{H} + 12/19\text{NH}_3$	-23.94	-	-	-

Sr-R077	$1/4\text{SrN}_2 + \text{H}_2 = 1/4\text{SrH}_2 + 1/2\text{NH}_3$	-22.48	-22.85	241.3	exergonic
Sr-R078	$2/9\text{SrN}_2 + \text{H}_2 = 2/9\text{SrH}_3 + 4/9\text{NH}_3$	-21.61	7.25	-	endergonic
Sr-R079	$2/5\text{SrN}_2 + \text{H}_2 = 1/5\text{Sr}_2\text{HN} + 3/5\text{NH}_3$	-17.73	-13.91	278.6	exergonic
Sr-R080	$1/2\text{SrN}_2 + \text{H}_2 = 1/2\text{SrHN} + 1/2\text{NH}_3$	-11.24	-	-	-
Sr-R081	$4/9\text{SrN}_2 + \text{H}_2 = 2/9\text{Sr}_2\text{N} + 2/3\text{NH}_3$	-18.17	6.36	-	endergonic
Sr-R082	$1/2\text{SrN}_2 + \text{H}_2 = 1/6\text{Sr}_3\text{N}_2 + 2/3\text{NH}_3$	-16.15	-5.6	-	endergonic
Sr-R083	$8/15\text{SrN}_2 + \text{H}_2 = 2/15\text{Sr}_4\text{N}_3 + 2/3\text{NH}_3$	-15.14	-	-	-
Sr-R084	$2/3\text{SrN}_2 + \text{H}_2 = 2/3\text{SrN} + 2/3\text{NH}_3$	-12.11	3.63	-	endergonic
Sr-R085	$6\text{SrN}_6 + \text{H}_2 = 2\text{Sr}_3\text{H} + 18\text{N}_2$	-48.76	-	-	-
Sr-R086	$\text{SrN}_6 + \text{H}_2 = \text{SrH}_2 + 3\text{N}_2$	-47.78	-	-	-
Sr-R087	$2/3\text{SrN}_6 + \text{H}_2 = 2/3\text{SrH}_3 + 2\text{N}_2$	-47.2	-	-	-
Sr-R088	$1/2\text{SrN}_6 + \text{H}_2 = 1/2\text{Sr}(\text{H}_2\text{N})_2 + \text{N}_2$	-30.29	-	-	-
Sr-R089	$4\text{SrN}_6 + \text{H}_2 = 2\text{Sr}_2\text{HN} + 11\text{N}_2$	-44.58	-	-	-
Sr-R090	$2\text{SrN}_6 + \text{H}_2 = 2\text{SrHN} + 5\text{N}_2$	-40.21	-	-	-
Sr-R091	$1/9\text{SrN}_6 + \text{H}_2 = 1/9\text{Sr} + 2/3\text{NH}_3$	-48.96	-	-	-
Sr-R092	$6/55\text{SrN}_6 + \text{H}_2 = 2/55\text{Sr}_3\text{H} + 36/55\text{NH}_3$	-48.76	-	-	-
Sr-R093	$1/10\text{SrN}_6 + \text{H}_2 = 1/10\text{SrH}_2 + 3/5\text{NH}_3$	-47.78	-	-	-
Sr-R094	$2/21\text{SrN}_6 + \text{H}_2 = 2/21\text{SrH}_3 + 4/7\text{NH}_3$	-47.2	-	-	-
Sr-R095	$1/8\text{SrN}_6 + \text{H}_2 = 1/8\text{Sr}(\text{H}_2\text{N})_2 + 1/2\text{NH}_3$	-30.29	-	-	-
Sr-R096	$2/17\text{SrN}_6 + \text{H}_2 = 1/17\text{Sr}_2\text{HN} + 11/17\text{NH}_3$	-44.58	-	-	-
Sr-R097	$1/8\text{SrN}_6 + \text{H}_2 = 1/8\text{SrHN} + 5/8\text{NH}_3$	-40.21	-	-	-
Sr-R098	$4/33\text{SrN}_6 + \text{H}_2 = 2/33\text{Sr}_2\text{N} + 2/3\text{NH}_3$	-44.88	-	-	-
Sr-R099	$1/8\text{SrN}_6 + \text{H}_2 = 1/24\text{Sr}_3\text{N}_2 + 2/3\text{NH}_3$	-43.52	-	-	-
Sr-R100	$8/63\text{SrN}_6 + \text{H}_2 = 2/63\text{Sr}_4\text{N}_3 + 2/3\text{NH}_3$	-42.84	-	-	-
Sr-R101	$2/15\text{SrN}_6 + \text{H}_2 = 2/15\text{SrN} + 2/3\text{NH}_3$	-40.8	-	-	-
Sr-R102	$1/6\text{SrN}_6 + \text{H}_2 = 1/6\text{SrN}_2 + 2/3\text{NH}_3$	-32.64	-	-	-
Sr-R103	$4\text{Sr} + \text{N}_2 = 2\text{Sr}_2\text{N}$	7.99	-388.99	-	exergonic
Sr-R104	$3\text{Sr} + \text{N}_2 = \text{Sr}_3\text{N}_2$	10.66	-391.21	-	exergonic
Sr-R105	$8/3\text{Sr} + \text{N}_2 = 2/3\text{Sr}_4\text{N}_3$	11.99	-	-	-
Sr-R106	$2\text{Sr} + \text{N}_2 = 2\text{SrN}$	15.99	-258.12	-	exergonic
Sr-R107	$\text{Sr} + \text{N}_2 = \text{SrN}_2$	31.97	-180.39	-	exergonic
Sr-R108	$1/3\text{Sr} + \text{N}_2 = 1/3\text{SrN}_6$	95.92	-	-	-
Sr-R109	$1/2\text{Sr}(\text{H}_2\text{N})_2 + \text{N}_2 = 1/2\text{SrN}_6 + \text{H}_2$	43.45	-	-	-
Sr-R110	$24\text{Sr}(\text{H}_2\text{N})_2 + \text{N}_2 = 6\text{Sr}_4\text{N}_3 + 32\text{NH}_3$	-18	-	-	-
Sr-R111	$6\text{Sr}(\text{H}_2\text{N})_2 + \text{N}_2 = 6\text{SrN} + 8\text{NH}_3$	-15.07	-	-	-
Sr-R112	$3/2\text{Sr}(\text{H}_2\text{N})_2 + \text{N}_2 = 3/2\text{SrN}_2 + 2\text{NH}_3$	-3.37	-	-	-
Sr-R113	$3/8\text{Sr}(\text{H}_2\text{N})_2 + \text{N}_2 = 3/8\text{SrN}_6 + 1/2\text{NH}_3$	43.45	-	-	-
Sr-R114	$6\text{Sr}_2\text{HN} + \text{N}_2 = 4\text{Sr}_3\text{N}_2 + 3\text{H}_2$	1.92	191.01	-	endergonic
Sr-R115	$4\text{Sr}_2\text{HN} + \text{N}_2 = 2\text{Sr}_4\text{N}_3 + 2\text{H}_2$	3.15	-	-	-
Sr-R116	$2\text{Sr}_2\text{HN} + \text{N}_2 = 4\text{SrN} + \text{H}_2$	6.83	69.05	-	endergonic
Sr-R117	$2/3\text{Sr}_2\text{HN} + \text{N}_2 = 4/3\text{SrN}_2 + 1/3\text{H}_2$	21.56	-45.43	99.7	exergonic
Sr-R118	$2/11\text{Sr}_2\text{HN} + \text{N}_2 = 4/11\text{SrN}_6 + 1/11\text{H}_2$	80.45	-	-	-
Sr-R119	$6\text{Sr}_2\text{HN} + \text{N}_2 = 6\text{Sr}_2\text{N} + 2\text{NH}_3$	-0.53	497.08	-	endergonic
Sr-R120	$3\text{Sr}_2\text{HN} + \text{N}_2 = 2\text{Sr}_3\text{N}_2 + \text{NH}_3$	1.92	49.61	-	endergonic
Sr-R121	$12/5\text{Sr}_2\text{HN} + \text{N}_2 = 6/5\text{Sr}_4\text{N}_3 + 4/5\text{NH}_3$	3.15	-	-	-
Sr-R122	$3/2\text{Sr}_2\text{HN} + \text{N}_2 = 3\text{SrN} + 1/2\text{NH}_3$	6.83	28.84	-	endergonic
Sr-R123	$3/5\text{Sr}_2\text{HN} + \text{N}_2 = 6/5\text{SrN}_2 + 1/5\text{NH}_3$	21.56	-50.07	113.3	exergonic
Sr-R124	$3/17\text{Sr}_2\text{HN} + \text{N}_2 = 6/17\text{SrN}_6 + 1/17\text{NH}_3$	80.45	-	-	-
Sr-R125	$6\text{Sr}_2\text{N} + \text{N}_2 = 4\text{Sr}_3\text{N}_2$	2.47	-397.86	506.1	exergonic



Sr-R126	$4\text{Sr}_2\text{N} + \text{N}_2 = 2\text{Sr}_4\text{N}_3$	3.7	-	-	-
Sr-R127	$2\text{Sr}_2\text{N} + \text{N}_2 = 4\text{SrN}$	7.4	-127.24	368.5	exergonic
Sr-R128	$2/3\text{Sr}_2\text{N} + \text{N}_2 = 4/3\text{SrN}_2$	22.2	-110.86	387.7	exergonic
Sr-R129	$2/11\text{Sr}_2\text{N} + \text{N}_2 = 4/11\text{SrN}_6$	81.42	-	-	-
Sr-R130	$4/3\text{Sr}_3\text{H} + \text{N}_2 = 2\text{Sr}_2\text{N} + 2/3\text{H}_2$	7.58	-	-	-
Sr-R131	$\text{Sr}_3\text{H} + \text{N}_2 = \text{Sr}_3\text{N}_2 + 1/2\text{H}_2$	10.23	-	-	-
Sr-R132	$8/9\text{Sr}_3\text{H} + \text{N}_2 = 2/3\text{Sr}_4\text{N}_3 + 4/9\text{H}_2$	11.56	-	-	-
Sr-R133	$2/3\text{Sr}_3\text{H} + \text{N}_2 = 2\text{SrN} + 1/3\text{H}_2$	15.54	-	-	-
Sr-R134	$1/3\text{Sr}_3\text{H} + \text{N}_2 = \text{SrN}_2 + 1/6\text{H}_2$	31.47	-	-	-
Sr-R135	$1/9\text{Sr}_3\text{H} + \text{N}_2 = 1/3\text{SrN}_6 + 1/18\text{H}_2$	95.17	-	-	-
Sr-R136	$6\text{Sr}_3\text{H} + \text{N}_2 = 18\text{Sr} + 2\text{NH}_3$	-0.38	-	-	-
Sr-R137	$12/11\text{Sr}_3\text{H} + \text{N}_2 = 18/11\text{Sr}_2\text{N} + 4/11\text{NH}_3$	7.58	-	-	-
Sr-R138	$6/7\text{Sr}_3\text{H} + \text{N}_2 = 6/7\text{Sr}_3\text{N}_2 + 2/7\text{NH}_3$	10.23	-	-	-
Sr-R139	$24/31\text{Sr}_3\text{H} + \text{N}_2 = 18/31\text{Sr}_4\text{N}_3 + 8/31\text{NH}_3$	11.56	-	-	-
Sr-R140	$3/5\text{Sr}_3\text{H} + \text{N}_2 = 9/5\text{SrN} + 1/5\text{NH}_3$	15.54	-	-	-
Sr-R141	$6/19\text{Sr}_3\text{H} + \text{N}_2 = 18/19\text{SrN}_2 + 2/19\text{NH}_3$	31.47	-	-	-
Sr-R142	$6/55\text{Sr}_3\text{H} + \text{N}_2 = 18/55\text{SrN}_6 + 2/55\text{NH}_3$	95.17	-	-	-
Sr-R143	$8\text{Sr}_3\text{N}_2 + \text{N}_2 = 6\text{Sr}_4\text{N}_3$	1.2	-	-	-
Sr-R144	$2\text{Sr}_3\text{N}_2 + \text{N}_2 = 6\text{SrN}$	4.82	8.07	-	endergonic
Sr-R145	$1/2\text{Sr}_3\text{N}_2 + \text{N}_2 = 3/2\text{SrN}_2$	19.26	-74.99	328.3	exergonic
Sr-R146	$1/8\text{Sr}_3\text{N}_2 + \text{N}_2 = 3/8\text{SrN}_6$	77.05	-	-	-
Sr-R147	$2\text{Sr}_4\text{N}_3 + \text{N}_2 = 8\text{SrN}$	3.57	-	-	-
Sr-R148	$2/5\text{Sr}_4\text{N}_3 + \text{N}_2 = 8/5\text{SrN}_2$	17.84	-	-	-
Sr-R149	$2/21\text{Sr}_4\text{N}_3 + \text{N}_2 = 8/21\text{SrN}_6$	74.94	-	-	-
Sr-R150	$4\text{SrH}_2 + \text{N}_2 = 2\text{Sr}_2\text{HN} + 3\text{H}_2$	6.13	134.72	244.9	exergonic
Sr-R151	$2\text{SrH}_2 + \text{N}_2 = 2\text{SrHN} + \text{H}_2$	14.5	-	-	-
Sr-R152	$4\text{SrH}_2 + \text{N}_2 = 2\text{Sr}_2\text{N} + 4\text{H}_2$	5.56	331.01	523.4	exergonic
Sr-R153	$3\text{SrH}_2 + \text{N}_2 = \text{Sr}_3\text{N}_2 + 3\text{H}_2$	8.17	148.79	533.1	exergonic
Sr-R154	$8/3\text{SrH}_2 + \text{N}_2 = 2/3\text{Sr}_4\text{N}_3 + 8/3\text{H}_2$	9.47	-	-	-
Sr-R155	$2\text{SrH}_2 + \text{N}_2 = 2\text{SrN} + 2\text{H}_2$	13.38	101.88	640.5	exergonic
Sr-R156	$\text{SrH}_2 + \text{N}_2 = \text{SrN}_2 + \text{H}_2$	29	-0.39	-	endergonic
Sr-R157	$1/3\text{SrH}_2 + \text{N}_2 = 1/3\text{SrN}_6 + 1/3\text{H}_2$	91.51	-	-	-
Sr-R158	$3\text{SrH}_2 + \text{N}_2 = 3\text{Sr} + 2\text{NH}_3$	-2.25	448.2	-	endergonic
Sr-R159	$18/5\text{SrH}_2 + \text{N}_2 = 6/5\text{Sr}_3\text{H} + 2\text{NH}_3$	-1.87	-	-	-
Sr-R160	$2\text{SrH}_2 + \text{N}_2 = \text{Sr}_2\text{HN} + \text{NH}_3$	6.13	21.46	442.9	exergonic
Sr-R161	$3/2\text{SrH}_2 + \text{N}_2 = 3/2\text{SrHN} + 1/2\text{NH}_3$	14.5	-	-	-
Sr-R162	$12/7\text{SrH}_2 + \text{N}_2 = 6/7\text{Sr}_2\text{N} + 8/7\text{NH}_3$	5.56	89.41	-	endergonic
Sr-R163	$3/2\text{SrH}_2 + \text{N}_2 = 1/2\text{Sr}_3\text{N}_2 + \text{NH}_3$	8.17	28.5	-	endergonic
Sr-R164	$24/17\text{SrH}_2 + \text{N}_2 = 6/17\text{Sr}_4\text{N}_3 + 16/17\text{NH}_3$	9.47	-	-	-
Sr-R165	$6/5\text{SrH}_2 + \text{N}_2 = 6/5\text{SrN} + 4/5\text{NH}_3$	13.38	24.41	-	endergonic
Sr-R166	$3/4\text{SrH}_2 + \text{N}_2 = 3/4\text{SrN}_2 + 1/2\text{NH}_3$	29	-23.24	54.3	exergonic
Sr-R167	$3/10\text{SrH}_2 + \text{N}_2 = 3/10\text{SrN}_6 + 1/5\text{NH}_3$	91.51	-	-	-
Sr-R168	$4\text{SrH}_3 + \text{N}_2 = 2\text{Sr}_2\text{HN} + 5\text{H}_2$	4.95	-361.3	-	exergonic
Sr-R169	$2\text{SrH}_3 + \text{N}_2 = 2\text{SrHN} + 2\text{H}_2$	13.23	-	-	-
Sr-R170	$4\text{SrH}_3 + \text{N}_2 = 2\text{Sr}_2\text{N} + 6\text{H}_2$	4.39	-165	-	exergonic
Sr-R171	$3\text{SrH}_3 + \text{N}_2 = \text{Sr}_3\text{N}_2 + 9/2\text{H}_2$	6.97	-223.22	-	exergonic
Sr-R172	$8/3\text{SrH}_3 + \text{N}_2 = 2/3\text{Sr}_4\text{N}_3 + 4\text{H}_2$	8.25	-	-	-
Sr-R173	$2\text{SrH}_3 + \text{N}_2 = 2\text{SrN} + 3\text{H}_2$	12.12	-146.12	-	exergonic
Sr-R174	$\text{SrH}_3 + \text{N}_2 = \text{SrN}_2 + 3/2\text{H}_2$	27.57	-124.4	-	exergonic

Sr-R175	$1/3\text{SrH}_3 + \text{N}_2 = 1/3\text{SrN}_6 + 1/2\text{H}_2$	89.38	-	-	-
Sr-R176	$2\text{SrH}_3 + \text{N}_2 = 2\text{Sr} + 2\text{NH}_3$	-3.34	20.2	-	exergonic
Sr-R177	$9/4\text{SrH}_3 + \text{N}_2 = 3/4\text{Sr}_3\text{H} + 2\text{NH}_3$	-2.97	-	-	-
Sr-R178	$6\text{SrH}_3 + \text{N}_2 = 6\text{SrH}_2 + 2\text{NH}_3$	-1.11	-835.81	-	exergonic
Sr-R179	$3/2\text{SrH}_3 + \text{N}_2 = 3/4\text{Sr}_2\text{HN} + 5/4\text{NH}_3$	4.95	-192.86	-	exergonic
Sr-R180	$6/5\text{SrH}_3 + \text{N}_2 = 6/5\text{SrHN} + 4/5\text{NH}_3$	13.23	-	-	-
Sr-R181	$4/3\text{SrH}_3 + \text{N}_2 = 2/3\text{Sr}_2\text{N} + 4/3\text{NH}_3$	4.39	-116.2	-	exergonic
Sr-R182	$6/5\text{SrH}_3 + \text{N}_2 = 2/5\text{Sr}_3\text{N}_2 + 6/5\text{NH}_3$	6.97	-144.36	-	exergonic
Sr-R183	$8/7\text{SrH}_3 + \text{N}_2 = 2/7\text{Sr}_4\text{N}_3 + 8/7\text{NH}_3$	8.25	-	-	-
Sr-R184	$\text{SrH}_3 + \text{N}_2 = \text{SrN} + \text{NH}_3$	12.12	-118.96	-	exergonic
Sr-R185	$2/3\text{SrH}_3 + \text{N}_2 = 2/3\text{SrN}_2 + 2/3\text{NH}_3$	27.57	-113.53	-	exergonic
Sr-R186	$2/7\text{SrH}_3 + \text{N}_2 = 2/7\text{SrN}_6 + 2/7\text{NH}_3$	89.38	-	-	-
Sr-R187	$2\text{SrHN} + \text{N}_2 = 2\text{SrN}_2 + \text{H}_2$	12.67	-	-	-
Sr-R188	$2/5\text{SrHN} + \text{N}_2 = 2/5\text{SrN}_6 + 1/5\text{H}_2$	67.25	-	-	-
Sr-R189	$24\text{SrHN} + \text{N}_2 = 6\text{Sr}_4\text{N}_3 + 8\text{NH}_3$	-4.39	-	-	-
Sr-R190	$6\text{SrHN} + \text{N}_2 = 6\text{SrN} + 2\text{NH}_3$	-0.98	-	-	-
Sr-R191	$3/2\text{SrHN} + \text{N}_2 = 3/2\text{SrN}_2 + 1/2\text{NH}_3$	12.67	-	-	-
Sr-R192	$3/8\text{SrHN} + \text{N}_2 = 3/8\text{SrN}_6 + 1/8\text{NH}_3$	67.25	-	-	-
Sr-R193	$2\text{SrN} + \text{N}_2 = 2\text{SrN}_2$	13.78	-102.67	400.4	exergonic
Sr-R194	$2/5\text{SrN} + \text{N}_2 = 2/5\text{SrN}_6$	68.91	-	-	-
Sr-R195	$1/2\text{SrN}_2 + \text{N}_2 = 1/2\text{SrN}_6$	48.45	-	-	-

Table S25: The W-based system

ID	Reaction	dm_stoich [%]	h298 [kJ/mol]	T_eq [°C]	Type
W-R01	$2/3\text{W}_2\text{N} + \text{H}_2 = 4/3\text{W} + 2/3\text{NH}_3$	-3.67	64.06	-	endergonic
W-R02	$2/9\text{W}_2\text{N}_3 + \text{H}_2 = 4/9\text{W} + 2/3\text{NH}_3$	-10.26	-	-	-
W-R03	$1/3\text{W}_2\text{N}_3 + \text{H}_2 = 1/3\text{W}_2\text{N} + 2/3\text{NH}_3$	-6.84	-	-	-
W-R04	$2\text{W}_2\text{N}_3 + \text{H}_2 = 4/3\text{W}_3\text{N}_4 + 2/3\text{NH}_3$	-1.14	-	-	-
W-R05	$14/27\text{W}_2\text{N}_3 + \text{H}_2 = 4/27\text{W}_7\text{N}_6 + 2/3\text{NH}_3$	-4.4	-	-	-
W-R06	$2/3\text{W}_2\text{N}_3 + \text{H}_2 = 4/3\text{WN} + 2/3\text{NH}_3$	-3.42	-	-	-
W-R07	$1/6\text{W}_3\text{N}_4 + \text{H}_2 = 1/2\text{W} + 2/3\text{NH}_3$	-9.22	-11.95	240.2	exergonic
W-R08	$4/15\text{W}_3\text{N}_4 + \text{H}_2 = 2/5\text{W}_2\text{N} + 2/3\text{NH}_3$	-5.76	-57.55	-	exergonic
W-R09	$7/15\text{W}_3\text{N}_4 + \text{H}_2 = 1/5\text{W}_7\text{N}_6 + 2/3\text{NH}_3$	-3.29	-	-	-
W-R10	$2/3\text{W}_3\text{N}_4 + \text{H}_2 = 2\text{WN} + 2/3\text{NH}_3$	-2.31	-23.97	164.7	exergonic
W-R11	$1/9\text{W}_7\text{N}_6 + \text{H}_2 = 7/9\text{W} + 2/3\text{NH}_3$	-6.13	-	-	-
W-R12	$4/15\text{W}_7\text{N}_6 + \text{H}_2 = 14/15\text{W}_2\text{N} + 2/3\text{NH}_3$	-2.55	-	-	-
W-R13	$2/3\text{WN} + \text{H}_2 = 2/3\text{W} + 2/3\text{NH}_3$	-7.08	-7.94	318.2	exergonic
W-R14	$4/3\text{WN} + \text{H}_2 = 2/3\text{W}_2\text{N} + 2/3\text{NH}_3$	-3.54	-79.94	-	exergonic
W-R15	$14/3\text{WN} + \text{H}_2 = 2/3\text{W}_7\text{N}_6 + 2/3\text{NH}_3$	-1.01	-	-	-
W-R16	$1/27\text{WN}_18 + \text{H}_2 = 1/27\text{W} + 2/3\text{NH}_3$	-57.83	-	-	-
W-R17	$4/105\text{WN}_18 + \text{H}_2 = 2/105\text{W}_2\text{N} + 2/3\text{NH}_3$	-56.23	-	-	-
W-	$4/99\text{WN}_18 + \text{H}_2 = 2/99\text{W}_2\text{N}_3 + 2/3\text{NH}_3$	-53.01	-	-	-

R18					
W-R19	$1/25WN18 + H2 = 1/75W3N4 + 2/3NH3$	-53.55	-	-	-
W-R20	$7/180WN18 + H2 = 1/180W7N6 + 2/3NH3$	-55.08	-	-	-
W-R21	$2/51WN18 + H2 = 2/51WN + 2/3NH3$	-54.62	-	-	-
W-R22	$1/24WN18 + H2 = 1/24WN2 + 2/3NH3$	-51.41	-	-	-
W-R23	$1/18WN18 + H2 = 1/18WN6 + 2/3NH3$	-38.55	-	-	-
W-R24	$1/3WN2 + H2 = 1/3W + 2/3NH3$	-13.22	8.12	-	endergonic
W-R25	$4/9WN2 + H2 = 2/9W2N + 2/3NH3$	-9.92	-10.53	103.7	exergonic
W-R26	$4/3WN2 + H2 = 2/3W2N3 + 2/3NH3$	-3.31	-	-	-
W-R27	$WN2 + H2 = 1/3W3N4 + 2/3NH3$	-4.41	48.25	-	endergonic
W-R28	$7/12WN2 + H2 = 1/12W7N6 + 2/3NH3$	-7.56	-	-	-
W-R29	$2/3WN2 + H2 = 2/3WN + 2/3NH3$	-6.61	24.17	-	endergonic
W-R30	$1/9WN6 + H2 = 1/9W + 2/3NH3$	-31.37	-	-	-
W-R31	$4/33WN6 + H2 = 2/33W2N + 2/3NH3$	-28.76	-	-	-
W-R32	$4/27WN6 + H2 = 2/27W2N3 + 2/3NH3$	-23.53	-	-	-
W-R33	$1/7WN6 + H2 = 1/21W3N4 + 2/3NH3$	-24.4	-	-	-
W-R34	$7/54WN6 + H2 = 1/54W7N6 + 2/3NH3$	-26.89	-	-	-
W-R35	$2/15WN6 + H2 = 2/15WN + 2/3NH3$	-26.14	-	-	-
W-R36	$1/6WN6 + H2 = 1/6WN2 + 2/3NH3$	-20.92	-	-	-
W-R37	$4W + N2 = 2W2N$	3.81	-283.98	-	exergonic
W-R38	$4/3W + N2 = 2/3W2N3$	11.43	-	-	-
W-R39	$3/2W + N2 = 1/2W3N4$	10.16	-55.95	142.3	exergonic
W-R40	$7/3W + N2 = 1/3W7N6$	6.53	-	-	-
W-R41	$2W + N2 = 2WN$	7.62	-67.97	133.2	exergonic
W-R42	$1/9W + N2 = 1/9WN18$	137.14	-	-	-
W-R43	$W + N2 = WN2$	15.24	-116.14	-	exergonic
W-R44	$1/3W + N2 = 1/3WN6$	45.71	-	-	-
W-R45	$W2N + N2 = W2N3$	7.34	-	-	-
W-R46	$6/5W2N + N2 = 4/5W3N4$	6.12	80.87	-	endergonic
W-R47	$14/5W2N + N2 = 4/5W7N6$	2.62	-	-	-
W-R48	$2W2N + N2 = 4WN$	3.67	148.03	-	endergonic
W-R49	$2/35W2N + N2 = 4/35WN18$	128.44	-	-	-
W-R50	$2/3W2N + N2 = 4/3WN2$	11.01	-60.2	298.1	exergonic
W-R51	$2/11W2N + N2 = 4/11WN6$	40.37	-	-	-
W-R52	$2/33W2N3 + N2 = 4/33WN18$	112.82	-	-	-
W-R53	$2W2N3 + N2 = 4WN2$	3.42	-	-	-

W-R54	$2/9W2N3 + N2 = 4/9WN6$	30.77	-	-	-
W-R55	$4W3N4 + N2 = 6W2N3$	1.15	-	-	-
W-R56	$1/25W3N4 + N2 = 3/25WN18$	115.27	-	-	-
W-R57	$W3N4 + N2 = 3WN2$	4.61	-236.53	-	exergonic
W-R58	$1/7W3N4 + N2 = 3/7WN6$	32.28	-	-	-
W-R59	$4/9W7N6 + N2 = 14/9W2N3$	4.6	-	-	-
W-R60	$3/5W7N6 + N2 = 7/5W3N4$	3.41	-	-	-
W-R61	$2W7N6 + N2 = 14WN$	1.02	-	-	-
W-R62	$1/60W7N6 + N2 = 7/60WN18$	122.61	-	-	-
W-R63	$1/4W7N6 + N2 = 7/4WN2$	8.17	-	-	-
W-R64	$1/18W7N6 + N2 = 7/18WN6$	36.78	-	-	-
W-R65	$4WN + N2 = 2W2N3$	3.54	-	-	-
W-R66	$6WN + N2 = 2W3N4$	2.36	-19.88	338.5	exergonic
W-R67	$2/17WN + N2 = 2/17WN18$	120.36	-	-	-
W-R68	$2WN + N2 = 2WN2$	7.08	-164.31	-	exergonic
W-R69	$2/5WN + N2 = 2/5WN6$	35.4	-	-	-
W-R70	$1/8WN2 + N2 = 1/8WN18$	105.79	-	-	-
W-R71	$1/2WN2 + N2 = 1/2WN6$	26.45	-	-	-
W-R72	$1/6WN6 + N2 = 1/6WN18$	62.75	-	-	-

Table S26: The Zn-based system

ID	Reaction	dm_stoich [%]	h298 [kJ/mol]	T_eq [°C]	Type
Zn-R01	$2Zn + H2 = 2ZnH$	1.54	-	-	-
Zn-R02	$1/3Zn + H2 = 1/3ZnH6$	9.25	-	-	-
Zn-R03	$1/9Zn(H15N8)2 + H2 = 1/9Zn + 16/9NH3$	-79.55	-	-	-
Zn-R04	$2/19Zn(H15N8)2 + H2 = 2/19ZnH + 32/19NH3$	-79.24	-	-	-
Zn-R05	$1/12Zn(H15N8)2 + H2 = 1/12ZnH6 + 4/3NH3$	-77.66	-	-	-
Zn-R06	$1/8Zn(H15N8)2 + H2 = 1/8Zn(H2N)2 + 7/4NH3$	-69.53	-	-	-
Zn-R07	$2/17Zn(H15N8)2 + H2 = 2/51Zn3N + 94/51NH3$	-78.09	-	-	-
Zn-R08	$1/8Zn(H15N8)2 + H2 = 1/24Zn3N2 + 23/12NH3$	-76.63	-	-	-
Zn-R09	$2/15Zn(H15N8)2 + H2 = 2/15ZnN + 2NH3$	-75.17	-	-	-
Zn-R10	Improbable stoichiometric coefficients	-53.27	-	-	-
Zn-R11	$Zn(H2N)2 + H2 = ZnH6 + N2$	-26.68	-	-	-
Zn-R12	$Zn(H2N)2 + H2 = Zn + 2NH3$	-32.89	-	-	-
Zn-R13	$2/3Zn(H2N)2 + H2 = 2/3ZnH + 4/3NH3$	-31.86	-	-	-
Zn-R14	$1/4Zn(H2N)2 + H2 = 1/4ZnH6 + 1/2NH3$	-26.68	-	-	-

Zn-R15	$2\text{Zn}(\text{H}_2\text{N})_2 + \text{H}_2 = 2/3\text{Zn}_3\text{N} + 10/3\text{NH}_3$	-28.1	-	-	-
Zn-R16	$1/11\text{Zn}(\text{H}_4\text{N}_5)_2 + \text{H}_2 = 1/11\text{Zn} + 10/11\text{NH}_3$	-69.38	-	-	-
Zn-R17	$2/23\text{Zn}(\text{H}_4\text{N}_5)_2 + \text{H}_2 = 2/23\text{ZnH} + 20/23\text{NH}_3$	-68.91	-	-	-
Zn-R18	$1/14\text{Zn}(\text{H}_4\text{N}_5)_2 + \text{H}_2 = 1/14\text{ZnH}_6 + 5/7\text{NH}_3$	-66.55	-	-	-
Zn-R19	$1/10\text{Zn}(\text{H}_4\text{N}_5)_2 + \text{H}_2 = 1/10\text{Zn}(\text{H}_2\text{N})_2 + 4/5\text{NH}_3$	-54.37	-	-	-
Zn-R20	$2/21\text{Zn}(\text{H}_4\text{N}_5)_2 + \text{H}_2 = 2/63\text{Zn}_3\text{N} + 58/63\text{NH}_3$	-67.19	-	-	-
Zn-R21	$1/10\text{Zn}(\text{H}_4\text{N}_5)_2 + \text{H}_2 = 1/30\text{Zn}_3\text{N}_2 + 14/15\text{NH}_3$	-65.01	-	-	-
Zn-R22	$2/19\text{Zn}(\text{H}_4\text{N}_5)_2 + \text{H}_2 = 2/19\text{ZnN} + 18/19\text{NH}_3$	-62.82	-	-	-
Zn-R23	$1/2\text{Zn}(\text{H}_4\text{N}_5)_2 + \text{H}_2 = 1/2\text{ZnN}_6 + 2\text{NH}_3$	-30.02	-	-	-
Zn-R24	$2/3\text{Zn}_3\text{N} + \text{H}_2 = 2\text{ZnH} + 1/3\text{N}_2$	-5.23	-	-	-
Zn-R25	$1/9\text{Zn}_3\text{N} + \text{H}_2 = 1/3\text{ZnH}_6 + 1/18\text{N}_2$	1.97	-	-	-
Zn-R26	$2/3\text{Zn}_3\text{N} + \text{H}_2 = 2\text{Zn} + 2/3\text{NH}_3$	-6.67	-	-	-
Zn-R27	$1/3\text{Zn}_3\text{N} + \text{H}_2 = \text{ZnH} + 1/3\text{NH}_3$	-5.23	-	-	-
Zn-R28	$2/21\text{Zn}_3\text{N} + \text{H}_2 = 2/7\text{ZnH}_6 + 2/21\text{NH}_3$	1.97	-	-	-
Zn-R29	$2/3\text{Zn}_3\text{N}_2 + \text{H}_2 = 2\text{ZnH} + 2/3\text{N}_2$	-11.15	-	-	-
Zn-R30	$1/9\text{Zn}_3\text{N}_2 + \text{H}_2 = 1/3\text{ZnH}_6 + 1/9\text{N}_2$	-4.4	-	-	-
Zn-R31	$1/3\text{Zn}_3\text{N}_2 + \text{H}_2 = \text{Zn} + 2/3\text{NH}_3$	-12.5	-23.21	-	exergonic
Zn-R32	$2/9\text{Zn}_3\text{N}_2 + \text{H}_2 = 2/3\text{ZnH} + 4/9\text{NH}_3$	-11.15	-	-	-
Zn-R33	$1/12\text{Zn}_3\text{N}_2 + \text{H}_2 = 1/4\text{ZnH}_6 + 1/6\text{NH}_3$	-4.4	-	-	-
Zn-R34	$2/3\text{Zn}_3\text{N}_2 + \text{H}_2 = 2/3\text{Zn}_3\text{N} + 2/3\text{NH}_3$	-6.25	-	-	-
Zn-R35	$2/5\text{ZnH} + \text{H}_2 = 2/5\text{ZnH}_6$	7.59	-	-	-
Zn-R36	$2\text{ZnN} + \text{H}_2 = 2\text{ZnH} + \text{N}_2$	-16.37	-	-	-
Zn-R37	$1/3\text{ZnN} + \text{H}_2 = 1/3\text{ZnH}_6 + 1/6\text{N}_2$	-10.03	-	-	-
Zn-R38	$2/3\text{ZnN} + \text{H}_2 = 2/3\text{Zn} + 2/3\text{NH}_3$	-17.64	-97.49	-	exergonic
Zn-R39	$1/2\text{ZnN} + \text{H}_2 = 1/2\text{ZnH} + 1/2\text{NH}_3$	-16.37	-	-	-
Zn-R40	$2/9\text{ZnN} + \text{H}_2 = 2/9\text{ZnH}_6 + 2/9\text{NH}_3$	-10.03	-	-	-
Zn-R41	$\text{ZnN} + \text{H}_2 = 1/3\text{Zn}_3\text{N} + 2/3\text{NH}_3$	-11.76	-	-	-
Zn-R42	$2\text{ZnN} + \text{H}_2 = 2/3\text{Zn}_3\text{N}_2 + 2/3\text{NH}_3$	-5.88	-246.07	-	exergonic
Zn-R43	$2\text{ZnN}_6 + \text{H}_2 = 2\text{ZnH} + 6\text{N}_2$	-55.57	-	-	-
Zn-R44	$1/3\text{ZnN}_6 + \text{H}_2 = 1/3\text{ZnH}_6 + \text{N}_2$	-52.2	-	-	-
Zn-R45	$1/2\text{ZnN}_6 + \text{H}_2 = 1/2\text{Zn}(\text{H}_2\text{N})_2 + \text{N}_2$	-34.8	-	-	-
Zn-R46	$1/9\text{ZnN}_6 + \text{H}_2 = 1/9\text{Zn} + 2/3\text{NH}_3$	-56.24	-	-	-
Zn-R47	$2/19\text{ZnN}_6 + \text{H}_2 = 2/19\text{ZnH} + 12/19\text{NH}_3$	-55.57	-	-	-
Zn-R48	$1/12\text{ZnN}_6 + \text{H}_2 = 1/12\text{ZnH}_6 + 1/2\text{NH}_3$	-52.2	-	-	-
Zn-R49	$1/8\text{ZnN}_6 + \text{H}_2 = 1/8\text{Zn}(\text{H}_2\text{N})_2 + 1/2\text{NH}_3$	-34.8	-	-	-
Zn-R50	$2/17\text{ZnN}_6 + \text{H}_2 = 2/51\text{Zn}_3\text{N} + 2/3\text{NH}_3$	-53.12	-	-	-

Zn-R51	$1/8\text{ZnN}_6 + \text{H}_2 = 1/24\text{Zn}_3\text{N}_2 + 2/3\text{NH}_3$	-50	-	-	-
Zn-R52	$2/15\text{ZnN}_6 + \text{H}_2 = 2/15\text{ZnN} + 2/3\text{NH}_3$	-46.87	-	-	-
Zn-R53	$6\text{Zn} + \text{N}_2 = 2\text{Zn}_3\text{N}$	7.14	-	-	-
Zn-R54	$3\text{Zn} + \text{N}_2 = \text{Zn}_3\text{N}_2$	14.28	-22.17	-	endergonic
Zn-R55	$2\text{Zn} + \text{N}_2 = 2\text{ZnN}$	21.42	200.69	-	endergonic
Zn-R56	$1/3\text{Zn} + \text{N}_2 = 1/3\text{ZnN}_6$	128.54	-	-	-
Zn-R57	$3/2\text{Zn}(\text{H}_15\text{N}_8)_2 + \text{N}_2 = 3/2\text{Zn}(\text{H}_4\text{N}_5)_2 + 11\text{NH}_3$	-33.22	-	-	-
Zn-R58	$1/2\text{Zn}(\text{H}_2\text{N})_2 + \text{N}_2 = 1/2\text{ZnN}_6 + \text{H}_2$	53.37	-	-	-
Zn-R59	$6\text{Zn}(\text{H}_2\text{N})_2 + \text{N}_2 = 6\text{ZnN} + 8\text{NH}_3$	-18.52	-	-	-
Zn-R60	$3/8\text{Zn}(\text{H}_2\text{N})_2 + \text{N}_2 = 3/8\text{ZnN}_6 + 1/2\text{NH}_3$	53.37	-	-	-
Zn-R61	$2\text{Zn}_3\text{N} + \text{N}_2 = 2\text{Zn}_3\text{N}_2$	6.67	-	-	-
Zn-R62	$\text{Zn}_3\text{N} + \text{N}_2 = 3\text{ZnN}$	13.33	-	-	-
Zn-R63	$2/17\text{Zn}_3\text{N} + \text{N}_2 = 6/17\text{ZnN}_6$	113.31	-	-	-
Zn-R64	$2\text{Zn}_3\text{N}_2 + \text{N}_2 = 6\text{ZnN}$	6.25	646.42	-	endergonic
Zn-R65	$1/8\text{Zn}_3\text{N}_2 + \text{N}_2 = 3/8\text{ZnN}_6$	99.98	-	-	-
Zn-R66	$6\text{ZnH} + \text{N}_2 = 2\text{Zn}_3\text{N} + 3\text{H}_2$	5.51	-	-	-
Zn-R67	$3\text{ZnH} + \text{N}_2 = \text{Zn}_3\text{N}_2 + 3/2\text{H}_2$	12.55	-	-	-
Zn-R68	$2\text{ZnH} + \text{N}_2 = 2\text{ZnN} + \text{H}_2$	19.58	-	-	-
Zn-R69	$1/3\text{ZnH} + \text{N}_2 = 1/3\text{ZnN}_6 + 1/6\text{H}_2$	125.07	-	-	-
Zn-R70	$6\text{ZnH} + \text{N}_2 = 6\text{Zn} + 2\text{NH}_3$	-1.52	-	-	-
Zn-R71	$3\text{ZnH} + \text{N}_2 = \text{Zn}_3\text{N} + \text{NH}_3$	5.51	-	-	-
Zn-R72	$2\text{ZnH} + \text{N}_2 = 2/3\text{Zn}_3\text{N}_2 + 2/3\text{NH}_3$	12.55	-	-	-
Zn-R73	$3/2\text{ZnH} + \text{N}_2 = 3/2\text{ZnN} + 1/2\text{NH}_3$	19.58	-	-	-
Zn-R74	$6/19\text{ZnH} + \text{N}_2 = 6/19\text{ZnN}_6 + 2/19\text{NH}_3$	125.07	-	-	-
Zn-R75	$\text{ZnH}_6 + \text{N}_2 = \text{Zn}(\text{H}_2\text{N})_2 + \text{H}_2$	36.4	-	-	-
Zn-R76	$6\text{ZnH}_6 + \text{N}_2 = 2\text{Zn}_3\text{N} + 18\text{H}_2$	-1.93	-	-	-
Zn-R77	$3\text{ZnH}_6 + \text{N}_2 = \text{Zn}_3\text{N}_2 + 9\text{H}_2$	4.61	-	-	-
Zn-R78	$2\text{ZnH}_6 + \text{N}_2 = 2\text{ZnN} + 6\text{H}_2$	11.14	-	-	-
Zn-R79	$1/3\text{ZnH}_6 + \text{N}_2 = 1/3\text{ZnN}_6 + \text{H}_2$	109.19	-	-	-
Zn-R80	$\text{ZnH}_6 + \text{N}_2 = \text{Zn} + 2\text{NH}_3$	-8.47	-	-	-
Zn-R81	$6/5\text{ZnH}_6 + \text{N}_2 = 6/5\text{ZnH} + 2\text{NH}_3$	-7.06	-	-	-
Zn-R82	$3/4\text{ZnH}_6 + \text{N}_2 = 3/4\text{Zn}(\text{H}_2\text{N})_2 + 1/2\text{NH}_3$	36.4	-	-	-
Zn-R83	$6/7\text{ZnH}_6 + \text{N}_2 = 2/7\text{Zn}_3\text{N} + 12/7\text{NH}_3$	-1.93	-	-	-
Zn-R84	$3/4\text{ZnH}_6 + \text{N}_2 = 1/4\text{Zn}_3\text{N}_2 + 3/2\text{NH}_3$	4.61	-	-	-
Zn-R85	$2/3\text{ZnH}_6 + \text{N}_2 = 2/3\text{ZnN} + 4/3\text{NH}_3$	11.14	-	-	-
Zn-R86	$1/4\text{ZnH}_6 + \text{N}_2 = 1/4\text{ZnN}_6 + 1/2\text{NH}_3$	109.19	-	-	-

Zn-R87	$2/5\text{ZnN} + \text{N}_2 = 2/5\text{ZnN}_6$	88.22	-	-	-
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### 1.5 Nitridation and hydrogenation reactions for the ideal cycle II

Table S27: Nitridation reactions examined in the Ellingham diagram of Figure 2a.

ID	Reaction	dm_stoich [%]	h298 [kJ/mol]	T_eq [°C]	Type
Al-R20	$2\text{Al} + \text{N}_2 = 2\text{AlN}$	51.91	-635.97	-	exergonic
Ca-R125	$4\text{Ca} + \text{N}_2 = 2\text{Ca}_2\text{N}$	17.47	-519.68	-	exergonic
Co-R081	$6\text{Co} + \text{N}_2 = 2\text{Co}_3\text{N}$	7.92	16.74	-	endergonic
Cr-R066	$4\text{Cr} + \text{N}_2 = 2\text{Cr}_2\text{N}$	13.47	-251.04	-	exergonic
Cu-R48	$2/3\text{Cu} + \text{N}_2 = 2/3\text{Cu}_3\text{N}$	66.13	75.6	-	endergonic
Fe-R131	$6\text{Fe} + \text{N}_2 = 2\text{Fe}_3\text{N}$	8.36	-121.76	218.7	exergonic
Li-R102	$6\text{Li} + \text{N}_2 = 2\text{Li}_3\text{N}$	67.28	-329.11	-	exergonic
Mn-R52	$8\text{Mn} + \text{N}_2 = 2\text{Mn}_4\text{N}$	6.37	-257.33	-	exergonic
Mo-R058	$4\text{Mo} + \text{N}_2 = 2\text{Mo}_2\text{N}$	7.30	-163.18	686.8	exergonic
Ni-R104	$6\text{Ni} + \text{N}_2 = 2\text{Ni}_3\text{N}$	7.95	1.67	-	endergonic
Sr-R103	$4\text{Sr} + \text{N}_2 = 2\text{Sr}_2\text{N}$	7.99	-388.99	-	exergonic
W-R37	$4\text{W} + \text{N}_2 = 2\text{W}_2\text{N}$	3.81	-283.98	-	exergonic
Zn-R54	$3\text{Zn} + \text{N}_2 = \text{Zn}_3\text{N}_2$	14.28	-22.17	-	endergonic

Table S28: Hydrogenation reactions examined in the Ellingham diagram of Figure 2b.

ID	Reaction	dm_stoich [%]	h298 [kJ/mol]	T_eq [°C]	Type
Al-R15	$2/3\text{AlN} + \text{H}_2 = 2/3\text{Al} + 2/3\text{NH}_3$	-34.17	181.39	-	endergonic
Ca-R040	$2/3\text{Ca}_2\text{N} + \text{H}_2 = 4/3\text{Ca} + 2/3\text{NH}_3$	-14.88	142.63	-	endergonic
Co-R022	$2/3\text{Co}_3\text{N} + \text{H}_2 = 2\text{Co} + 2/3\text{NH}_3$	-7.34	-36.18	-	exergonic
Cr-R009	$2/3\text{Cr}_2\text{N} + \text{H}_2 = 4/3\text{Cr} + 2/3\text{NH}_3$	-11.87	53.08	-	endergonic
Cu-R21	$2/9\text{Cu}_3\text{N} + \text{H}_2 = 2/9\text{Cu} + 2/3\text{NH}_3$	-39.81	-55.8	-	exergonic
Fe-R054	$2/3\text{Fe}_3\text{N} + \text{H}_2 = 2\text{Fe} + 2/3\text{NH}_3$	-7.72	9.99	415.8	exergonic
Li-R033	$2/3\text{Li}_3\text{N} + \text{H}_2 = 2\text{Li} + 2/3\text{NH}_3$	-40.22	79.11	-	endergonic
Mn-R36	$2/3\text{Mn}_4\text{N} + \text{H}_2 = 8/3\text{Mn} + 2/3\text{NH}_3$	-5.99	55.18	-	endergonic
Mo-R016	$2/3\text{Mo}_2\text{N} + \text{H}_2 = 4/3\text{Mo} + 2/3\text{NH}_3$	-6.80	23.79	-	endergonic
Ni-R035	$2/3\text{Ni}_3\text{N} + \text{H}_2 = 2\text{Ni} + 2/3\text{NH}_3$	-7.37	-31.16	-	exergonic
Sr-R020	$2/3\text{Sr}_2\text{N} + \text{H}_2 = 4/3\text{Sr} + 2/3\text{NH}_3$	-7.40	99.07	-	endergonic
W-R01	$2/3\text{W}_2\text{N} + \text{H}_2 = 4/3\text{W} + 2/3\text{NH}_3$	-3.67	64.06	-	endergonic
Zn-R31	$1/3\text{Zn}_3\text{N}_2 + \text{H}_2 = \text{Zn} + 2/3\text{NH}_3$	-12.50	-23.21	-	exergonic

### 1.6 Ellingham diagrams

Ellingham diagrams of all identified reactions (see Section 1.4 Reactions): standard Gibbs free energy change per mol of  $\text{N}_2$  (nitridation) and per mole of  $\text{H}_2$  (hydrogenation) as a function of temperature. Dashed lines indicate species from the MP database with an  $E_{hull}$  greater than 0, i.e. potentially unstable at standard conditions.

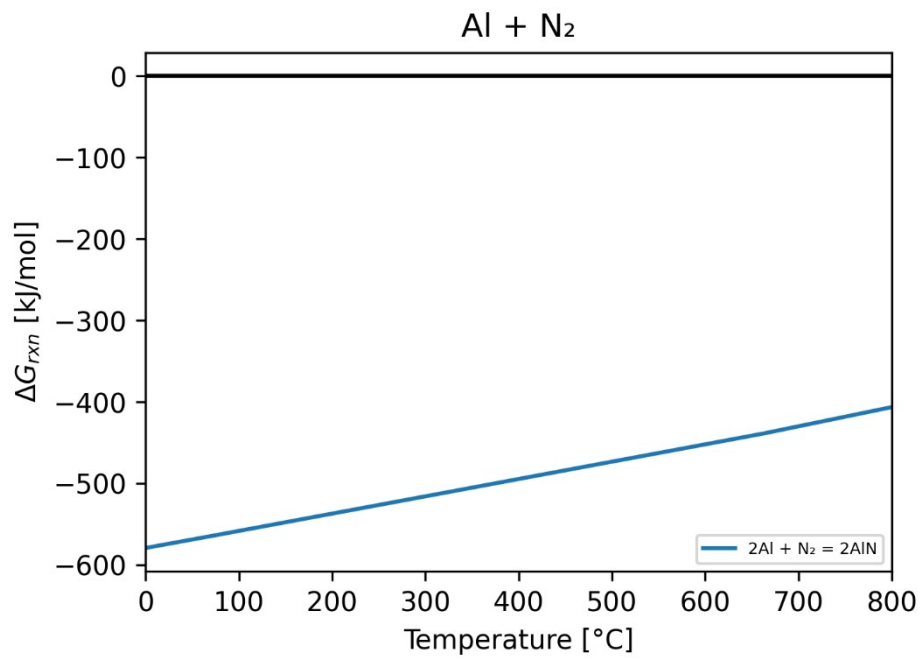


Figure S2: Ellingham diagram of the Al nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

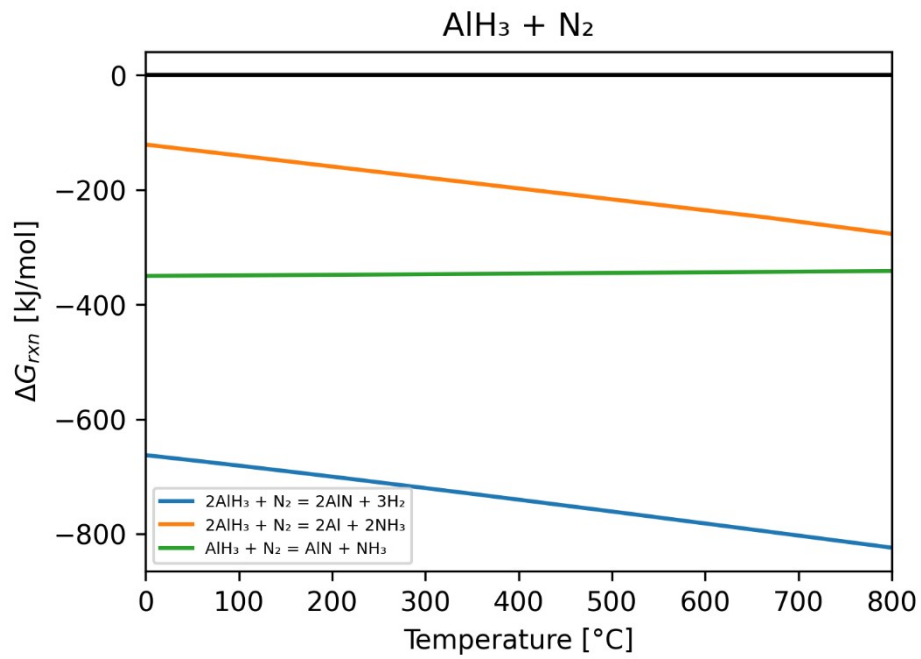


Figure S3: Ellingham diagram of the AlH<sub>3</sub> nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.



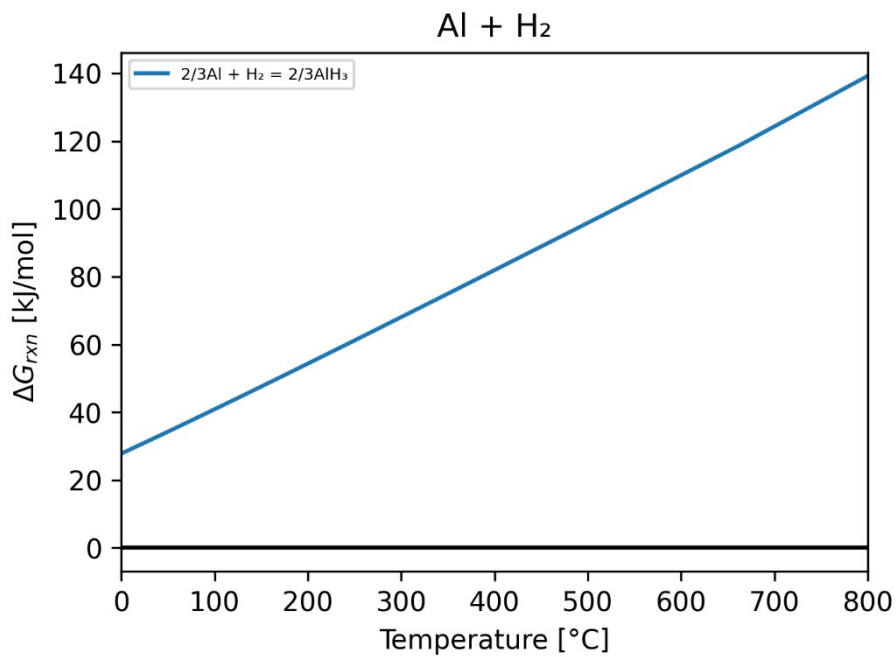


Figure S4: Ellingham diagram of the Al hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

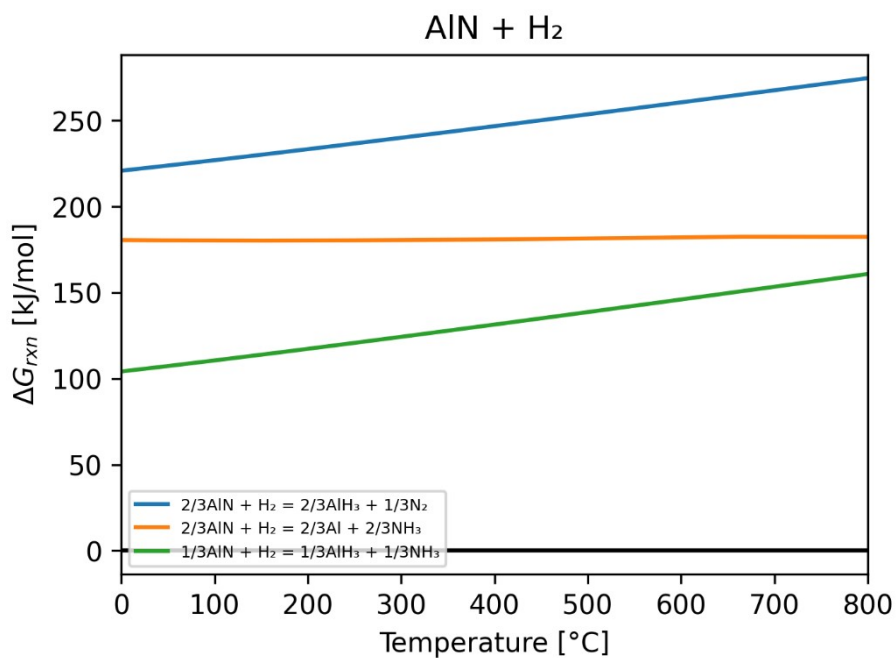


Figure S5: Ellingham diagram of the AlN hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

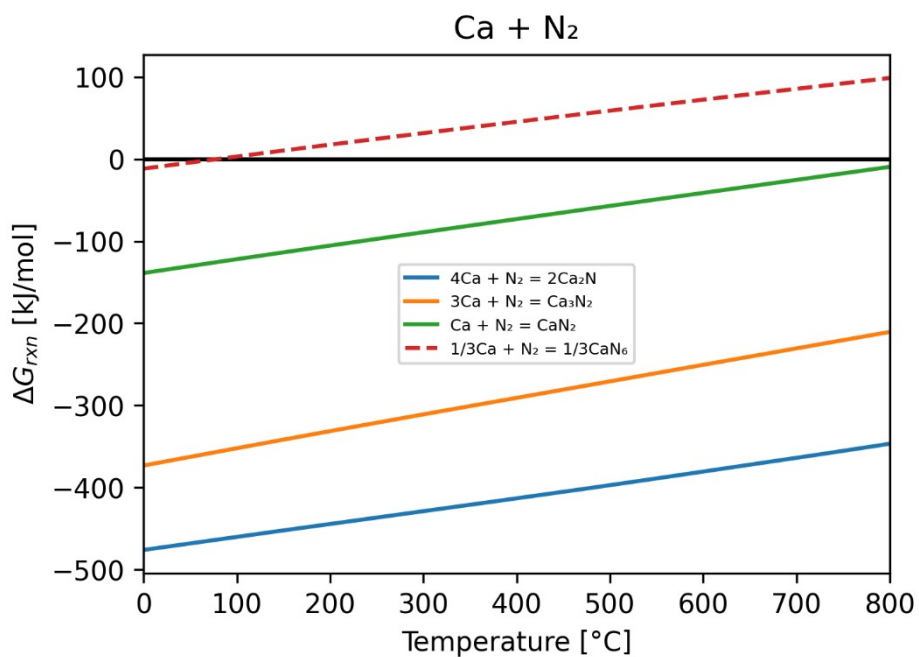


Figure S6: Ellingham diagram of the Ca nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

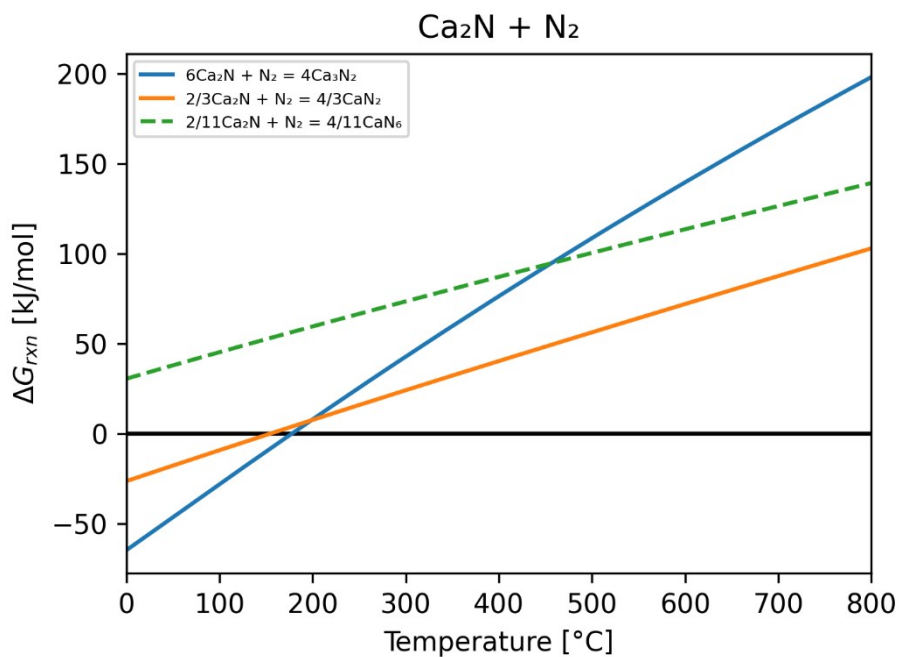


Figure S7: Ellingham diagram of the Ca<sub>2</sub>N nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.



Figure S8: Ellingham diagram of the  $\text{Ca}_2\text{N}$  nitridation step: standard Gibbs free energy change per mol  $\text{N}_2$  as a function of temperature.

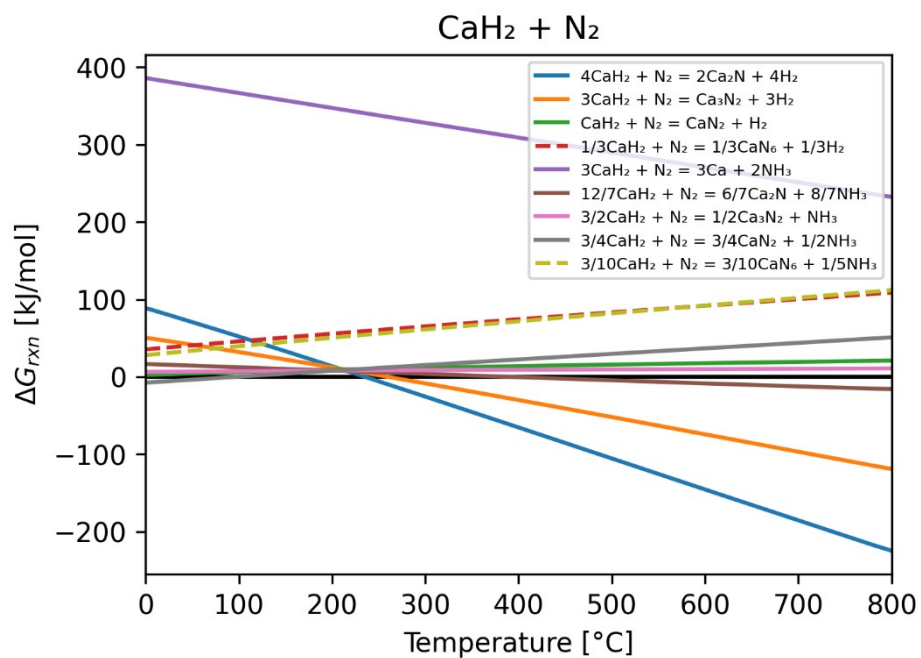


Figure S9: Ellingham diagram of the  $\text{CaH}_2$  nitridation step: standard Gibbs free energy change per mol  $\text{N}_2$  as a function of temperature.

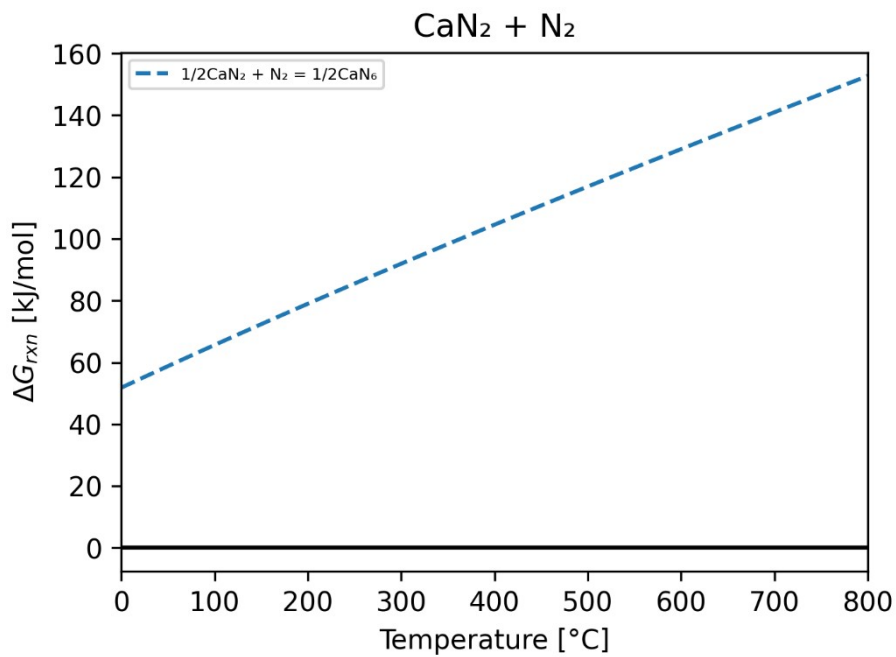


Figure S10: Ellingham diagram of the CaN<sub>2</sub> nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

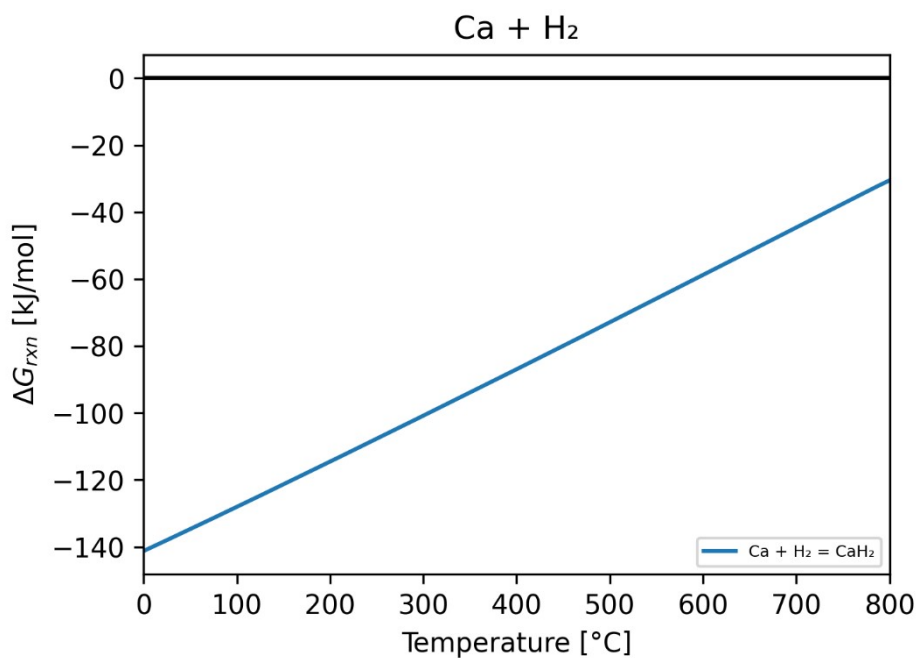


Figure S11: Ellingham diagram of the Ca hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

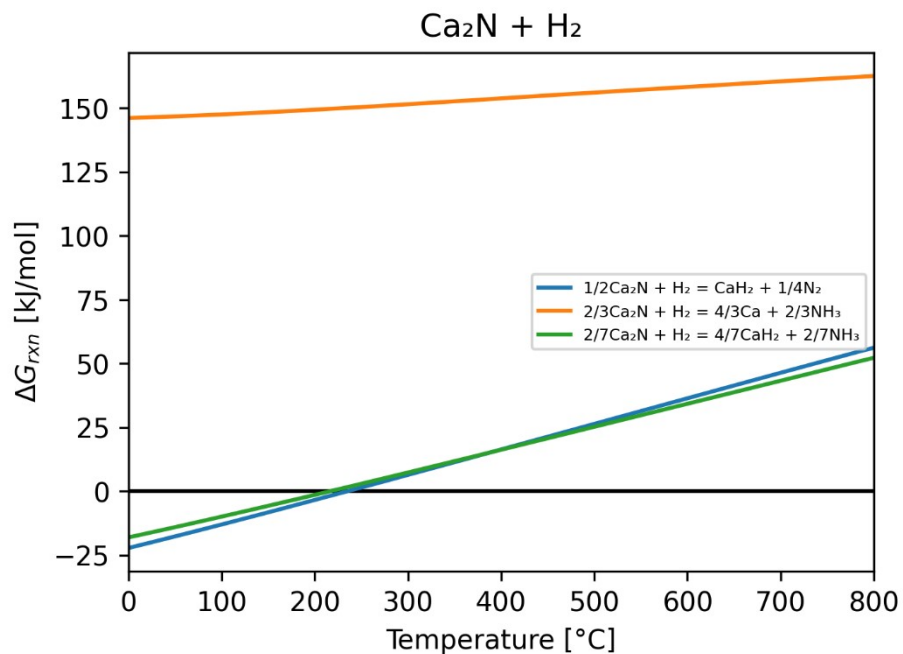


Figure S12: Ellingham diagram of the Ca<sub>2</sub>N hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

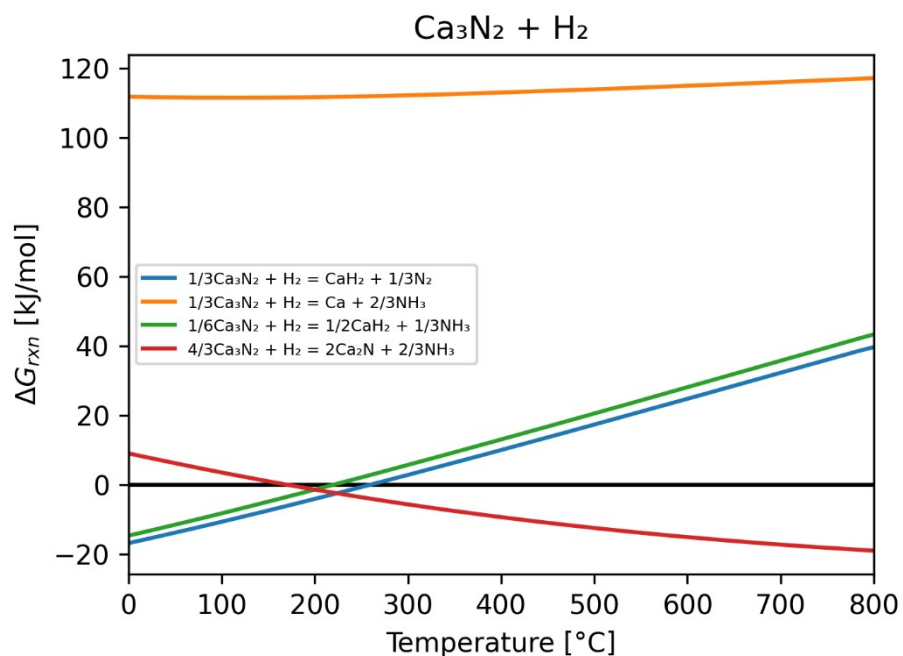


Figure S13: Ellingham diagram of the Ca<sub>3</sub>N<sub>2</sub> hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

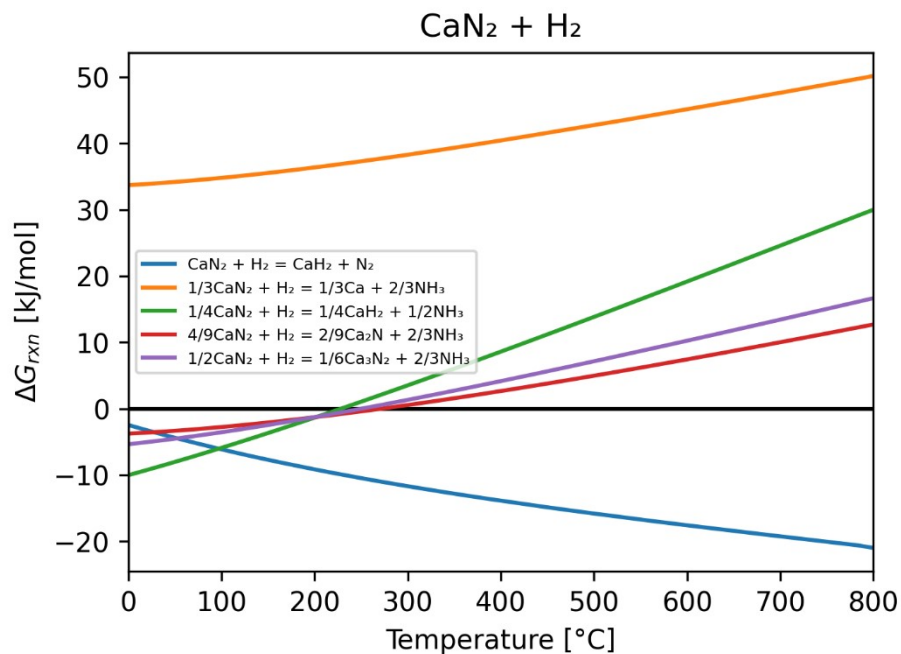


Figure S14: Ellingham diagram of the CaN<sub>2</sub> hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

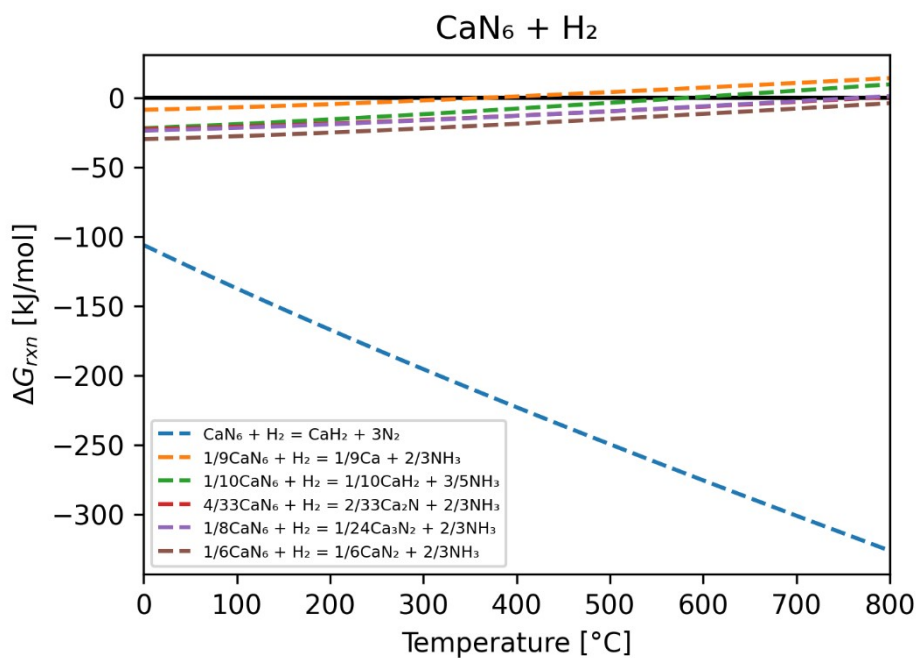


Figure S15: Ellingham diagram of the CaN<sub>6</sub> hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

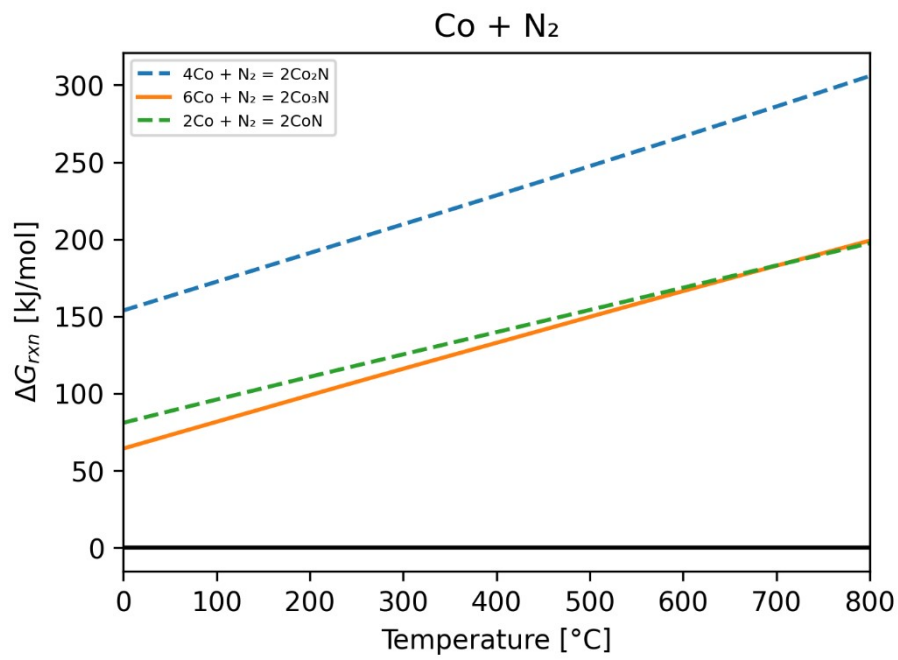


Figure S16: Ellingham diagram of the Co nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

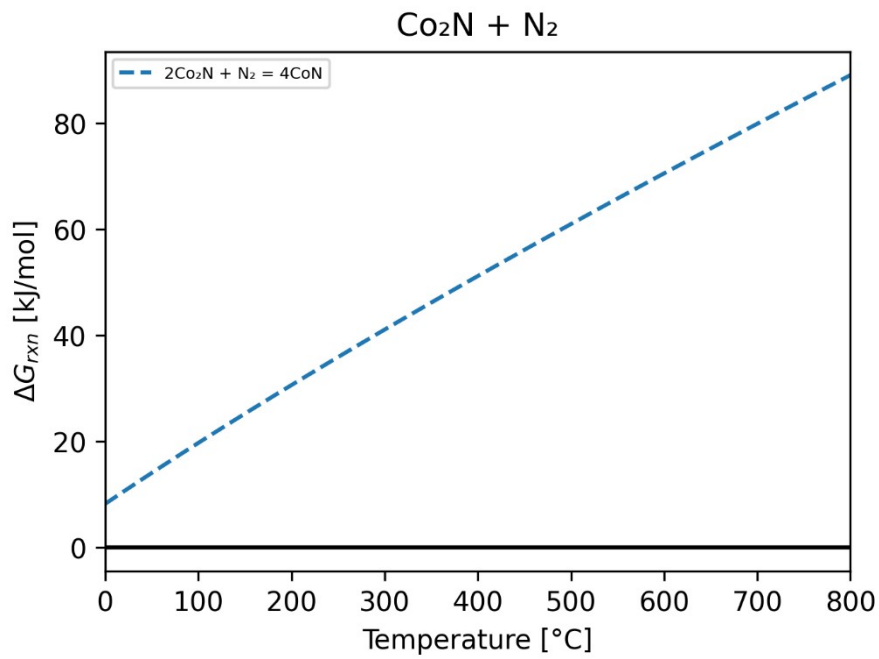


Figure S17: Ellingham diagram of the Co<sub>2</sub>N nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

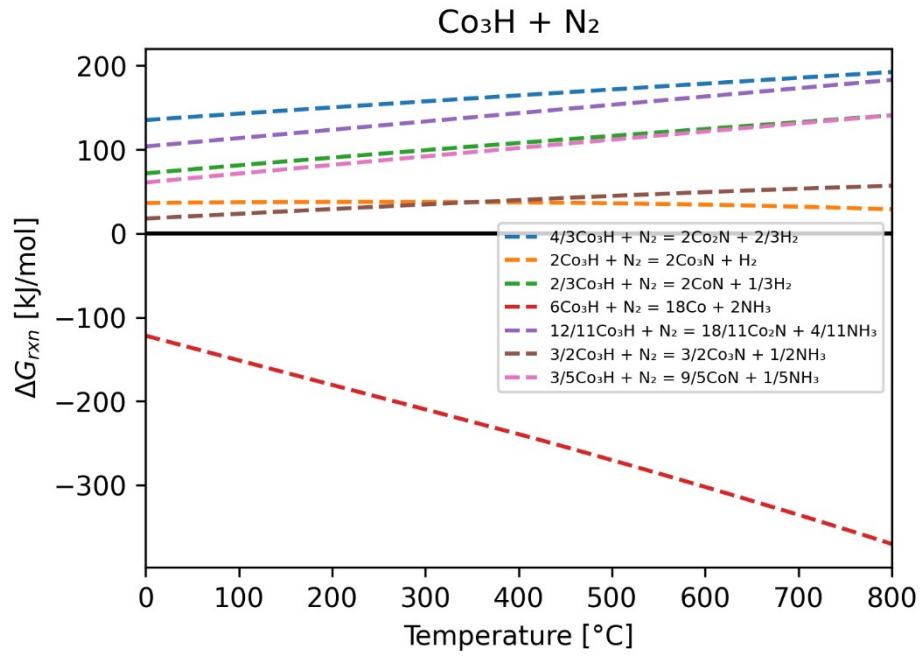


Figure S18: Ellingham diagram of the Co<sub>3</sub>H nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

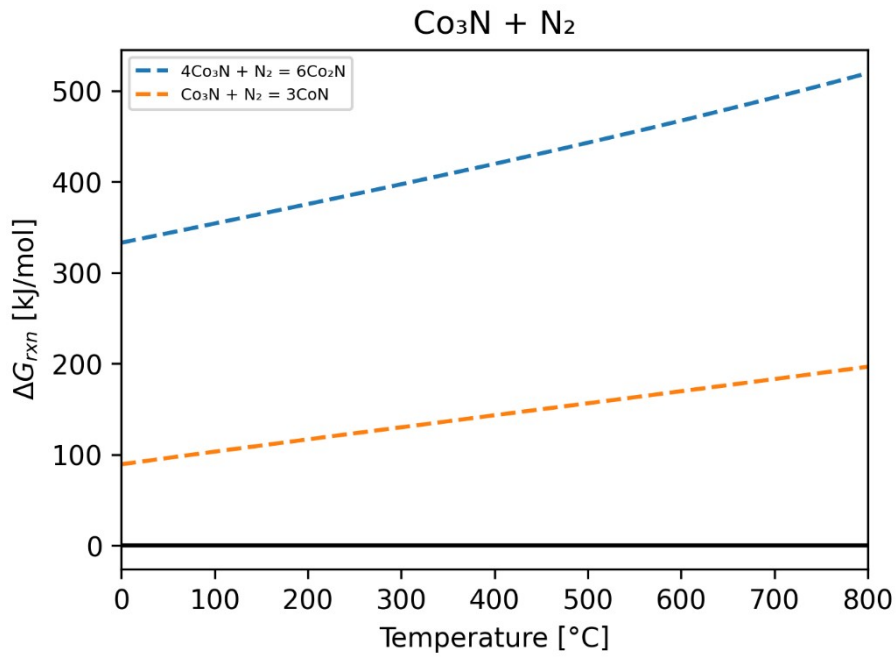


Figure S19: Ellingham diagram of the Co<sub>3</sub>N nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.



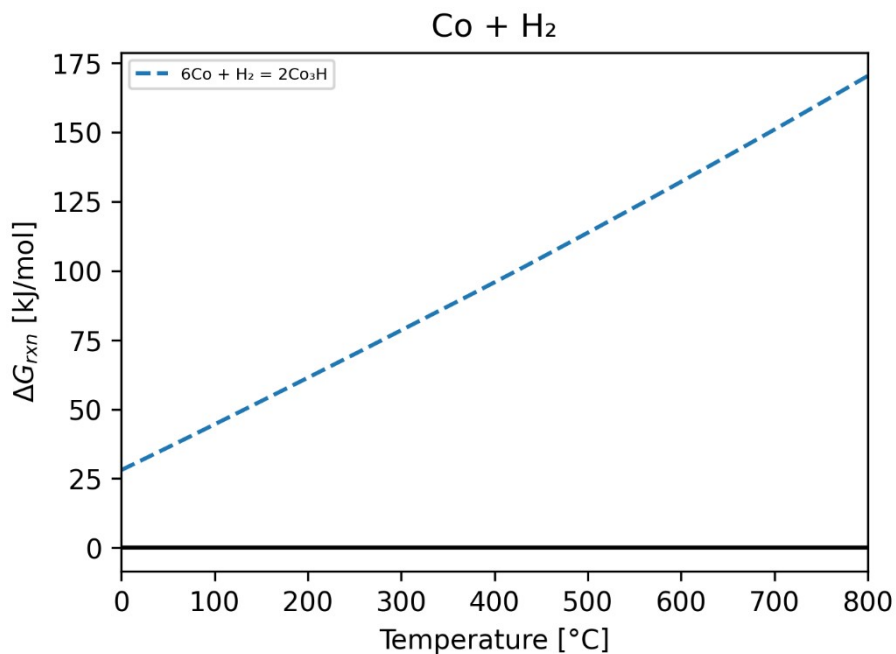


Figure S20: Ellingham diagram of the Co hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

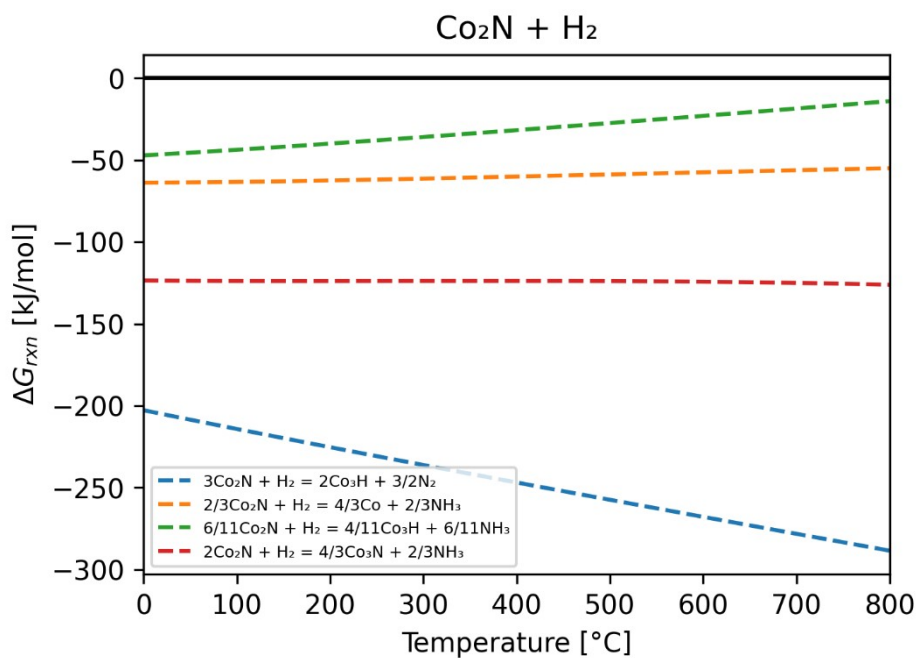


Figure S21: Ellingham diagram of the CO<sub>2</sub>N hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

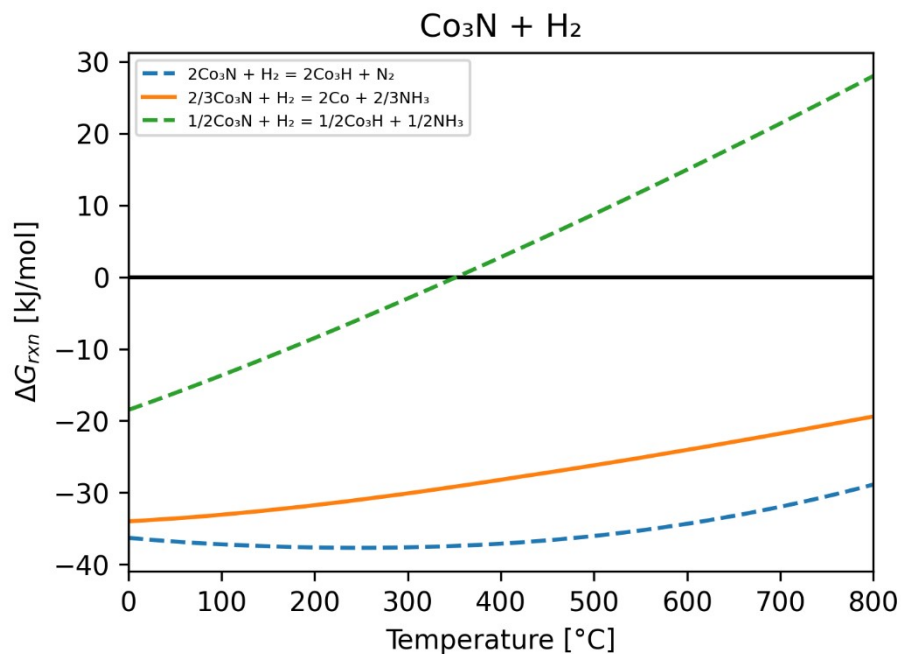


Figure S22: Ellingham diagram of the Co<sub>3</sub>N hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

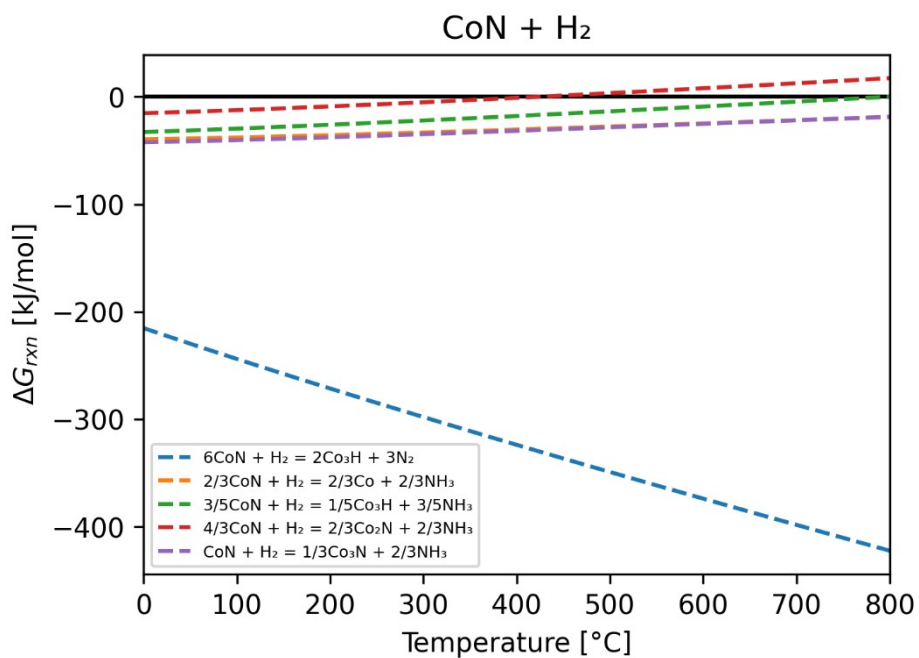


Figure S23: Ellingham diagram of the CoN hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

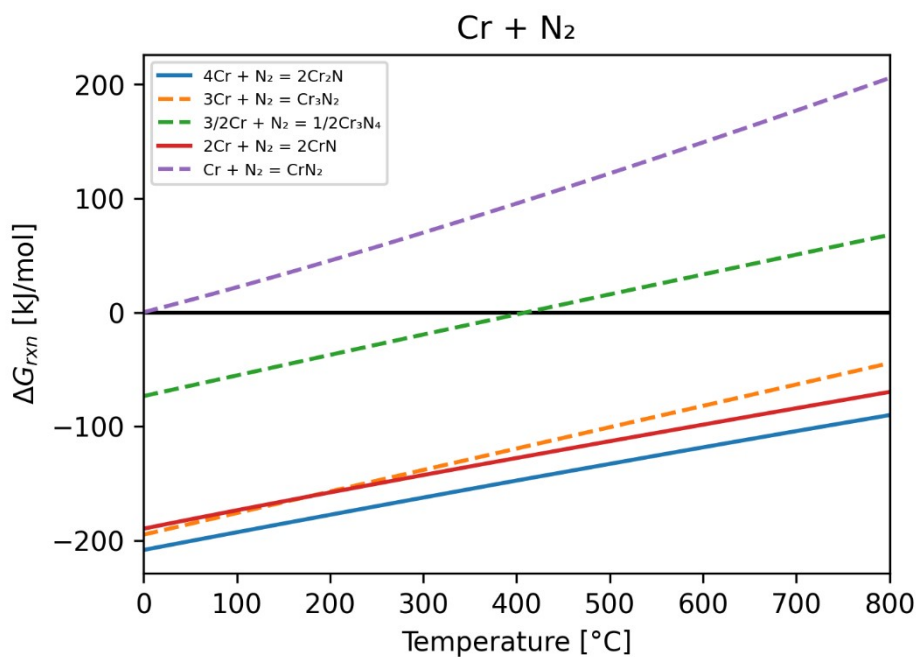


Figure S24: Ellingham diagram of the Cr nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

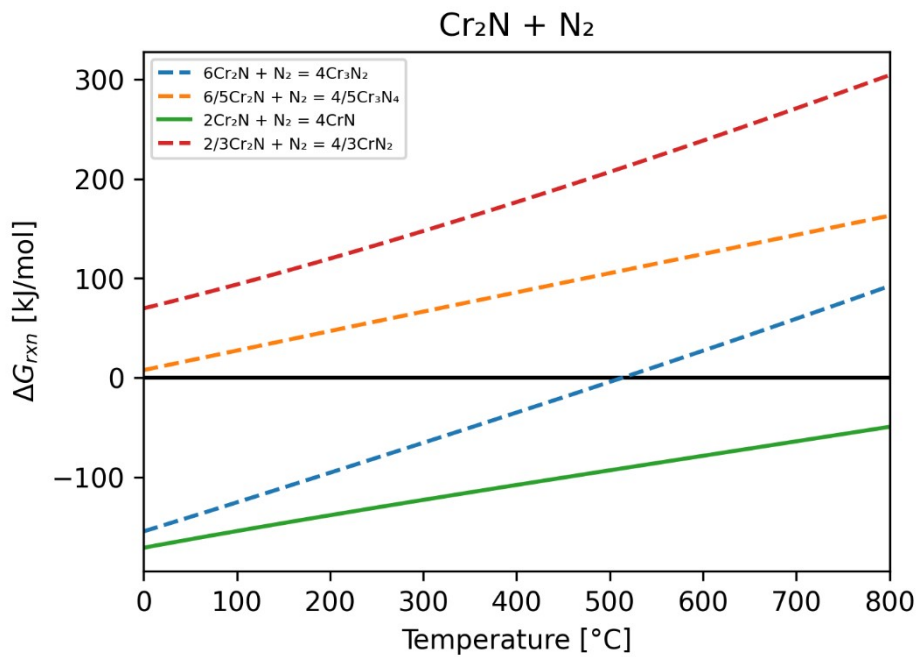


Figure S25: Ellingham diagram of the Cr<sub>2</sub>N nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

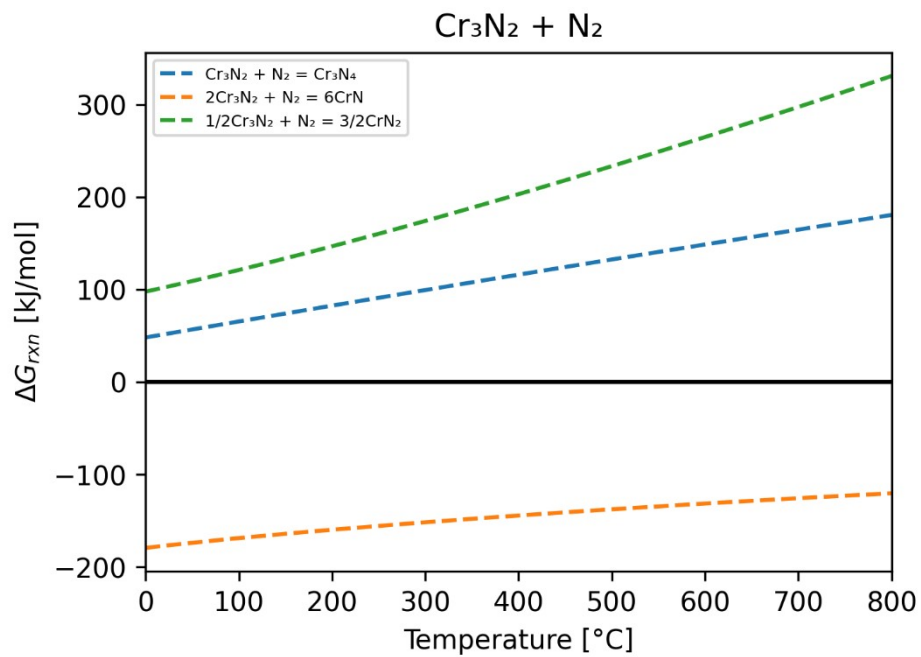


Figure S26: Ellingham diagram of the  $\text{Cr}_3\text{N}_2$  nitridation step: standard Gibbs free energy change per mol  $\text{N}_2$  as a function of temperature.

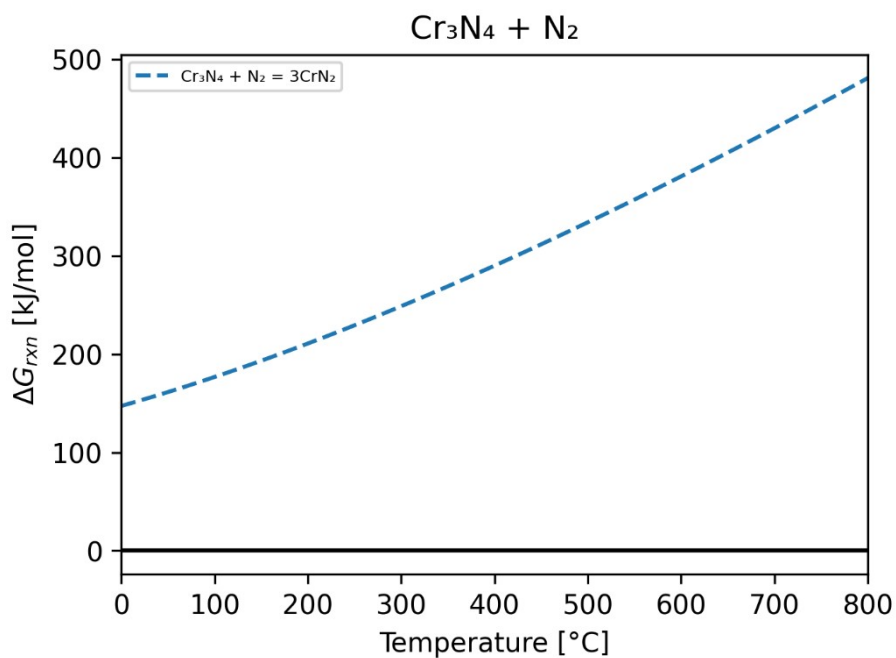


Figure S27: Ellingham diagram of the  $\text{Cr}_3\text{N}_4$  nitridation step: standard Gibbs free energy change per mol  $\text{N}_2$  as a function of temperature.

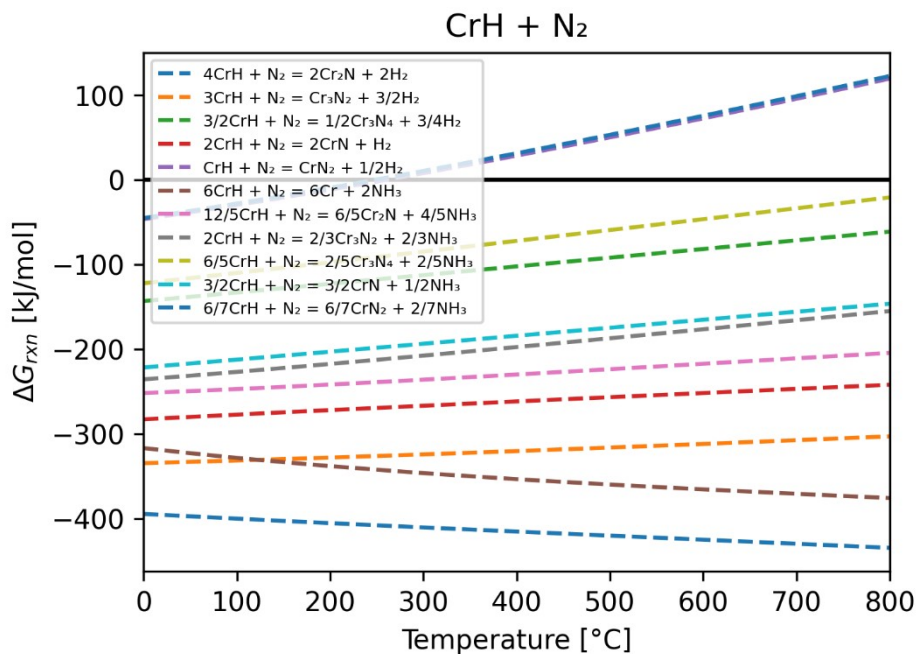


Figure S28: Ellingham diagram of the CrH nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

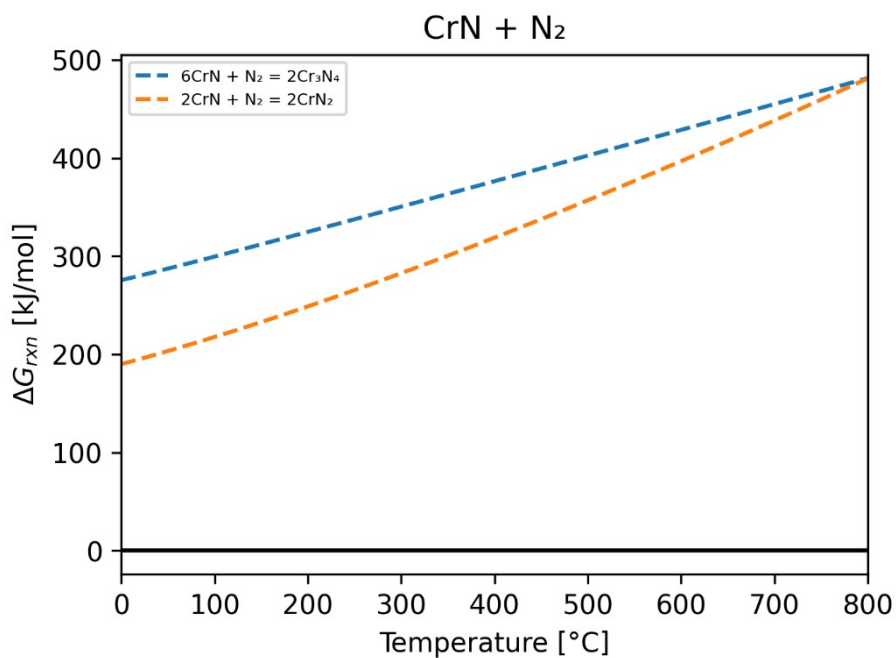


Figure S29: Ellingham diagram of the CrN nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

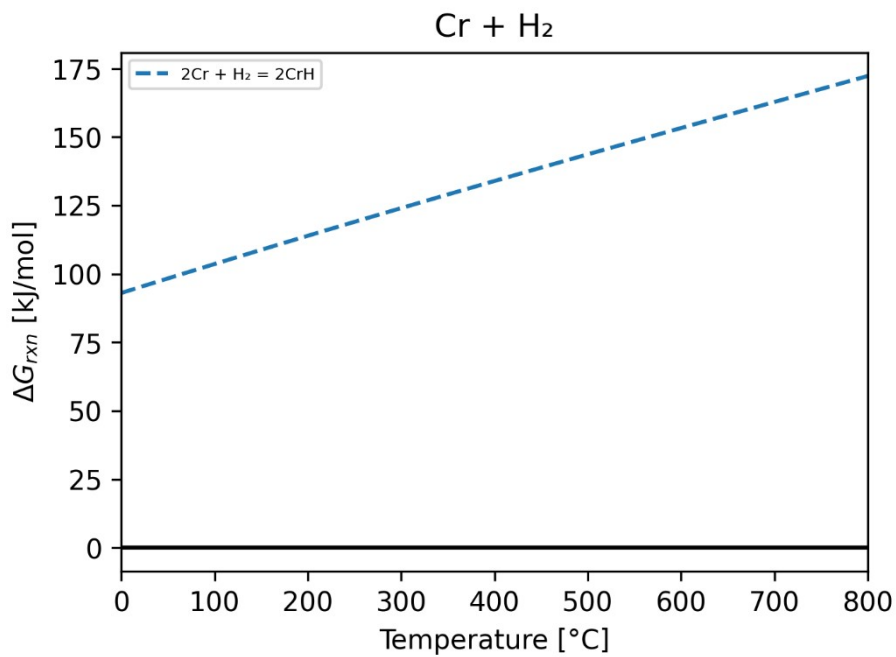


Figure S30: Ellingham diagram of the Cr hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

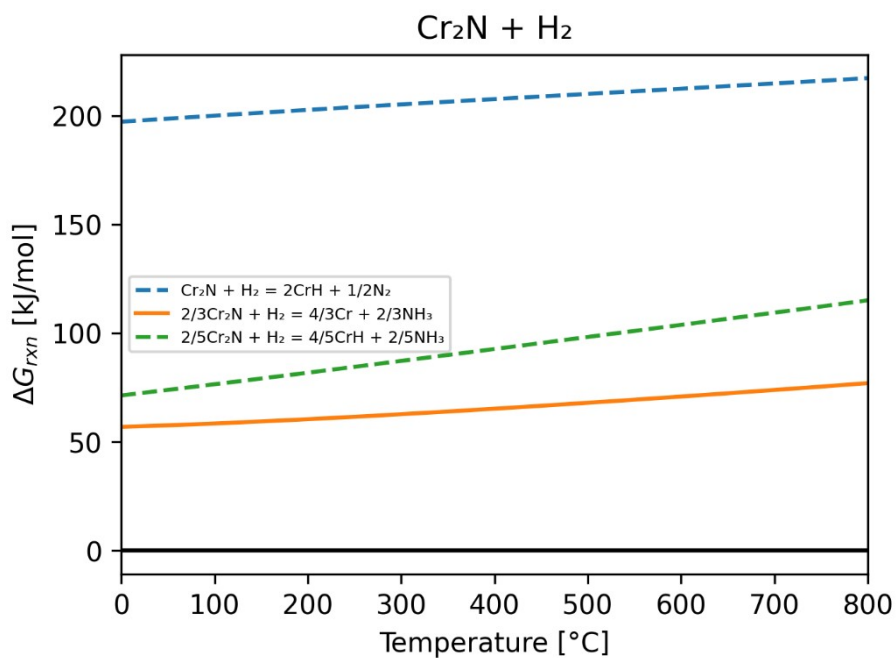


Figure S31: Ellingham diagram of the Cr<sub>2</sub>N hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

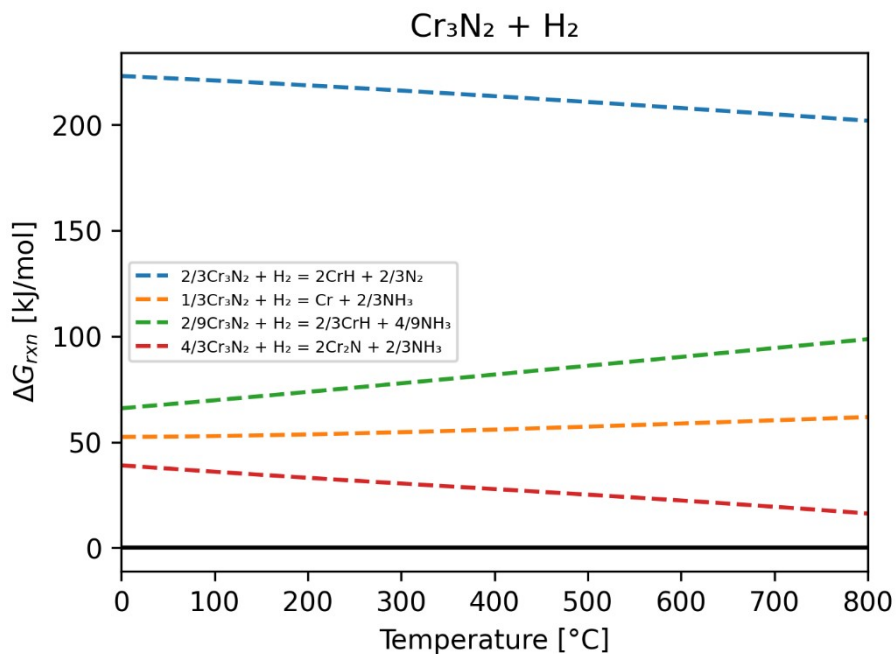


Figure S32: Ellingham diagram of the  $\text{Cr}_3\text{N}_2$  hydrogenation step: standard Gibbs free energy change per mol  $\text{H}_2$  as a function of temperature.

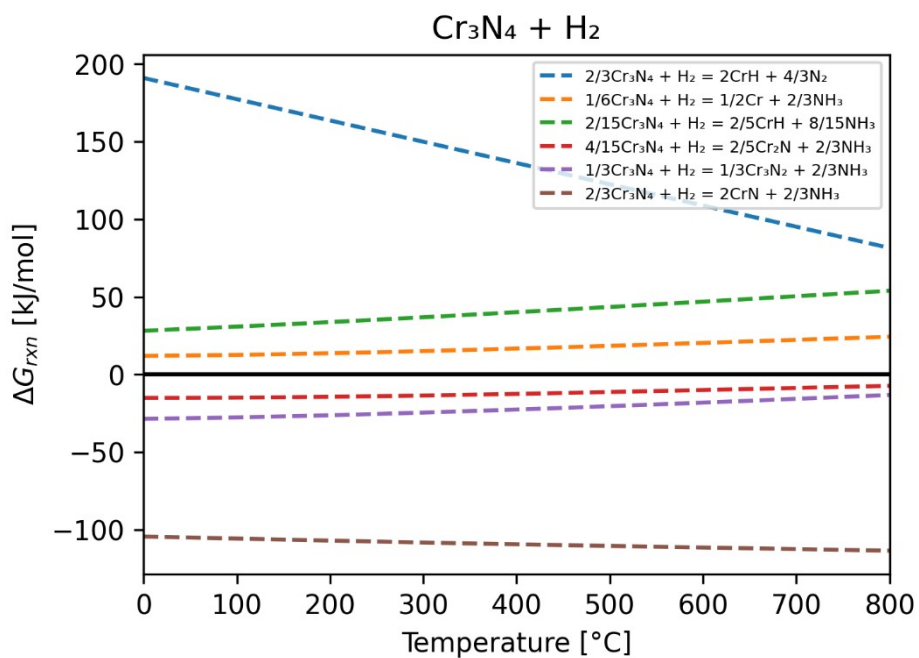


Figure S33: Ellingham diagram of the  $\text{Cr}_3\text{N}_4$  hydrogenation step: standard Gibbs free energy change per mol  $\text{H}_2$  as a function of temperature.

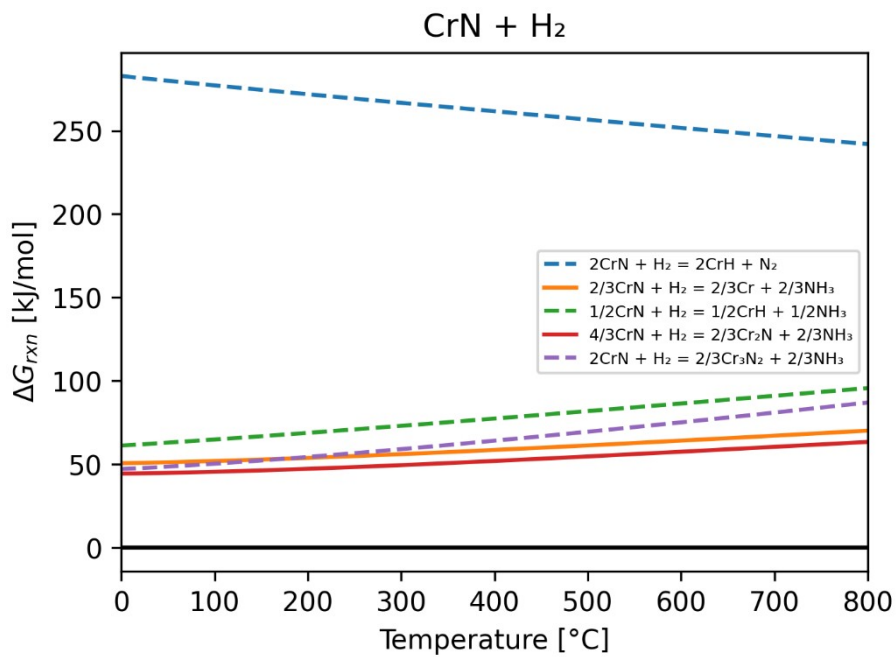


Figure S34: Ellingham diagram of the CrN hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

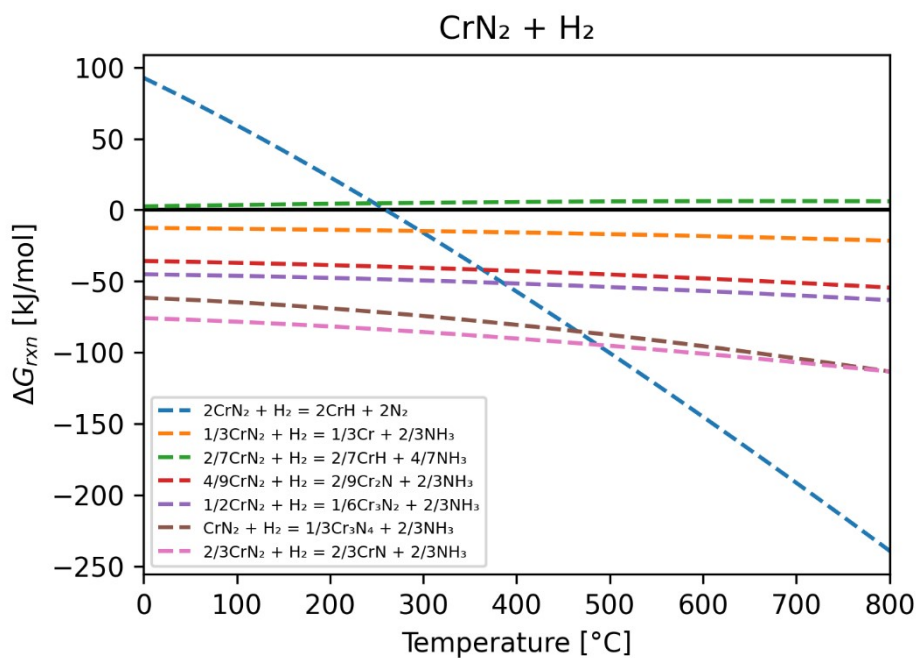


Figure S35: Ellingham diagram of the CrN<sub>2</sub> hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.



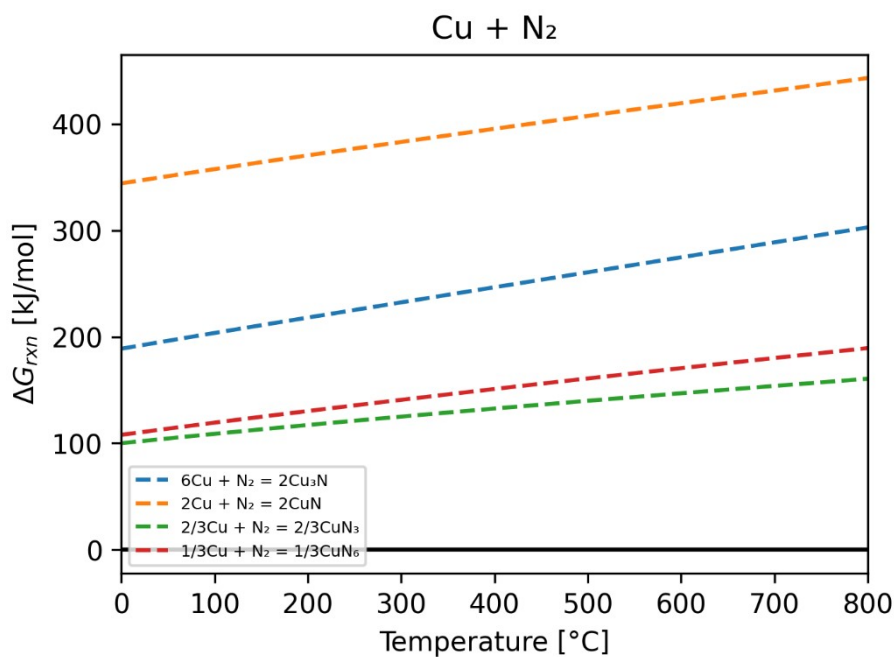


Figure S36: Ellingham diagram of the Cu nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

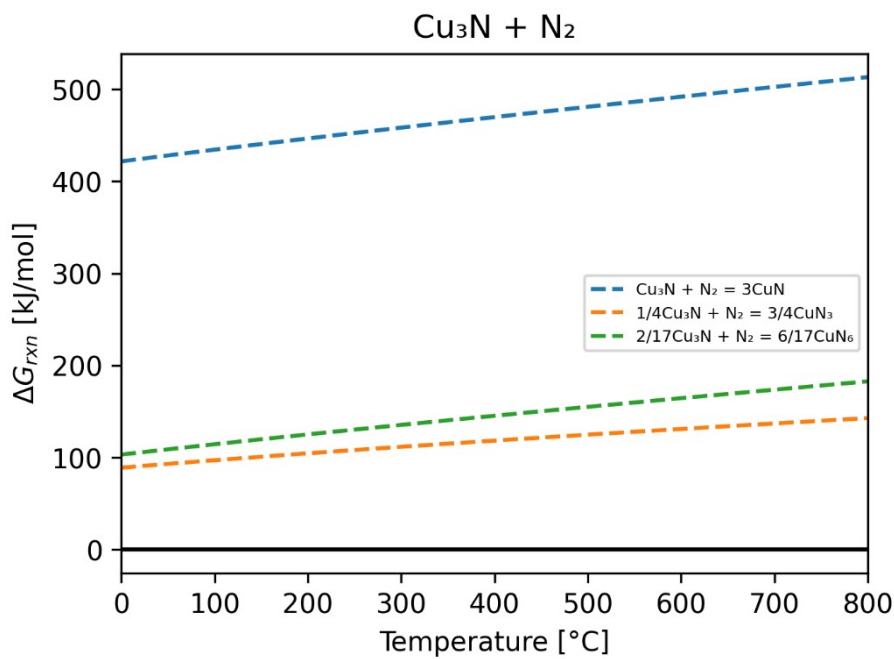


Figure S37: Ellingham diagram of the Cu<sub>3</sub>N nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

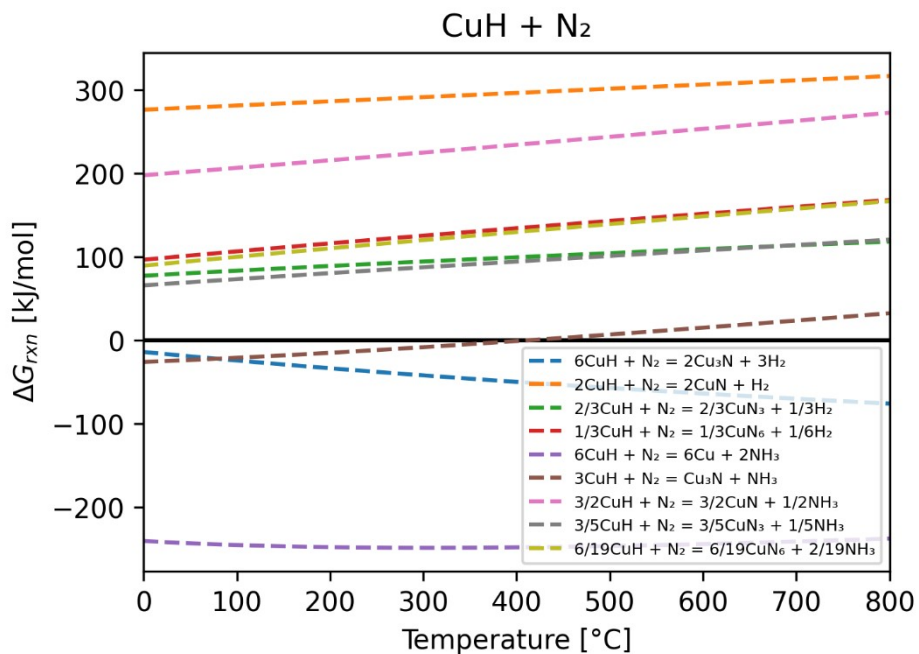


Figure S38: Ellingham diagram of the CuH nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

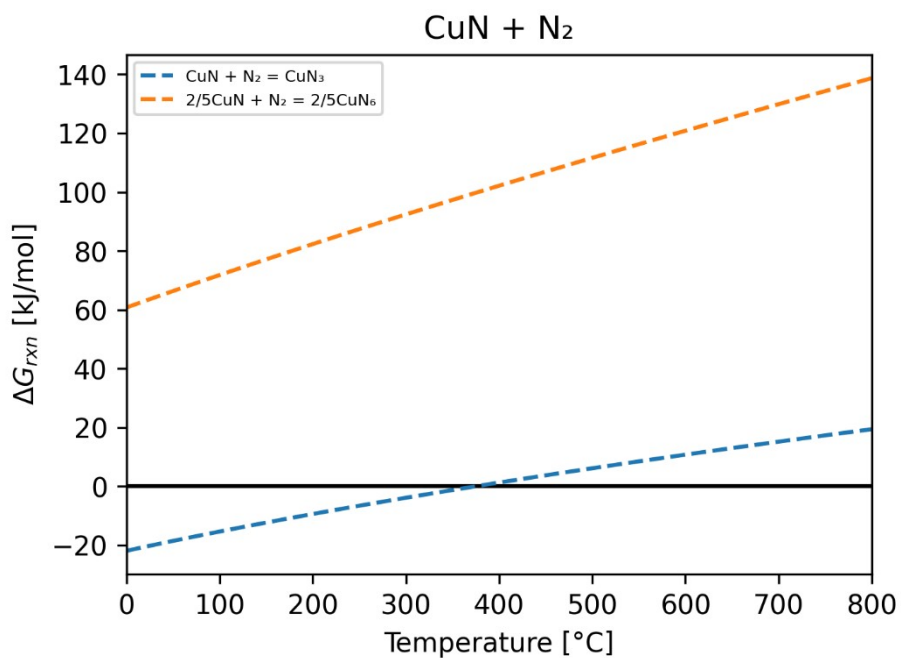


Figure S39: Ellingham diagram of the CuN nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

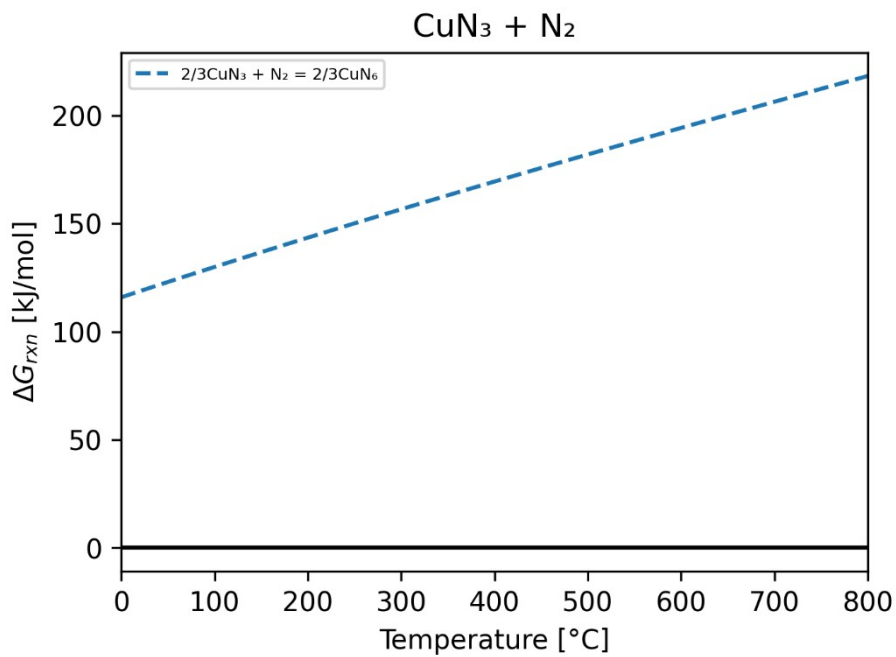


Figure S40: Ellingham diagram of the CuN<sub>3</sub> nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

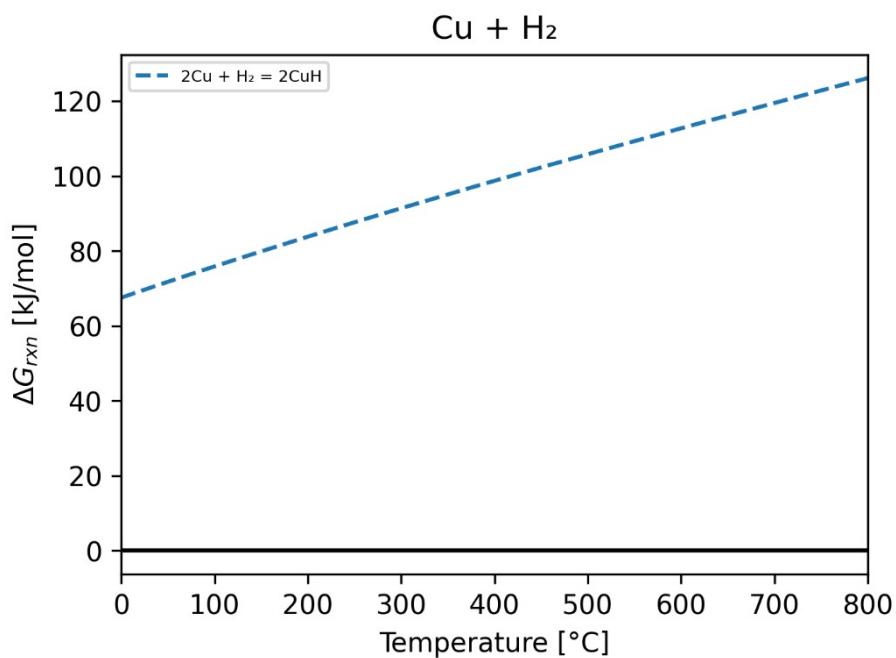


Figure S41: Ellingham diagram of the Cu hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

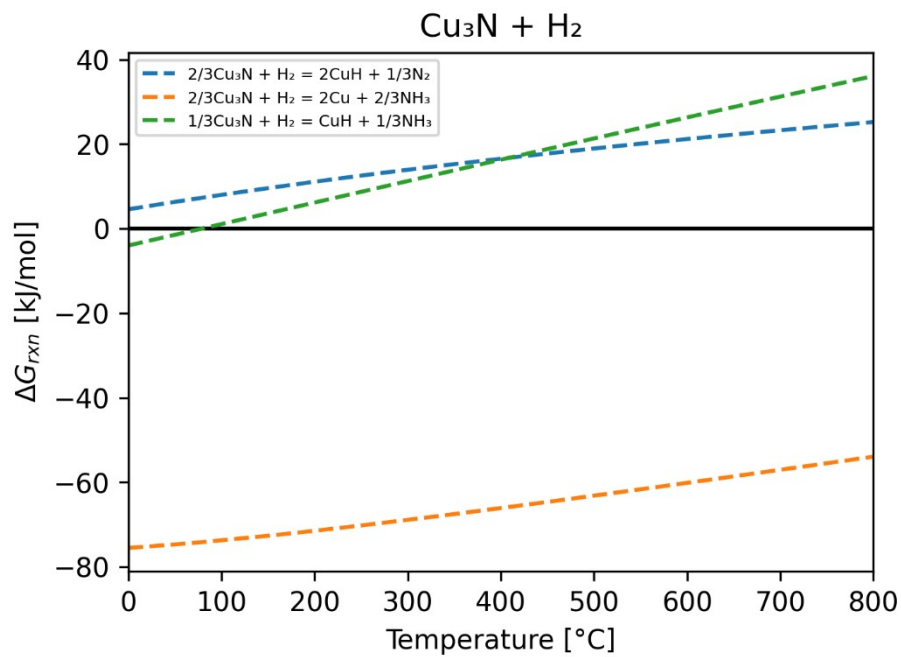


Figure S42: Ellingham diagram of the Cu<sub>3</sub>N hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

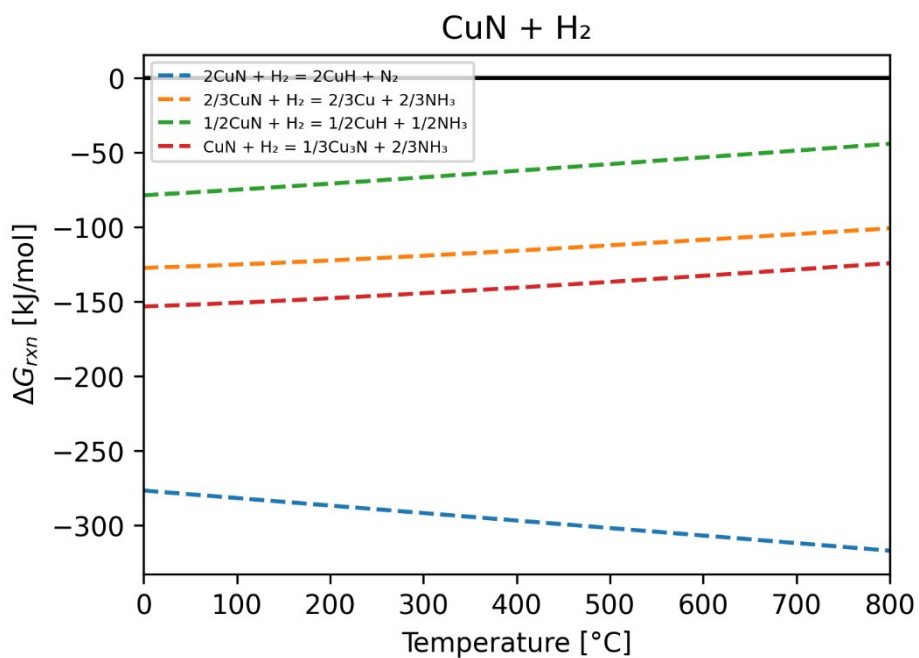


Figure S43: Ellingham diagram of the CuN hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

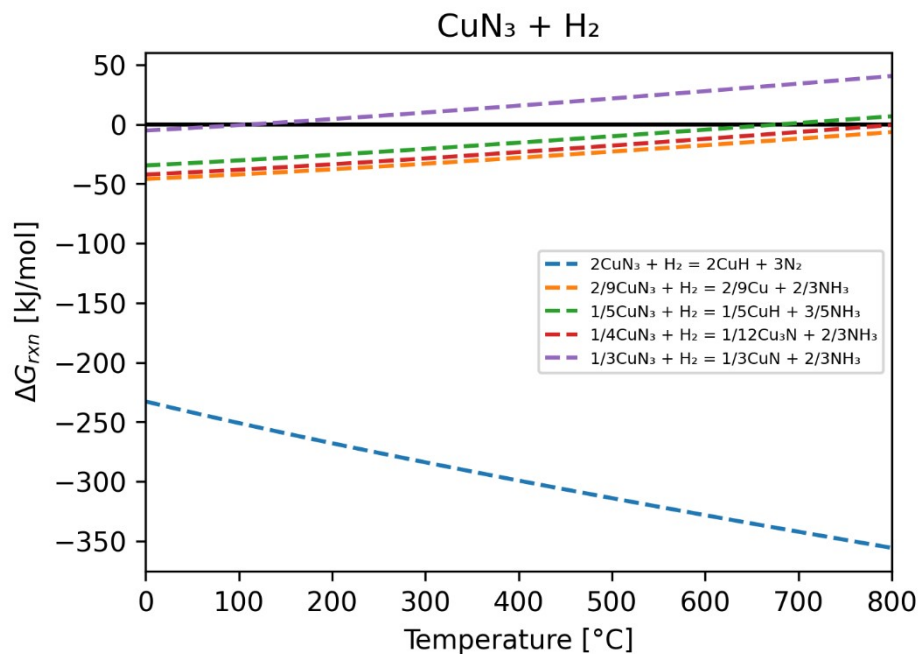


Figure S44: Ellingham diagram of the CuN<sub>3</sub> hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

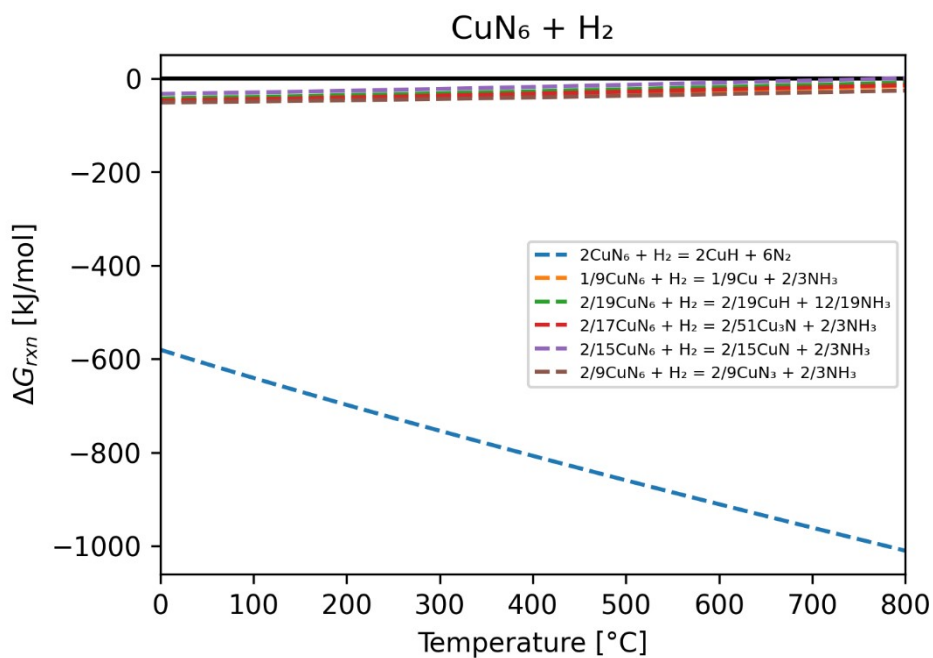


Figure S45: Ellingham diagram of the CuN<sub>6</sub> hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

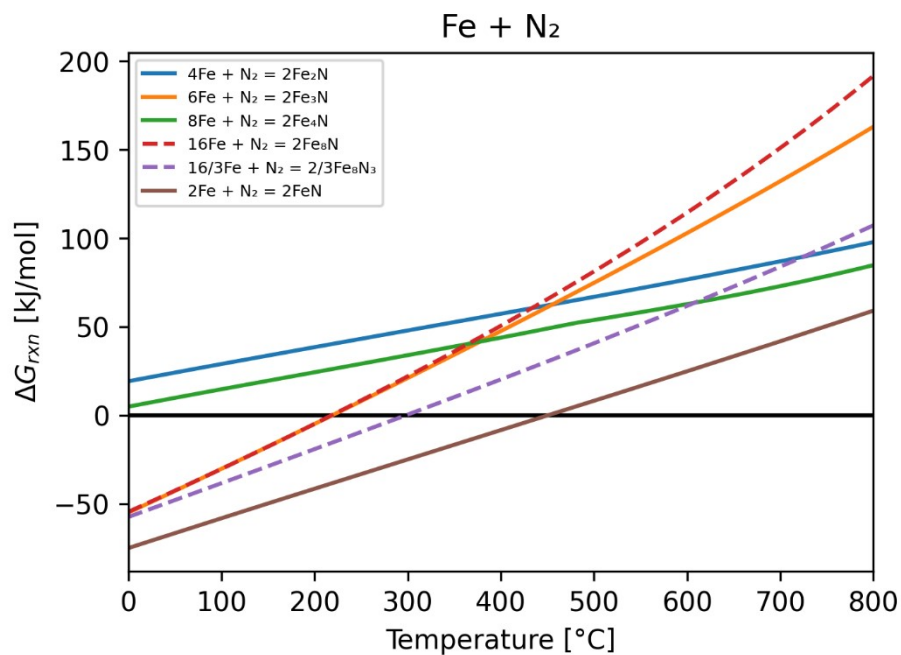


Figure S46: Ellingham diagram of the Fe nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

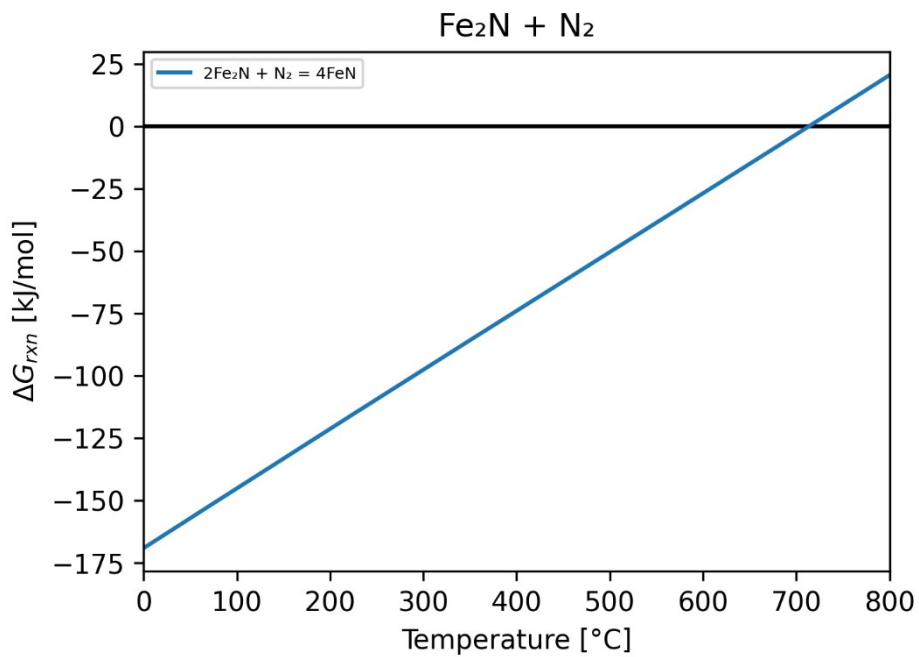


Figure S47: Ellingham diagram of the Fe<sub>2</sub>N nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

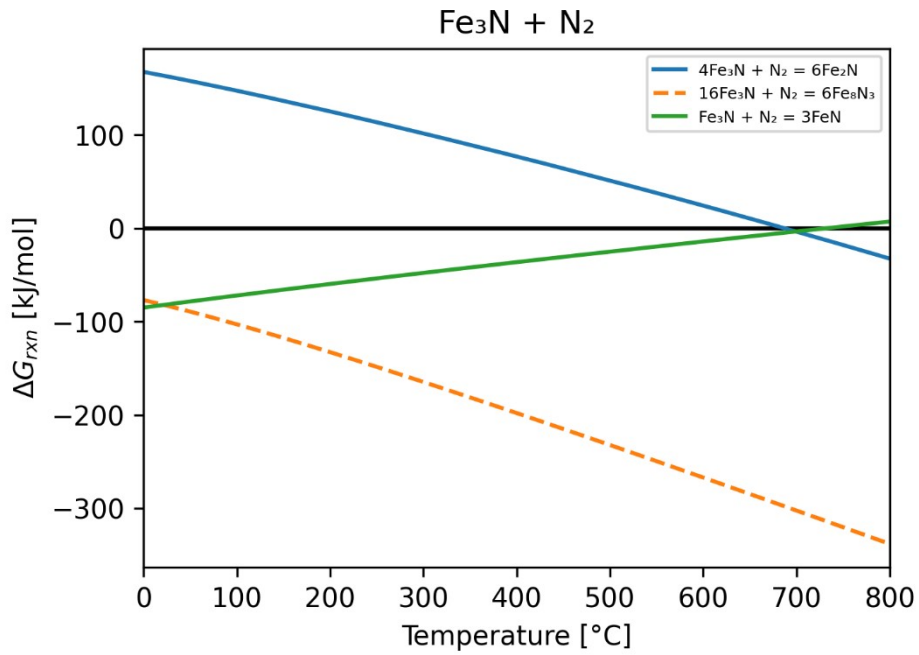


Figure S48: Ellingham diagram of the Fe<sub>3</sub>N nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

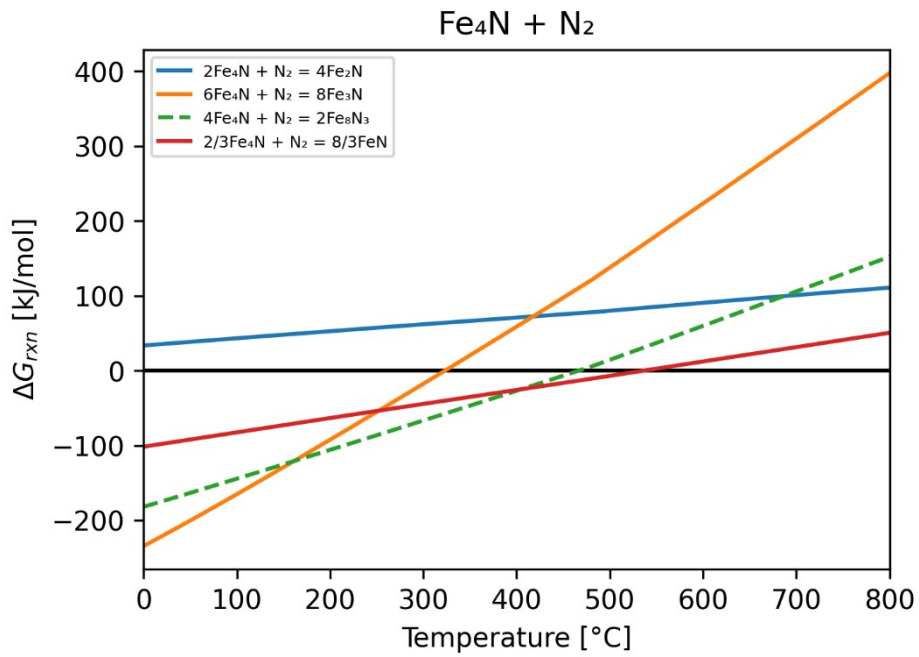


Figure S49: Ellingham diagram of the Fe<sub>4</sub>N nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

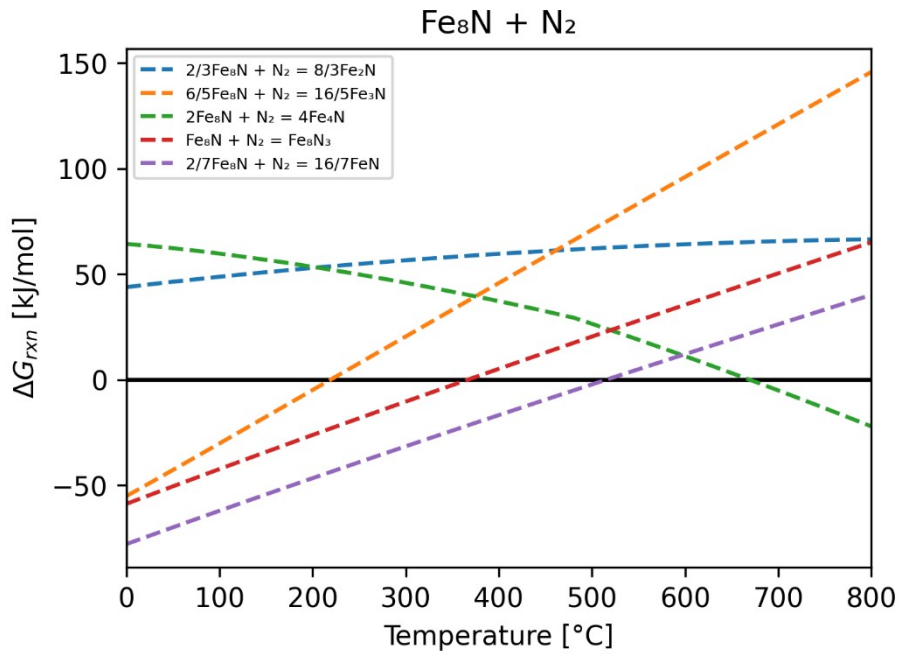


Figure S50: Ellingham diagram of the Fe<sub>8</sub>N nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

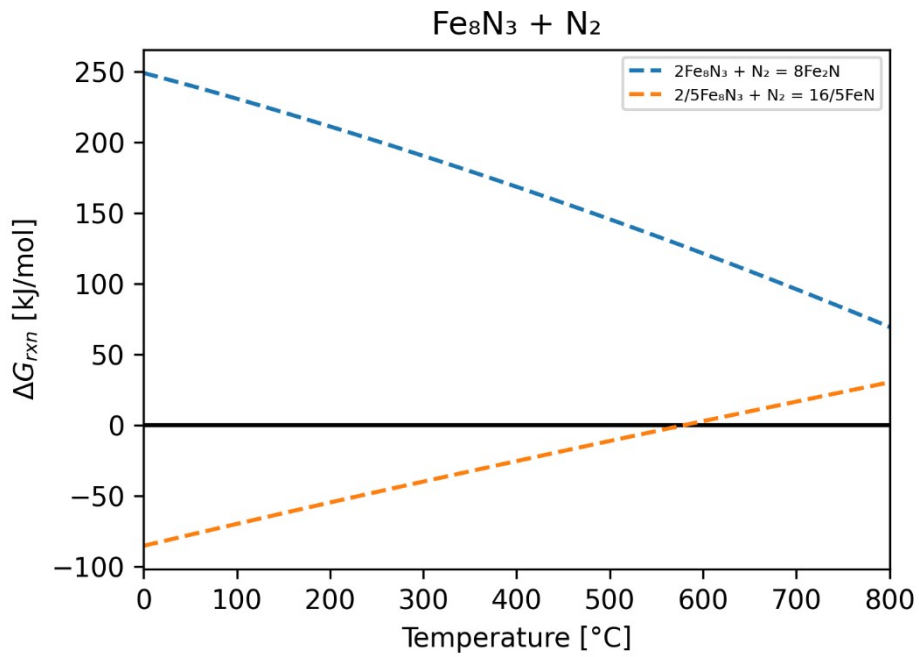


Figure S51: Ellingham diagram of the Fe<sub>8</sub>N<sub>3</sub> nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.



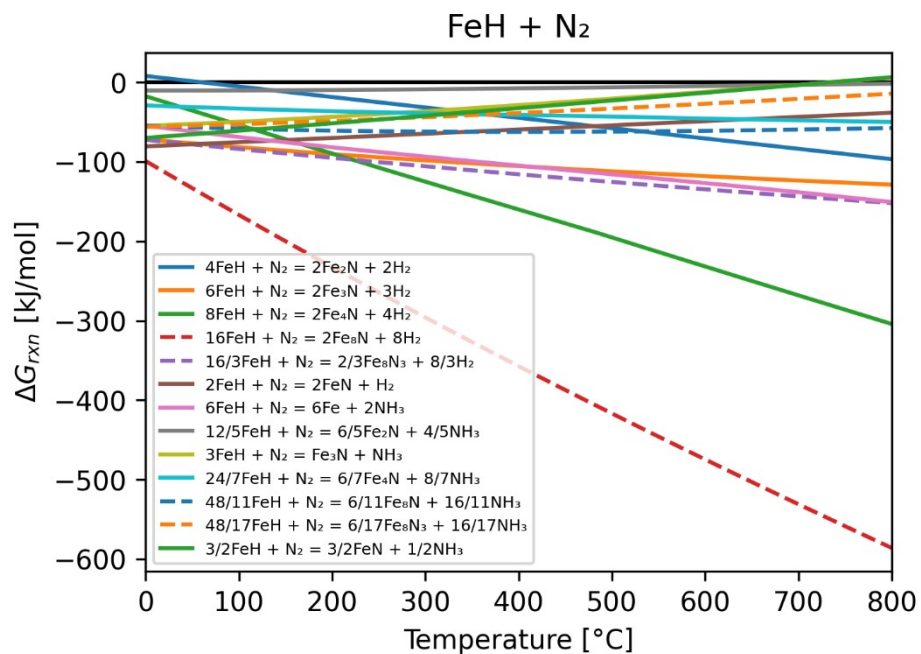


Figure S52: Ellingham diagram of the FeH nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

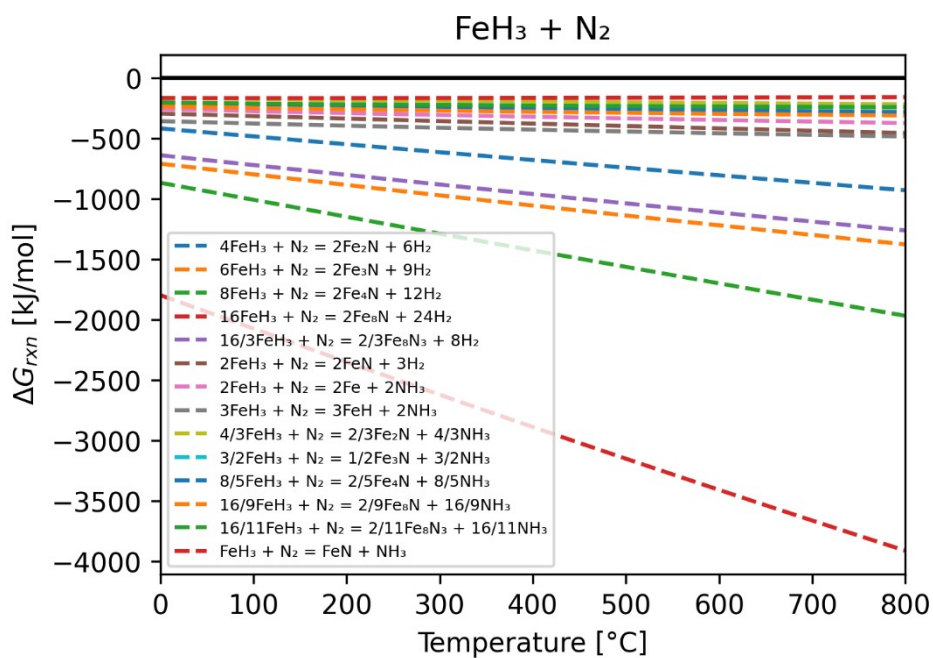


Figure S53: Ellingham diagram of the FeH<sub>3</sub> nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

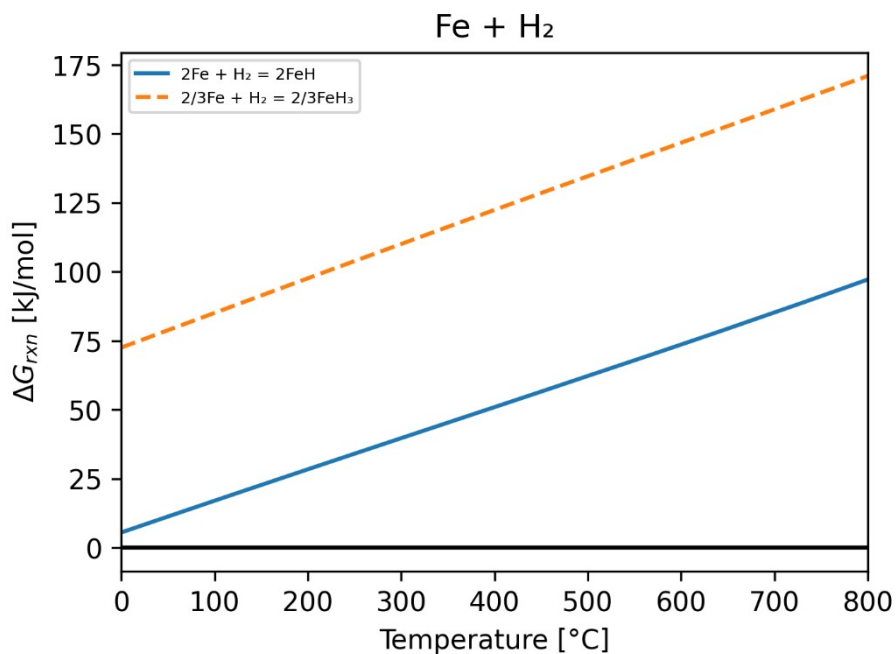


Figure S54: Ellingham diagram of the Fe hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

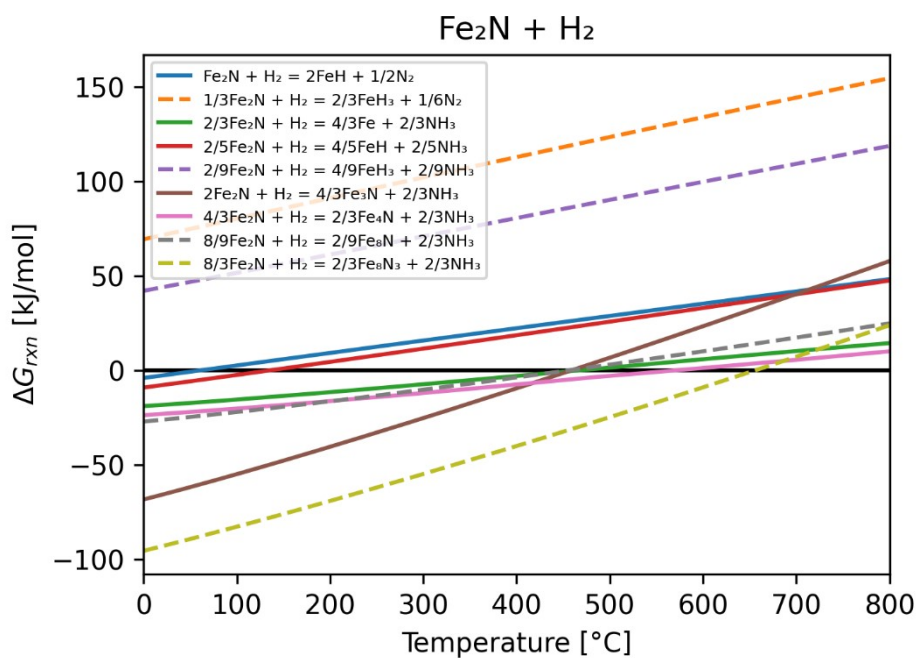


Figure S55: Ellingham diagram of the Fe<sub>2</sub>N hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

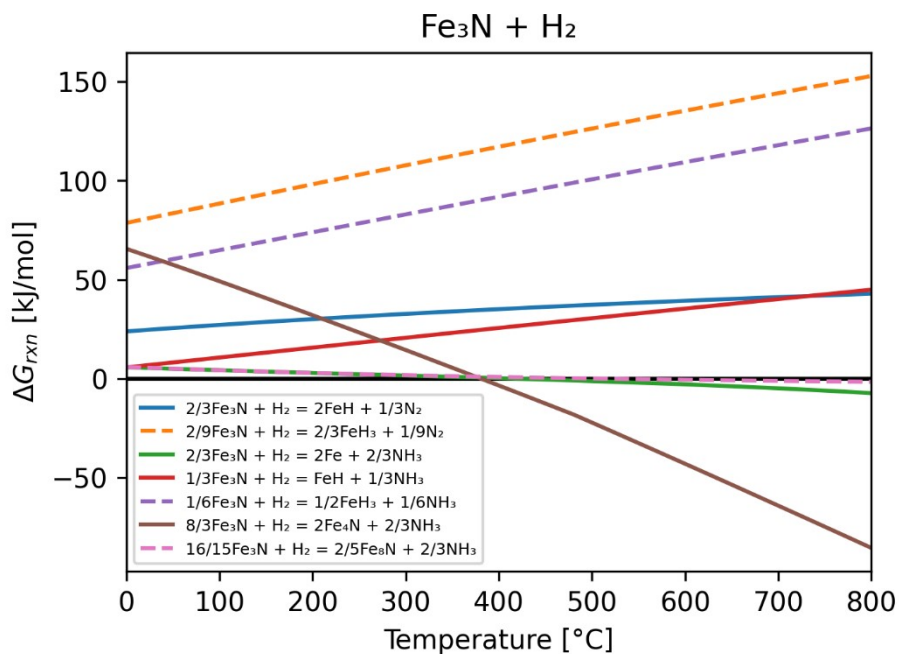


Figure S56: Ellingham diagram of the Fe<sub>3</sub>N hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

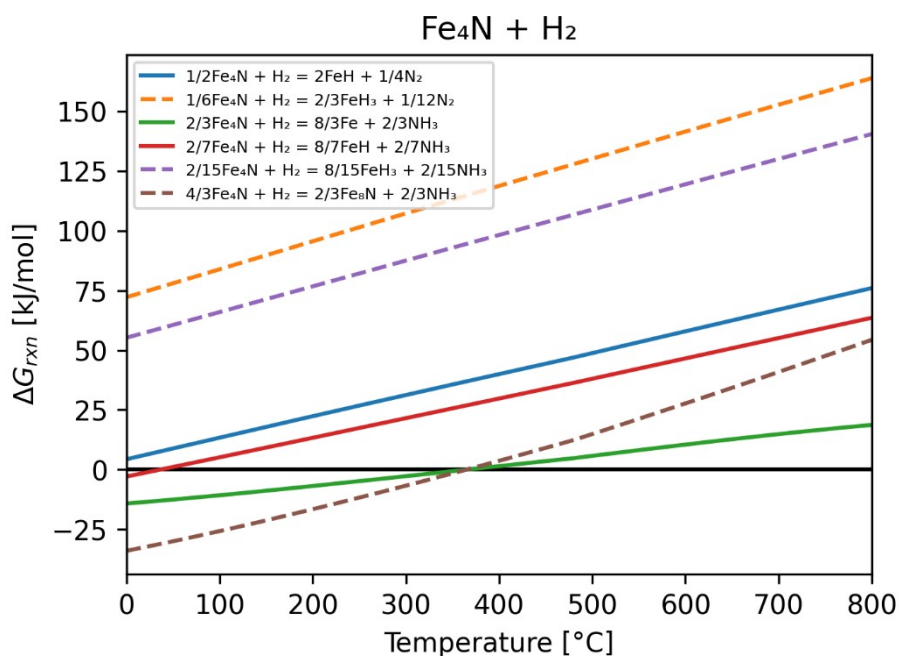


Figure S57: Ellingham diagram of the Fe<sub>4</sub>N hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

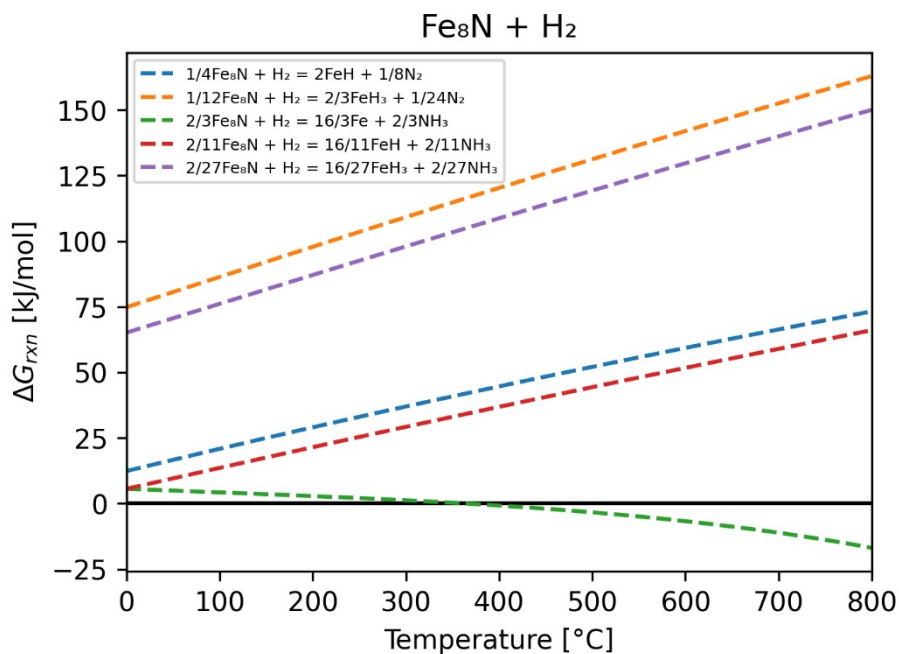


Figure S58: Ellingham diagram of the Fe<sub>8</sub>N hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

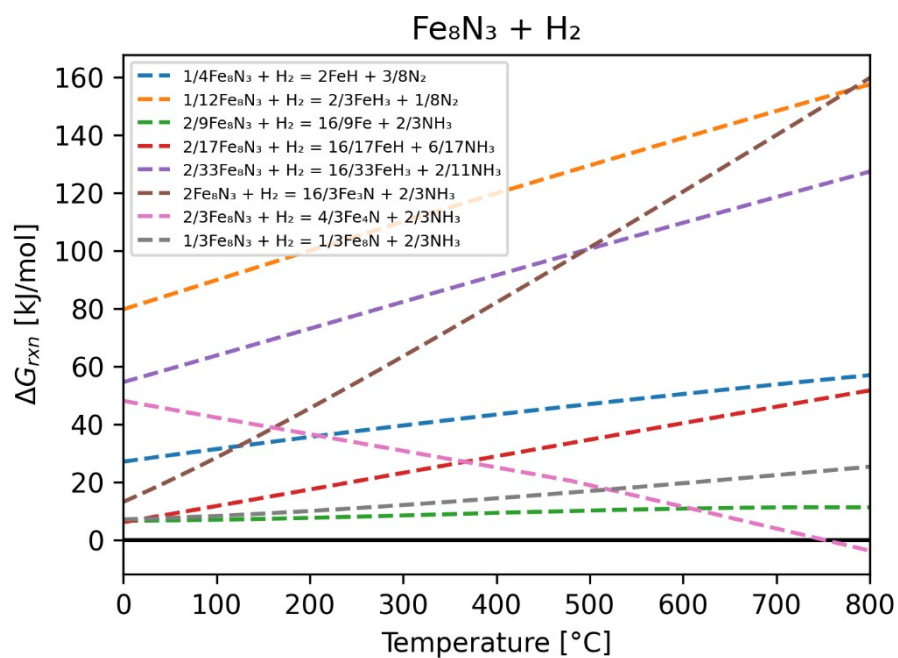


Figure S59: Ellingham diagram of the Fe<sub>8</sub>N<sub>3</sub> hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

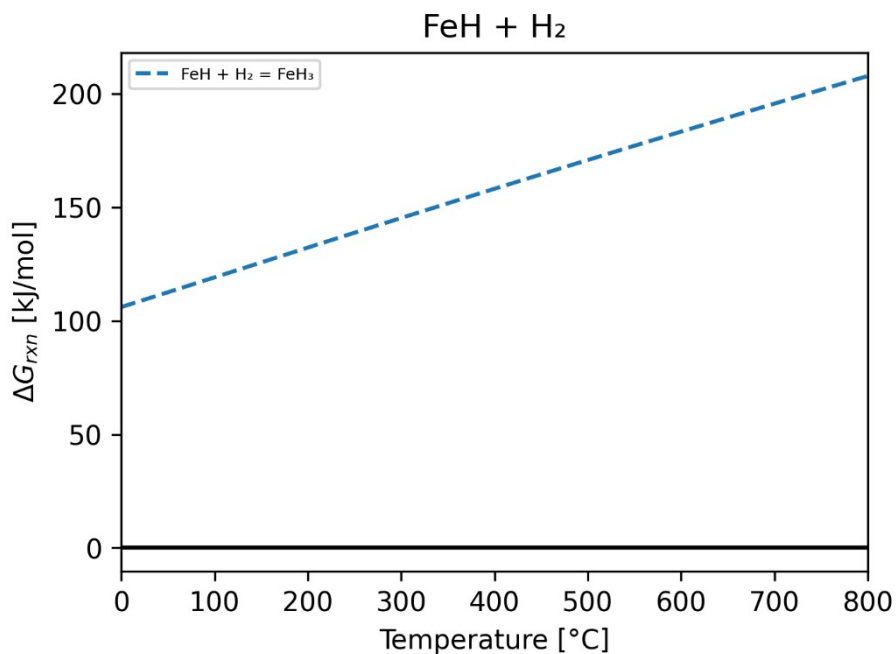


Figure S60: Ellingham diagram of the FeH hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

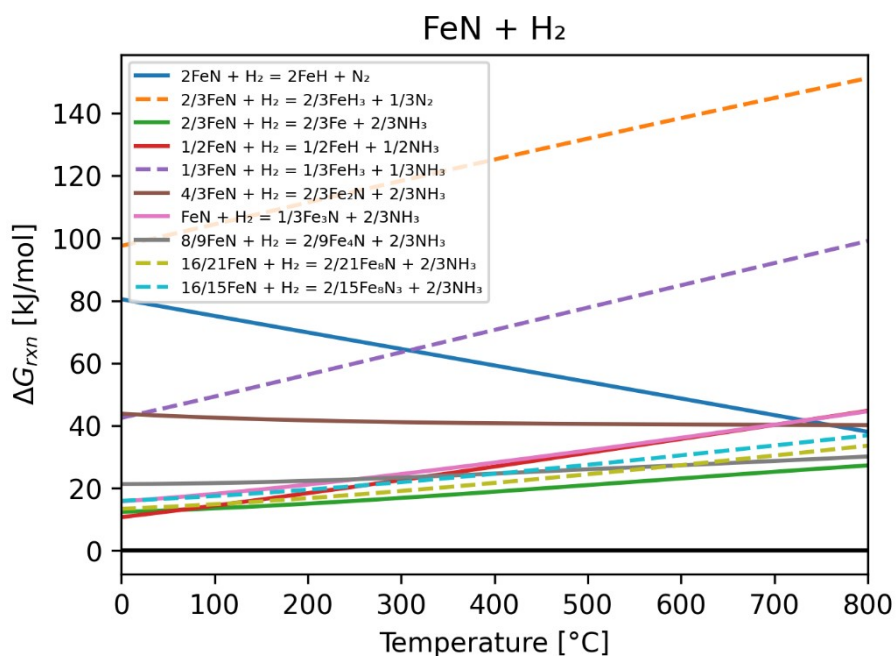


Figure S61: Ellingham diagram of the FeN hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

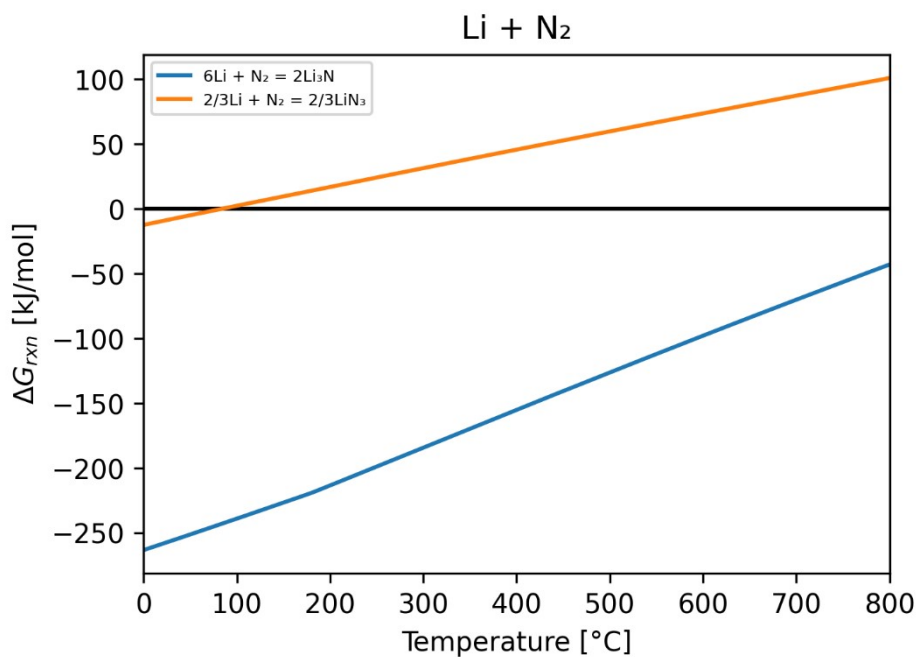


Figure S62: Ellingham diagram of the Li nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

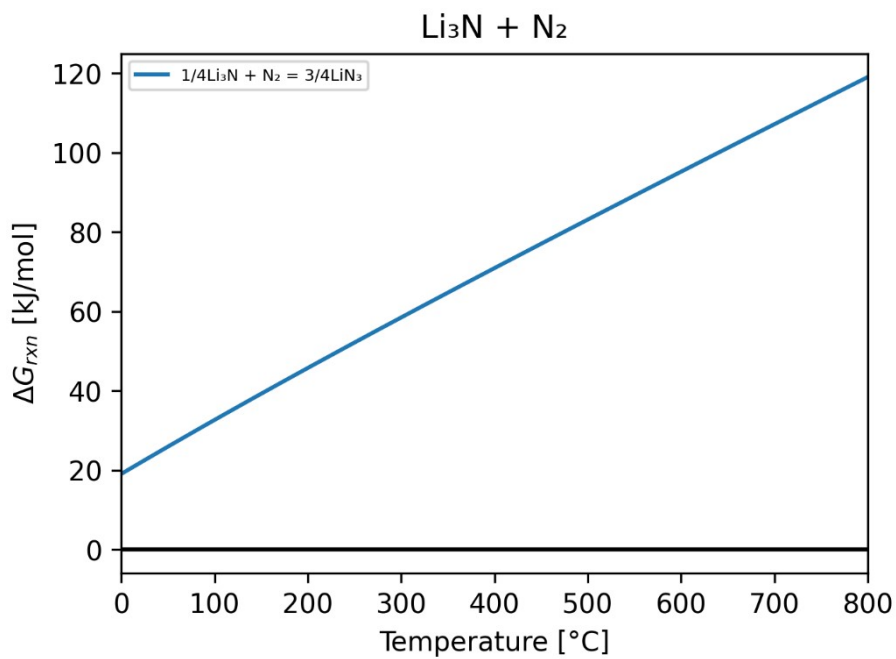


Figure S63: Ellingham diagram of the Li<sub>3</sub>N nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

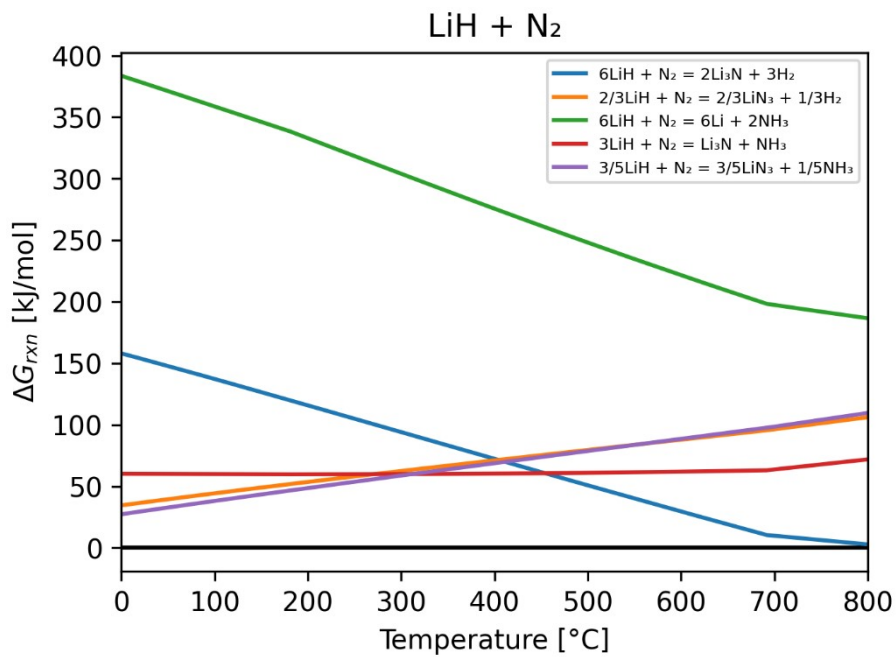


Figure S64: Ellingham diagram of the LiH nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

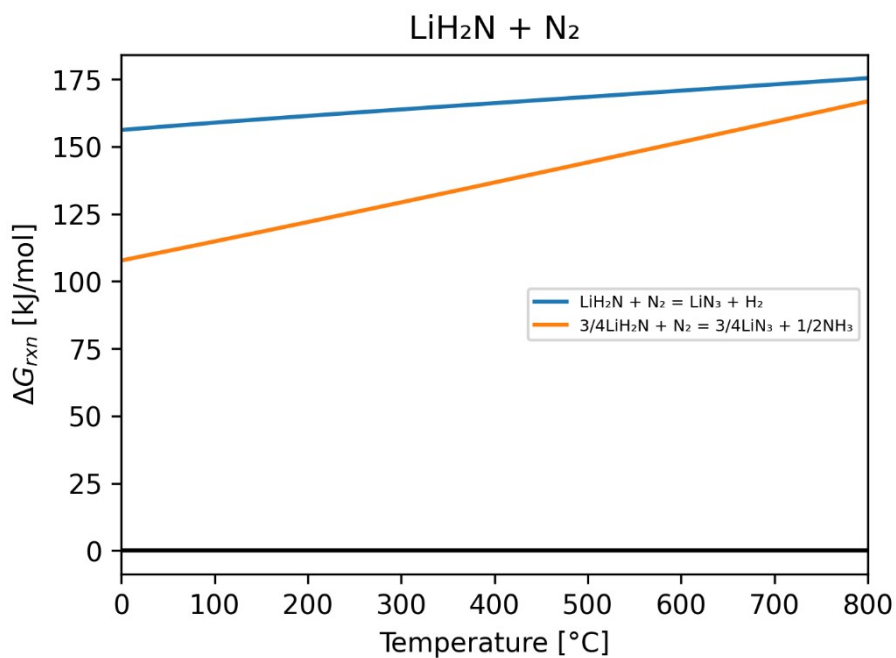


Figure S65: Ellingham diagram of the LiH<sub>2</sub>N nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

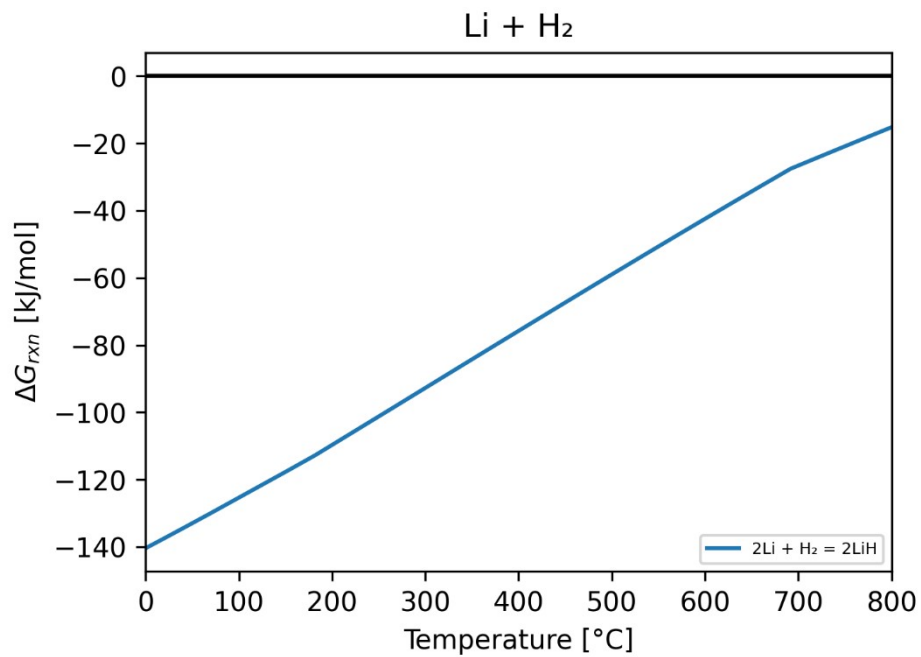


Figure S66: Ellingham diagram of the Li hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

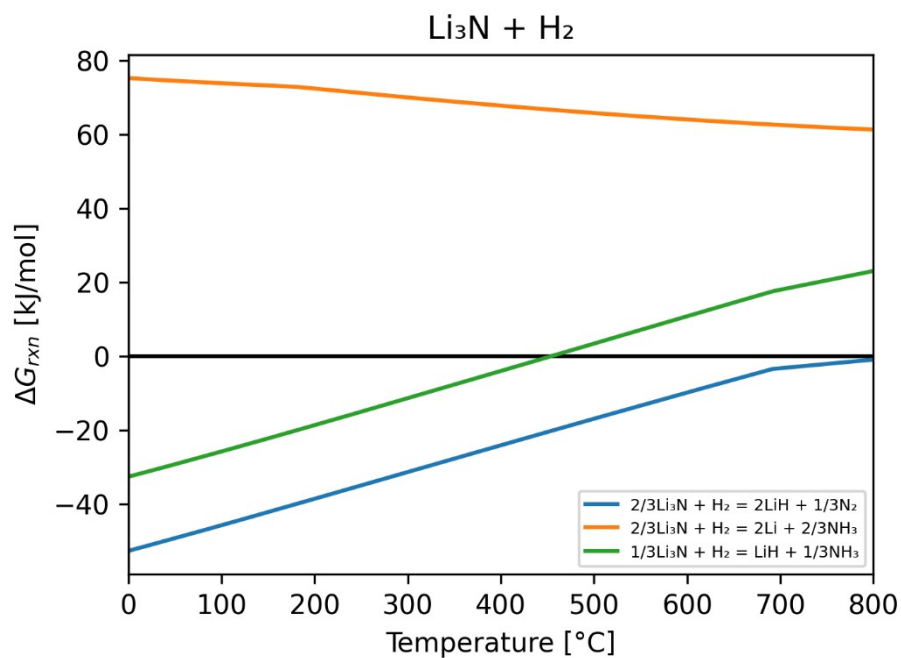


Figure S67: Ellingham diagram of the Li<sub>3</sub>N hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.



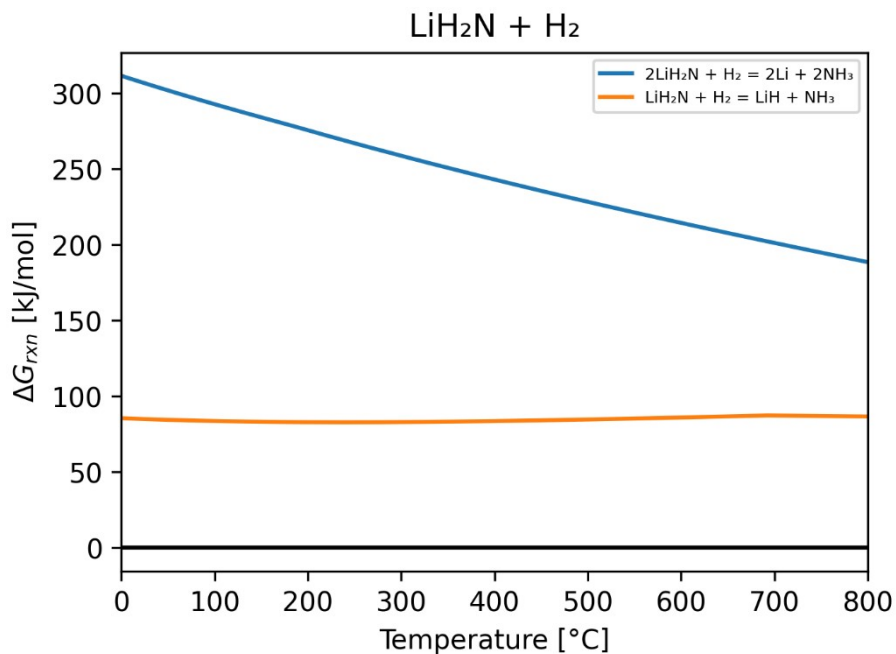


Figure S68: Ellingham diagram of the LiH<sub>2</sub>N hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

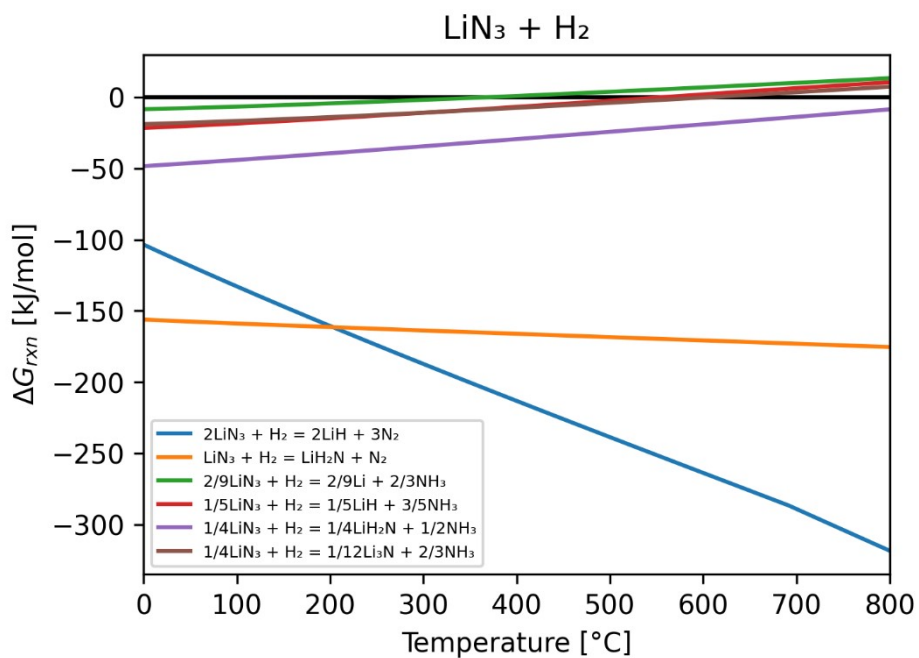


Figure S69: Ellingham diagram of the LiN<sub>3</sub> hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

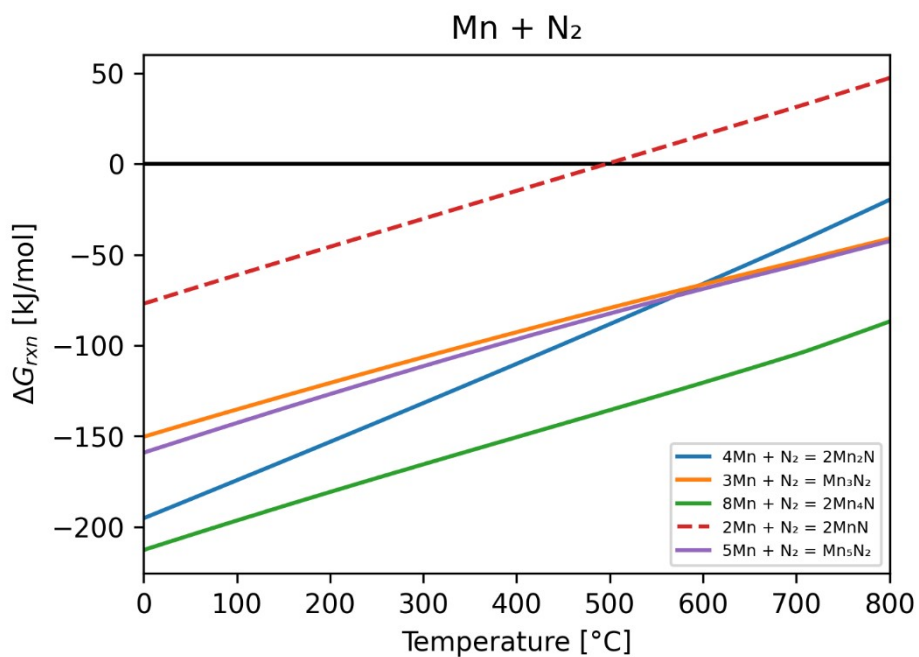


Figure S70: Ellingham diagram of the Mn nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

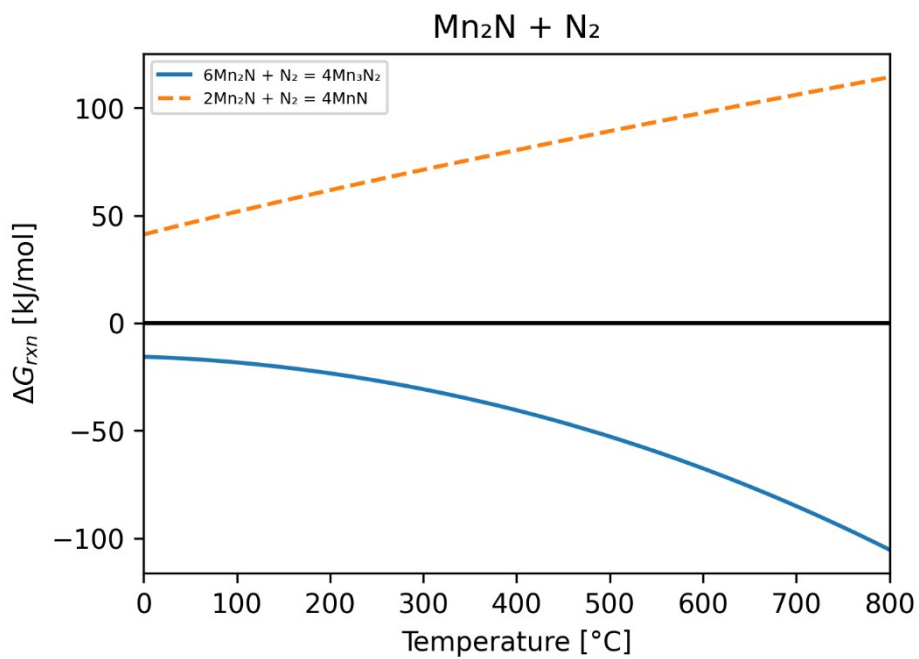


Figure S71: Ellingham diagram of the Mn<sub>2</sub>N nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

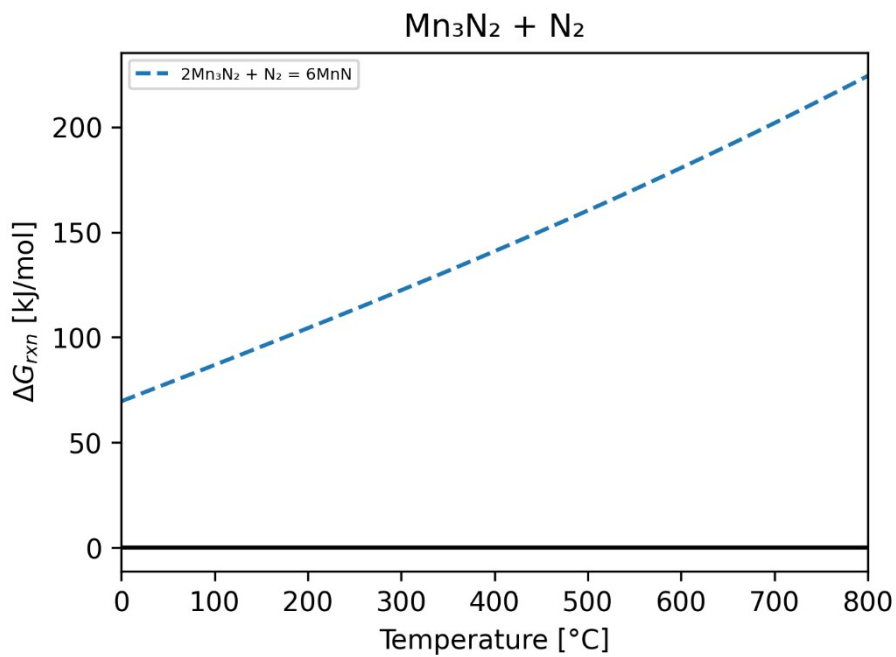


Figure S72: Ellingham diagram of the  $\text{Mn}_3\text{N}_2$  nitridation step: standard Gibbs free energy change per mol  $\text{N}_2$  as a function of temperature.

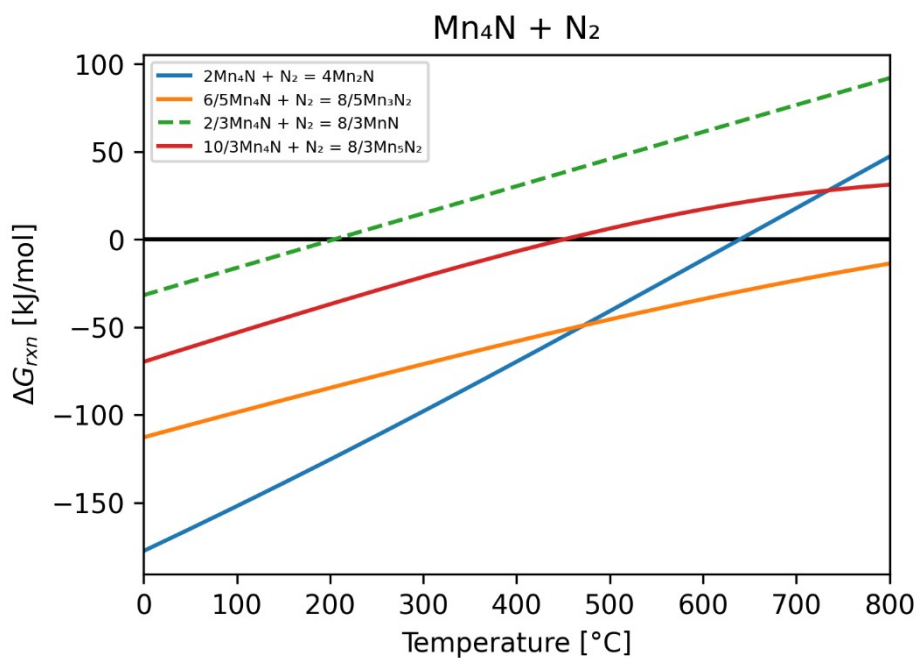


Figure S73: Ellingham diagram of the  $\text{Mn}_4\text{N}$  nitridation step: standard Gibbs free energy change per mol  $\text{N}_2$  as a function of temperature.

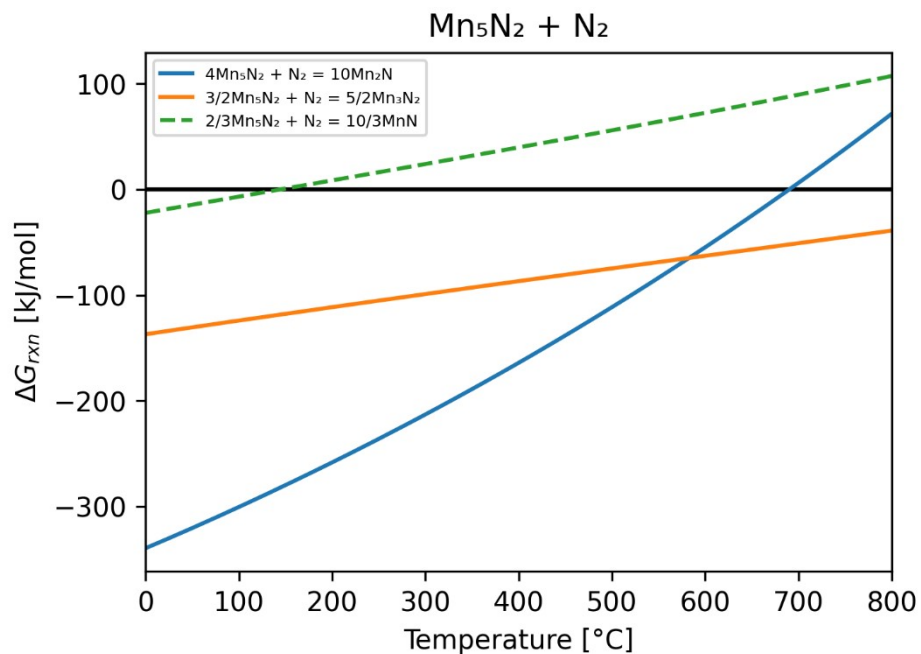


Figure S74: Ellingham diagram of the Mn<sub>5</sub>N<sub>2</sub> nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

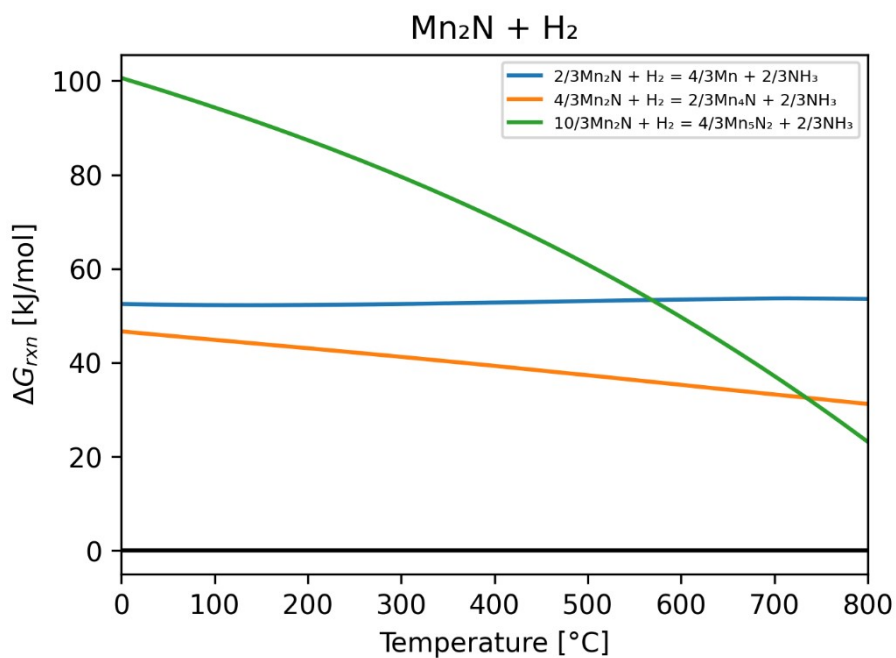


Figure S75: Ellingham diagram of the Mn<sub>2</sub>N hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

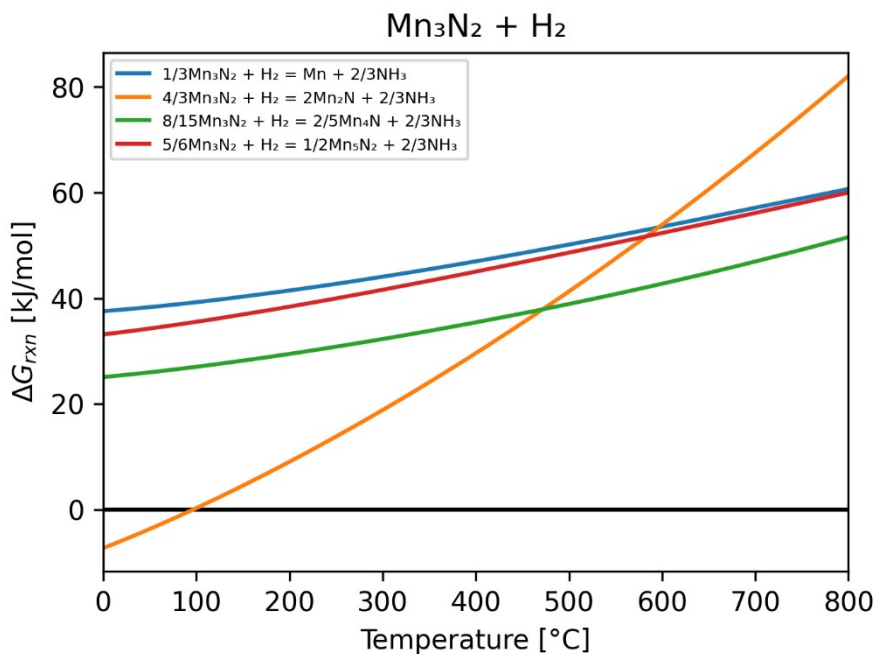


Figure S76: Ellingham diagram of the Mn<sub>3</sub>N<sub>2</sub> hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

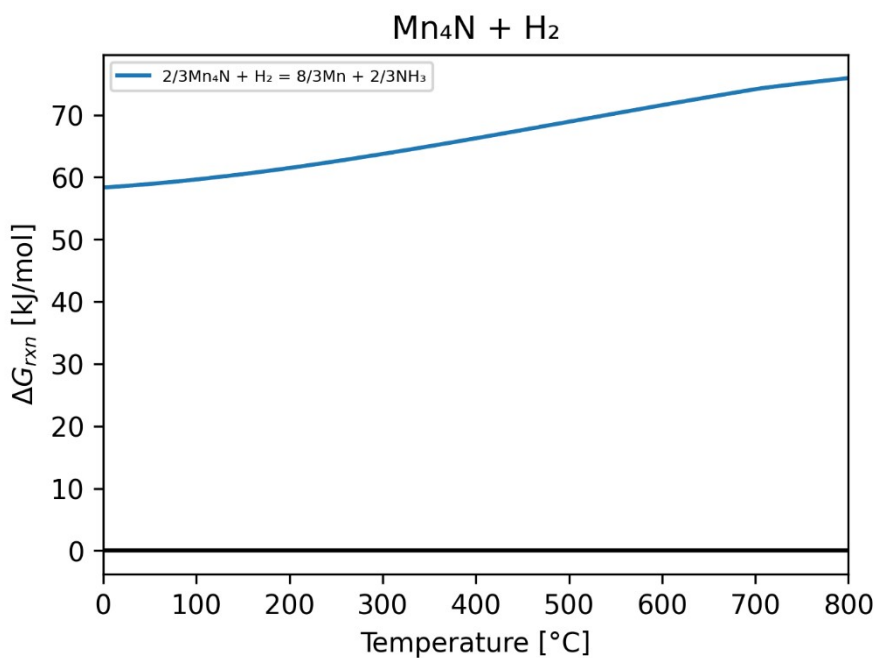


Figure S77: Ellingham diagram of the Mn<sub>4</sub>N hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

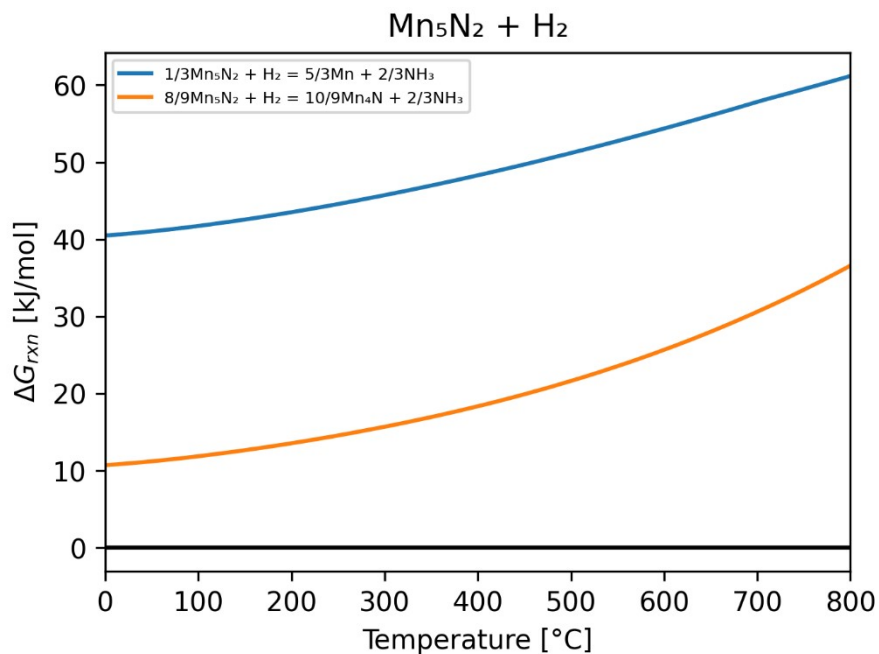


Figure S78: Ellingham diagram of the Mn<sub>5</sub>N<sub>2</sub> hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

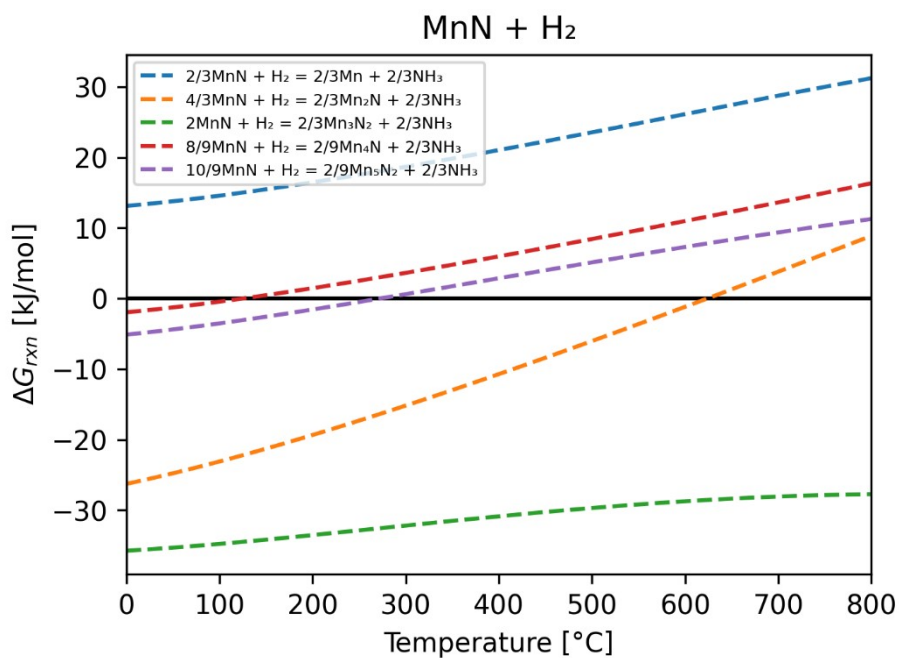


Figure S79: Ellingham diagram of the MnN hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

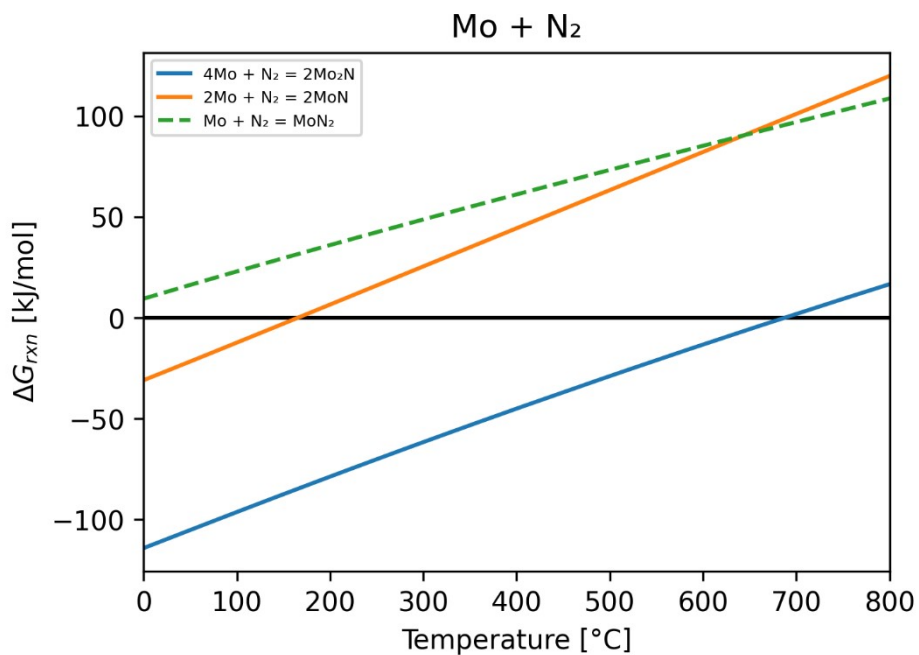


Figure S80: Ellingham diagram of the Mo nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

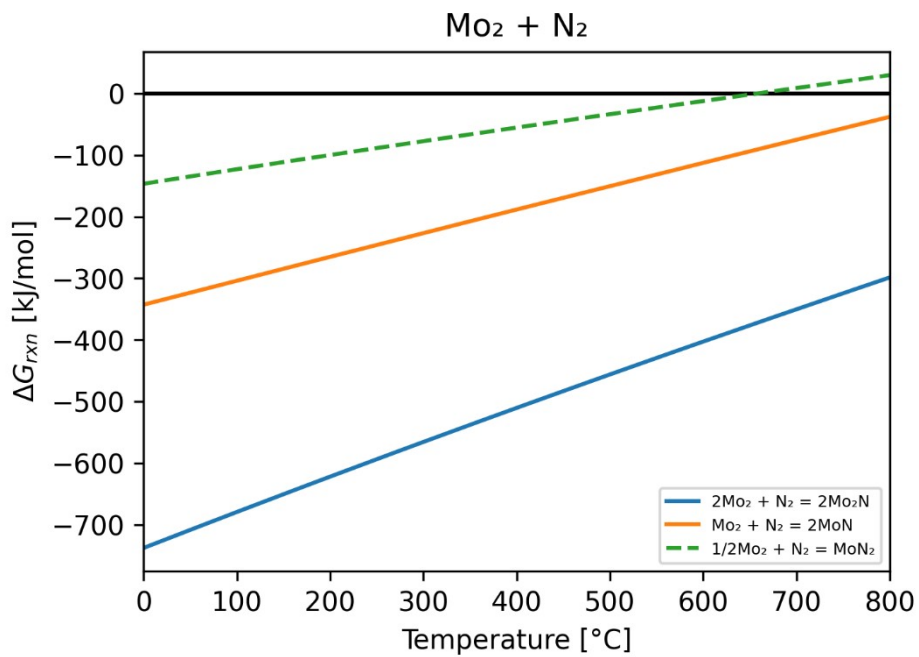


Figure S81: Ellingham diagram of the Mo<sub>2</sub> nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

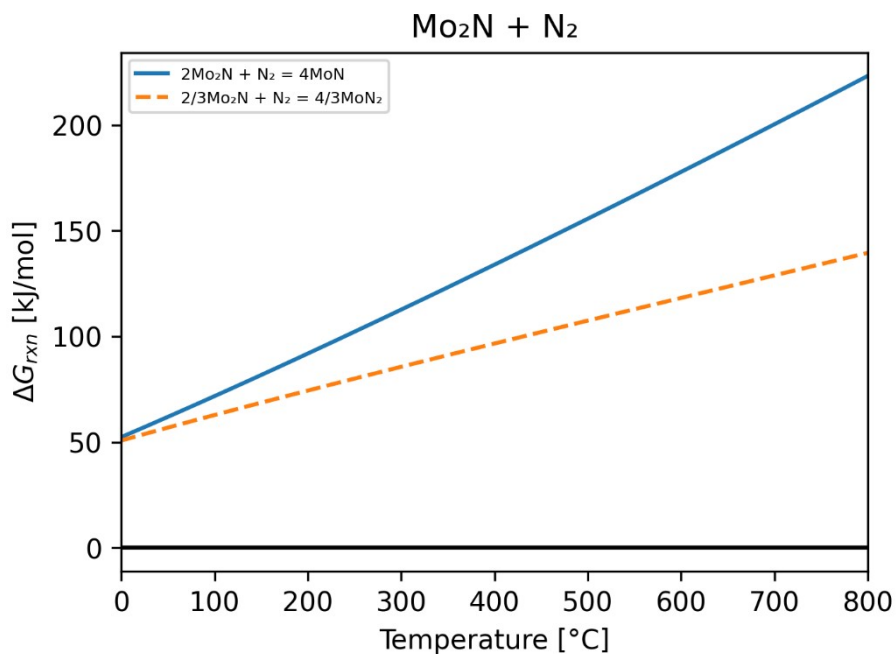


Figure S82: Ellingham diagram of the Mo<sub>2</sub>N nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

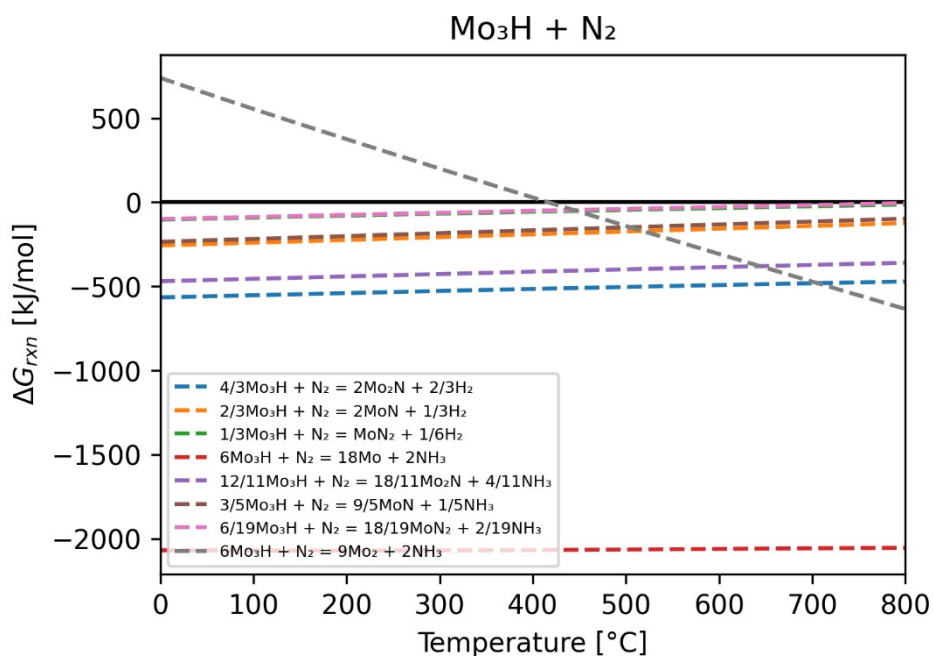


Figure S83: Ellingham diagram of the Mo<sub>3</sub>H nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.



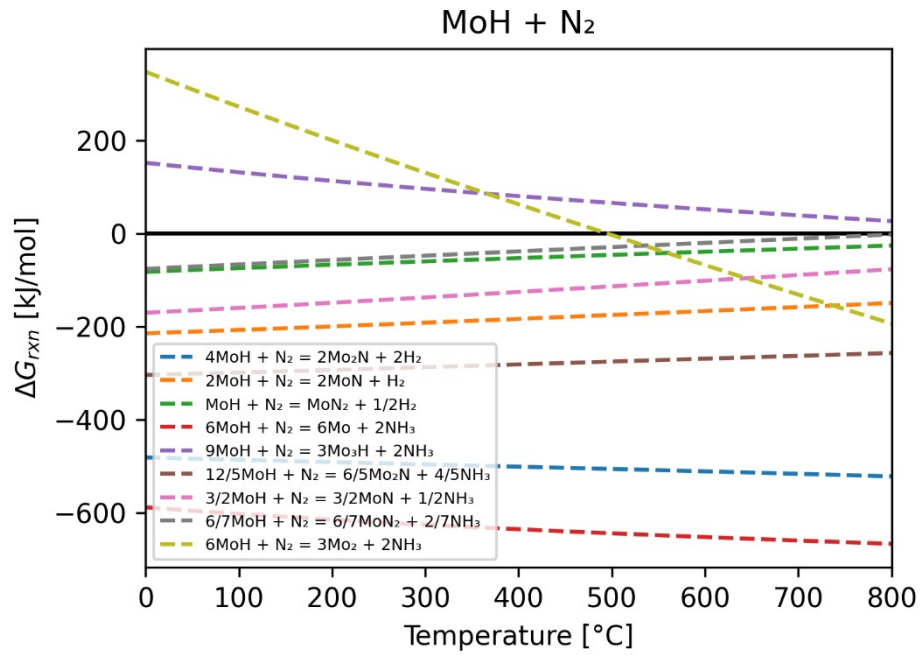


Figure S84: Ellingham diagram of the MoH nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

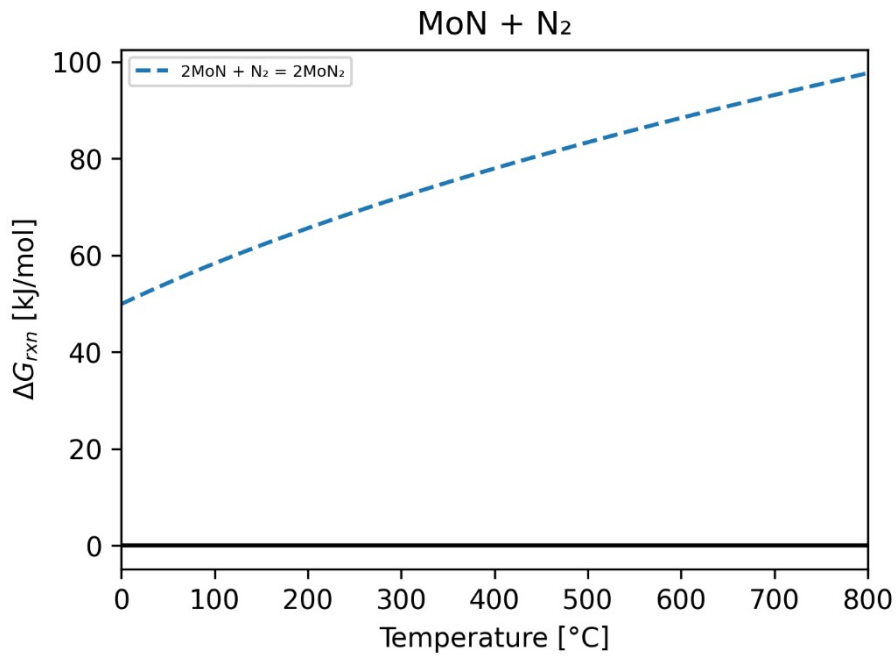


Figure S85: Ellingham diagram of the MoN nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

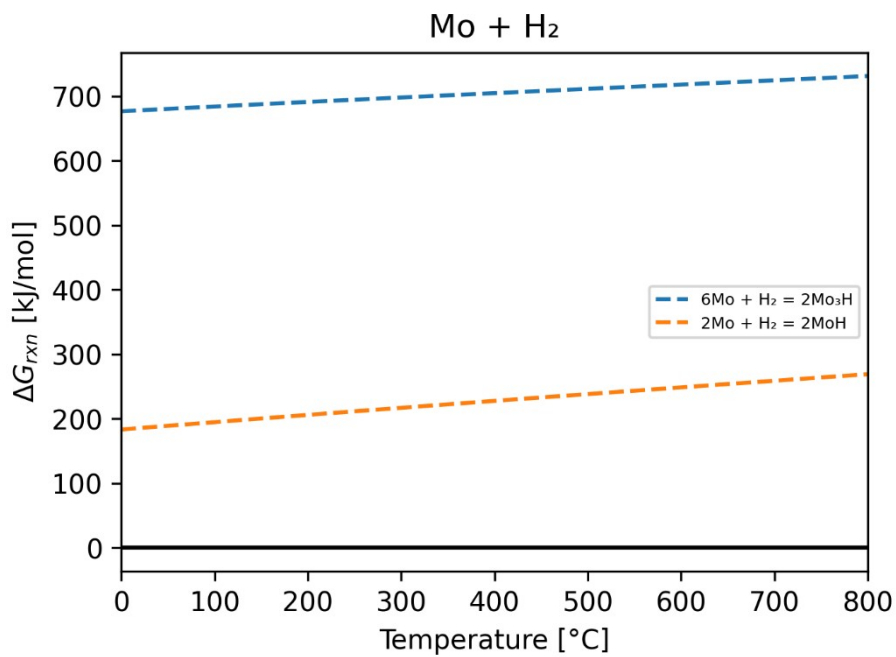


Figure S86: Ellingham diagram of the Mo hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

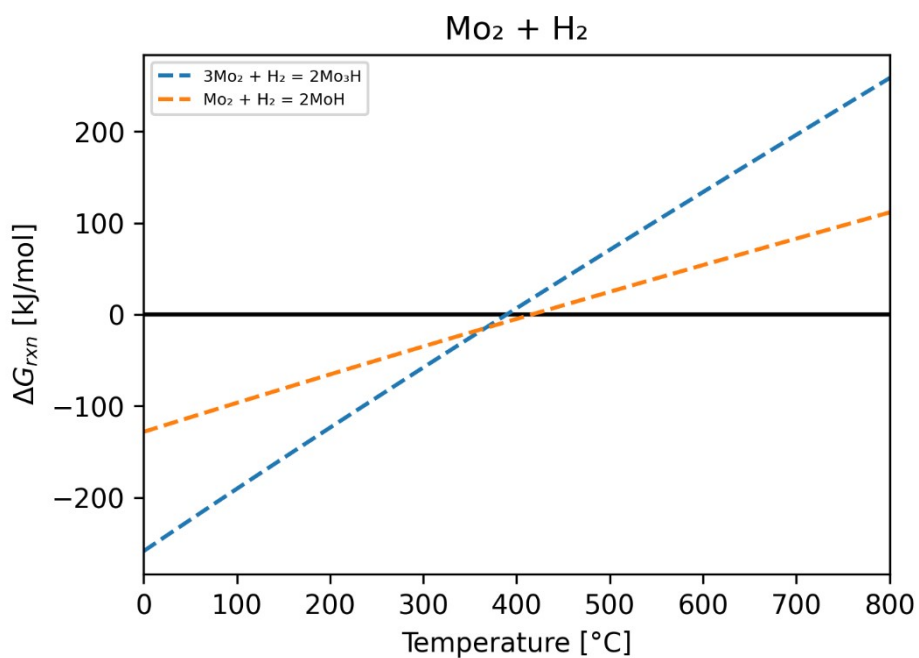


Figure S87: Ellingham diagram of the Mo<sub>2</sub> hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

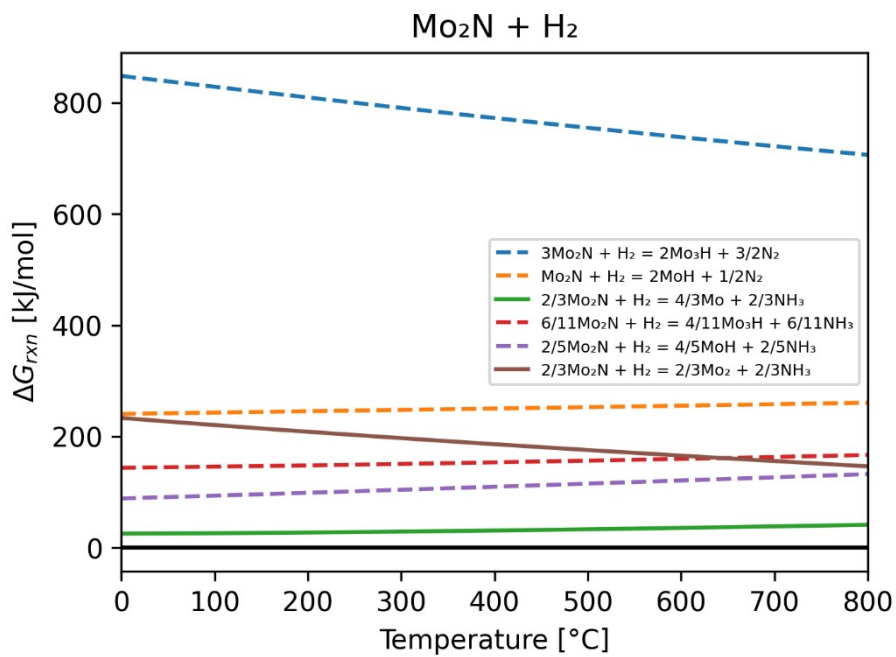


Figure S88: Ellingham diagram of the Mo<sub>2</sub>N hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

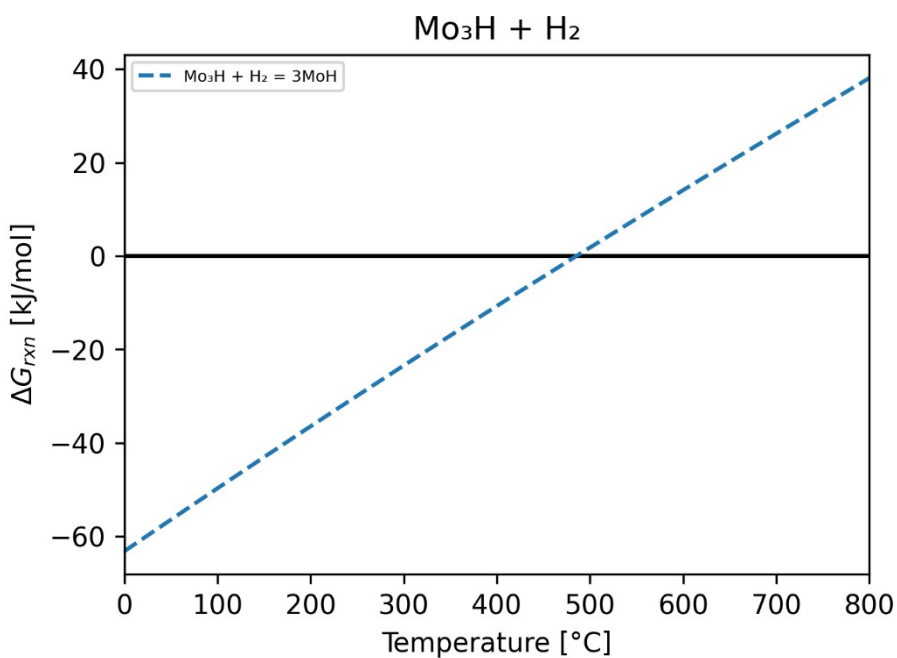


Figure S89: Ellingham diagram of the Mo<sub>3</sub>H hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

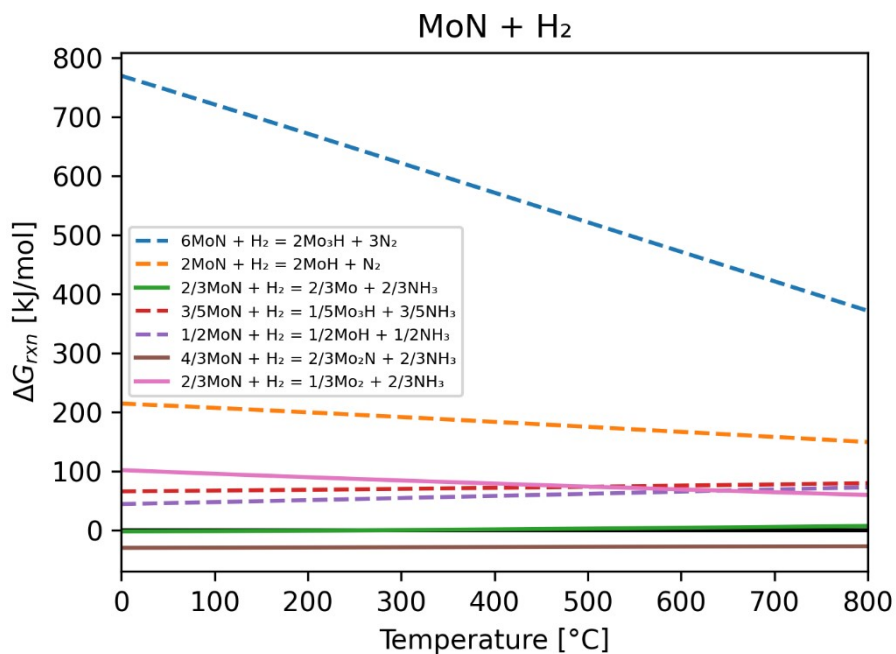


Figure S90: Ellingham diagram of the MoN hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

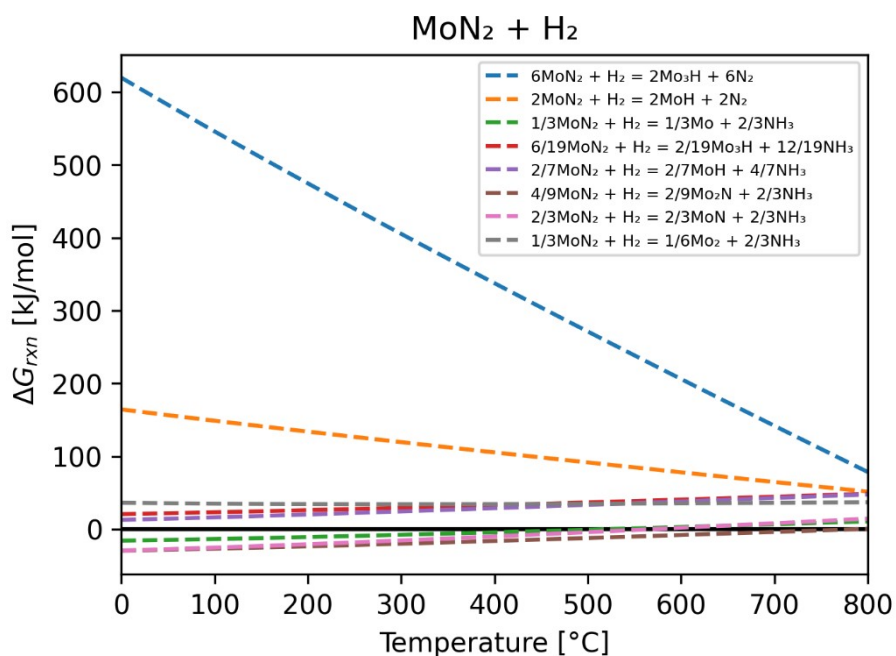


Figure S91: Ellingham diagram of the MoN<sub>2</sub> hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

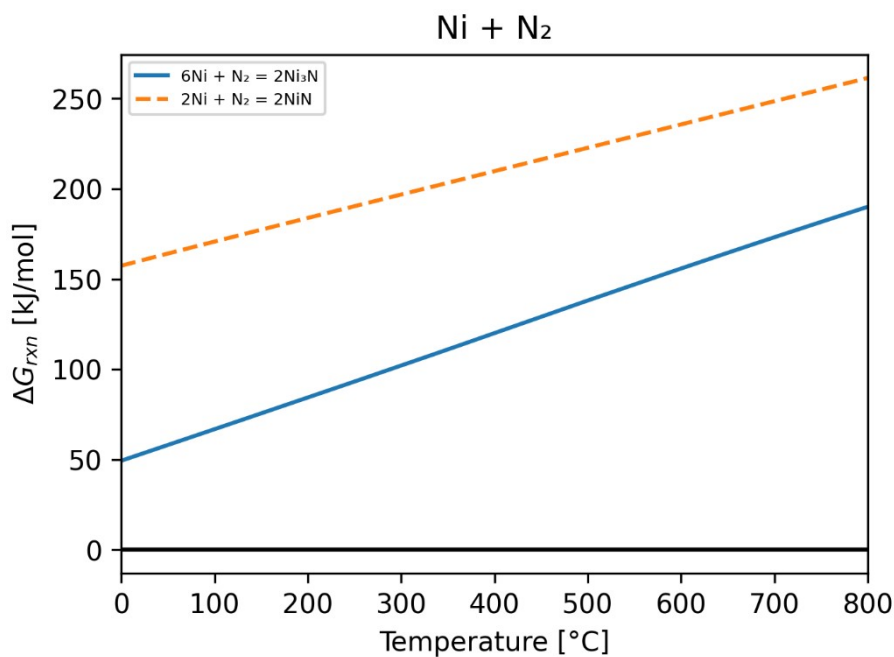


Figure S92: Ellingham diagram of the Ni nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

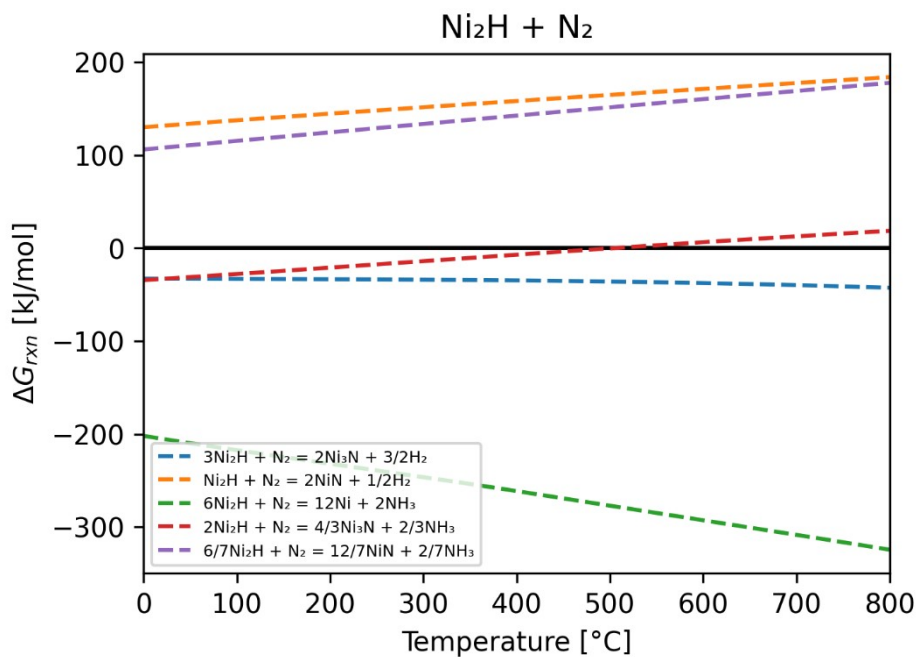


Figure S93: Ellingham diagram of the Ni<sub>2</sub>H nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

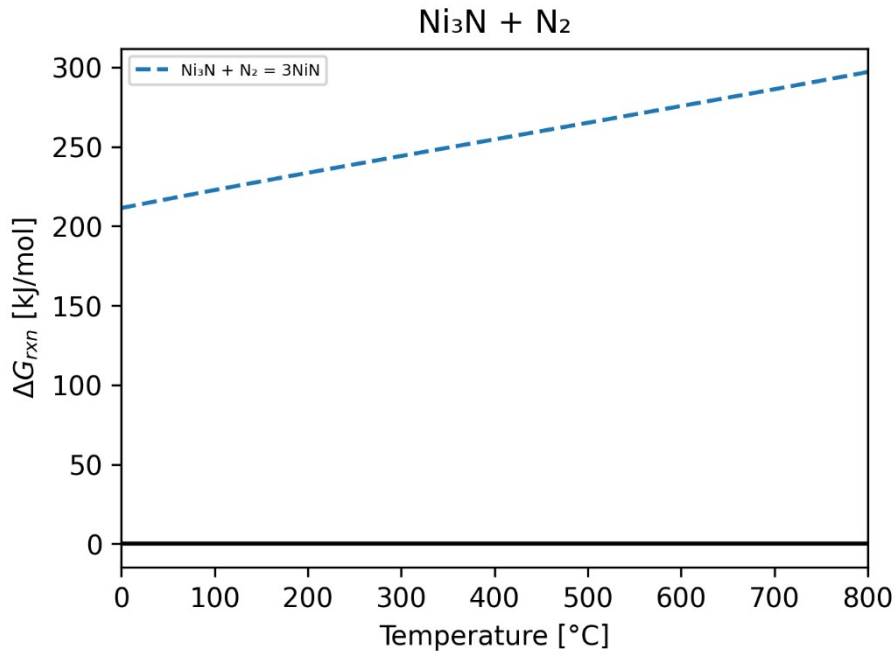


Figure S94: Ellingham diagram of the Ni<sub>3</sub>N nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

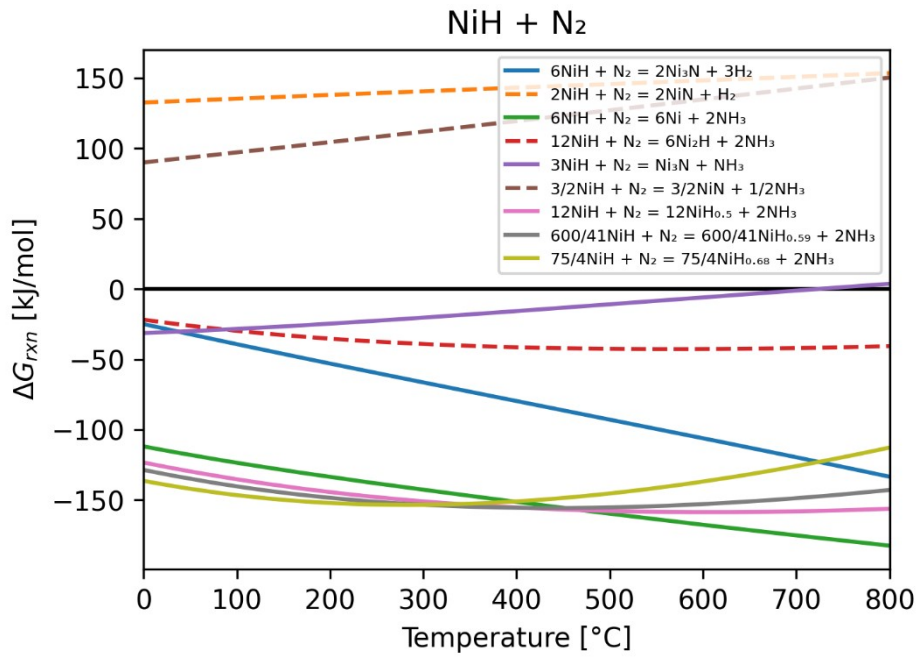


Figure S95: Ellingham diagram of the NiH nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

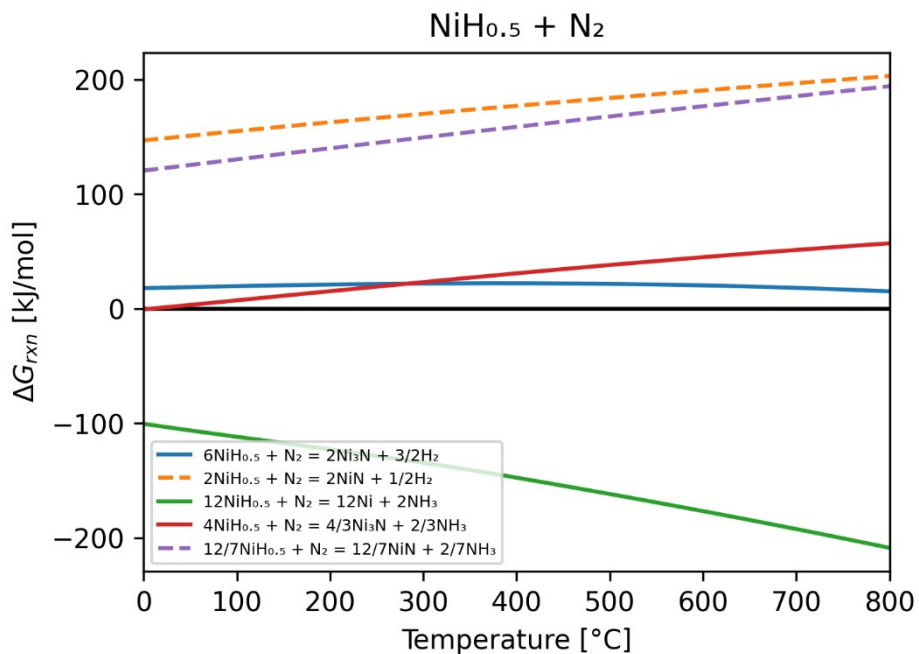


Figure S96: Ellingham diagram of the NiH<sub>0.5</sub> nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

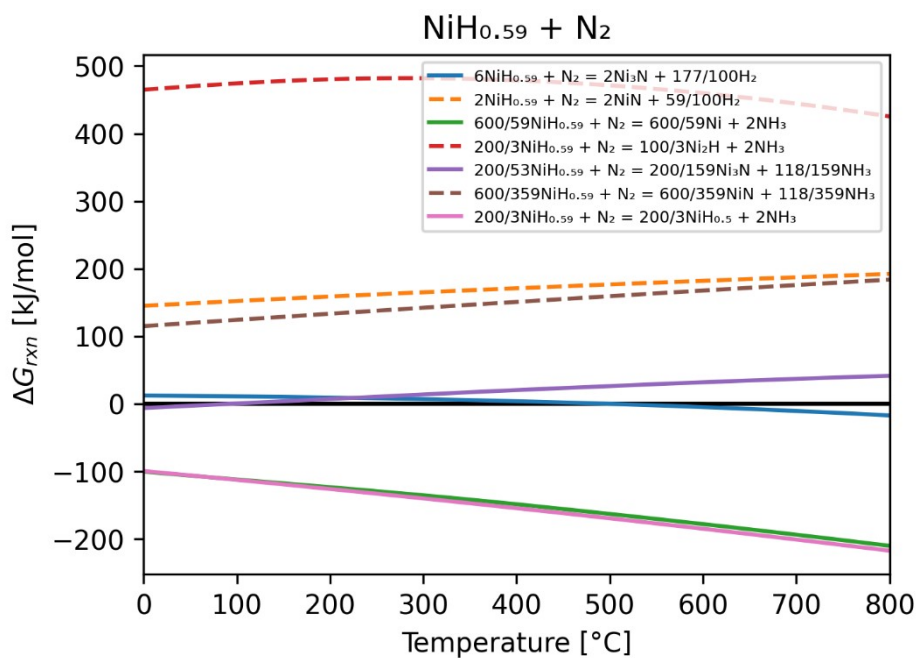


Figure S97: Ellingham diagram of the NiH<sub>0.59</sub> nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

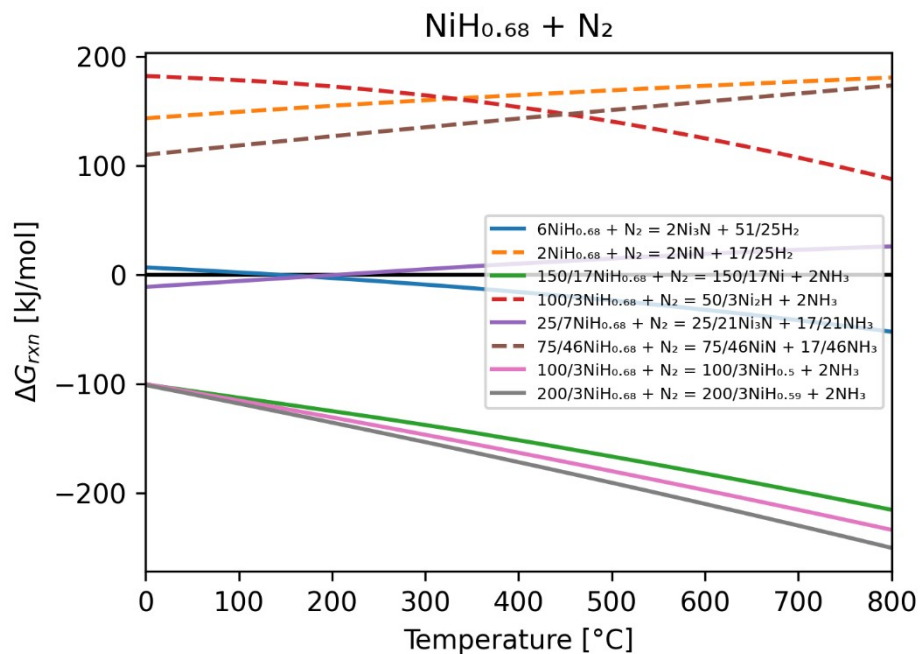


Figure S98: Ellingham diagram of the NiH<sub>0.68</sub> nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

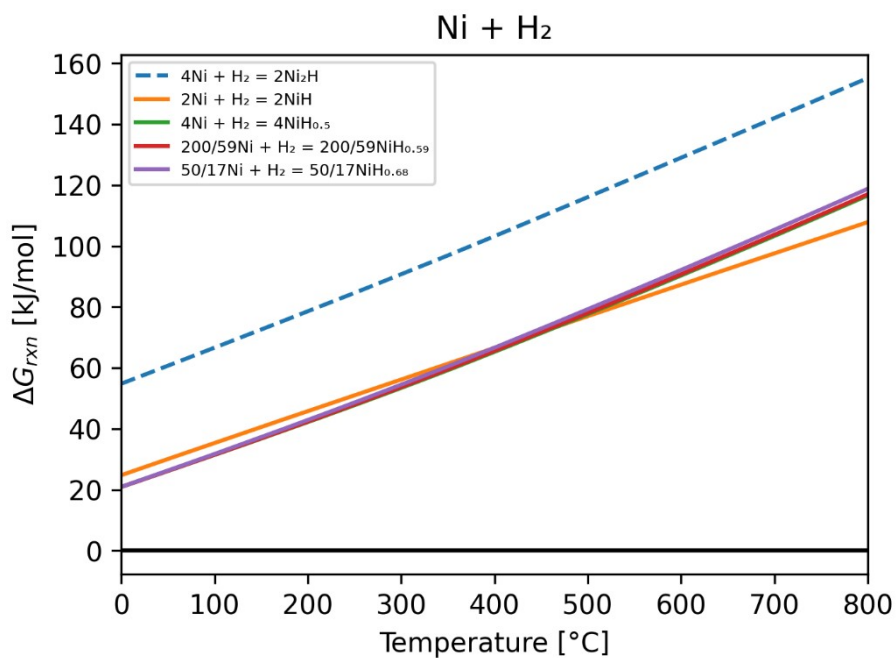


Figure S99: Ellingham diagram of the Ni hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.



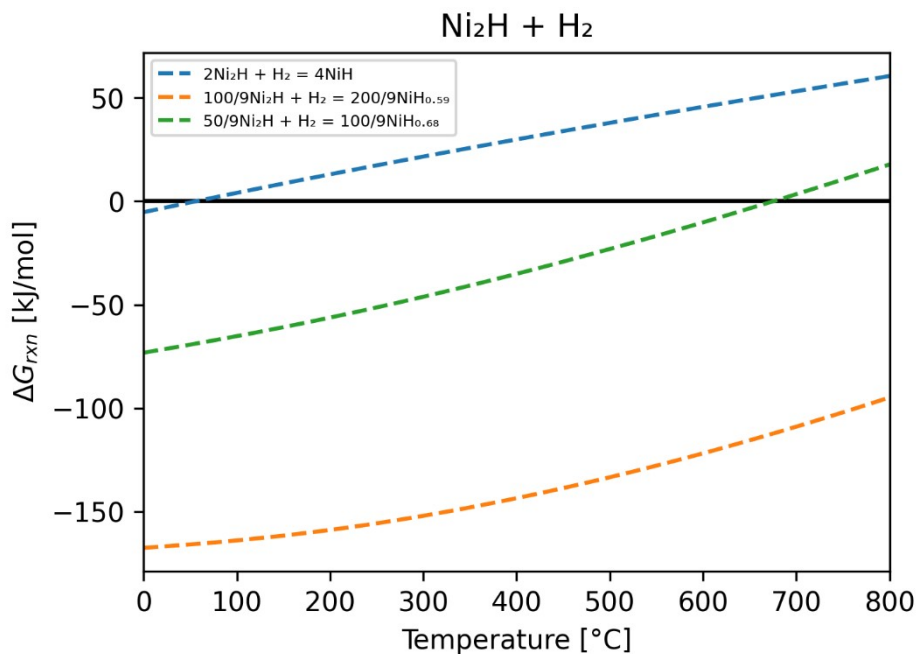


Figure S100: Ellingham diagram of the Ni<sub>2</sub>H hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

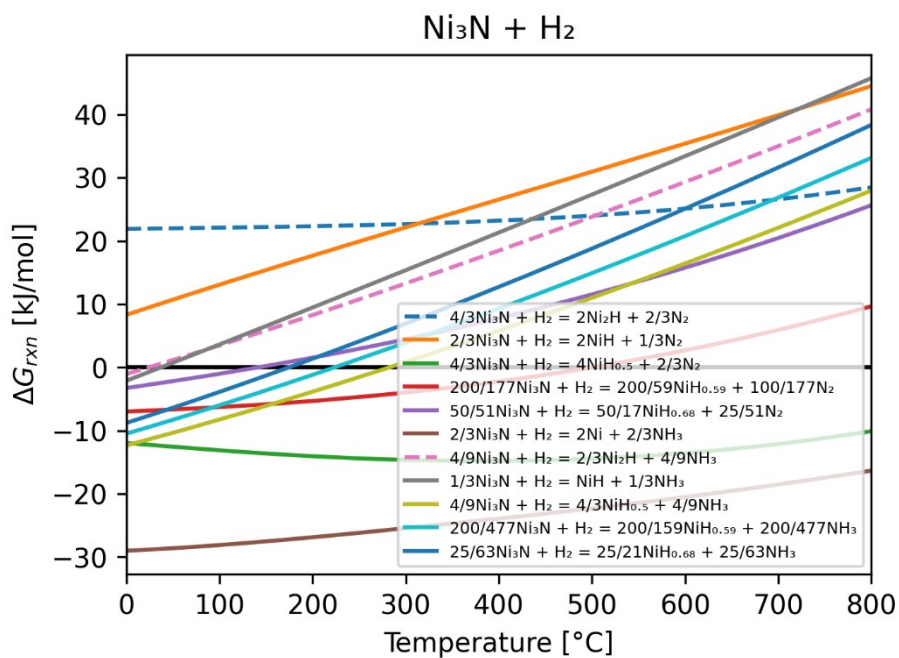


Figure S101: Ellingham diagram of the Ni<sub>3</sub>N hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

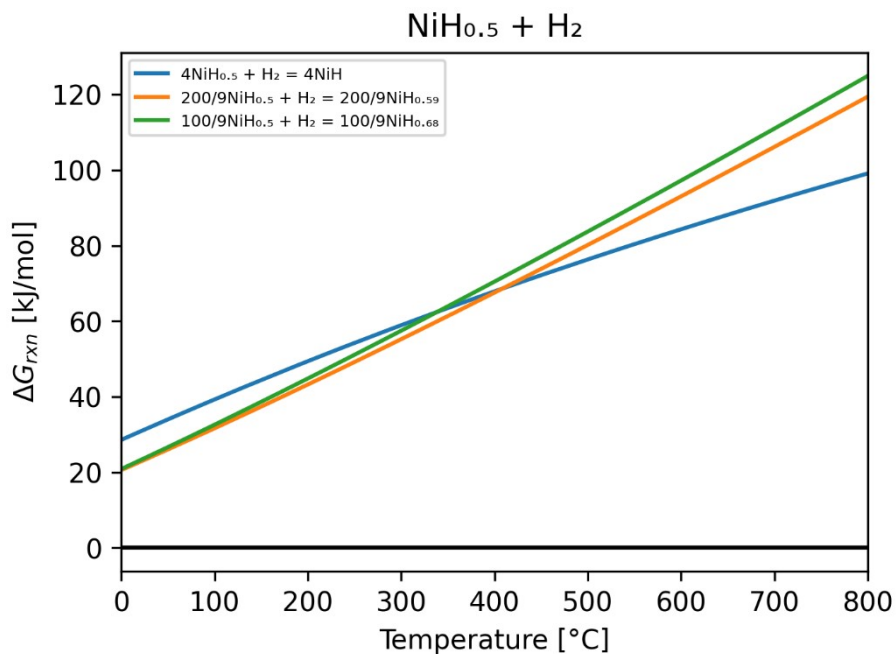


Figure S102: Ellingham diagram of the NiH<sub>0.5</sub> hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

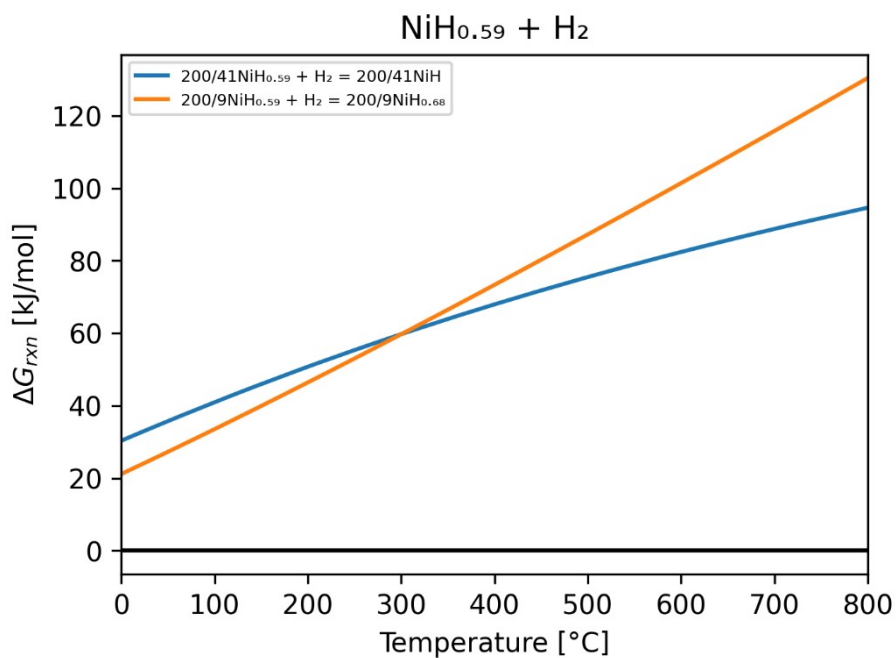


Figure S103: Ellingham diagram of the NiH<sub>0.59</sub> hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

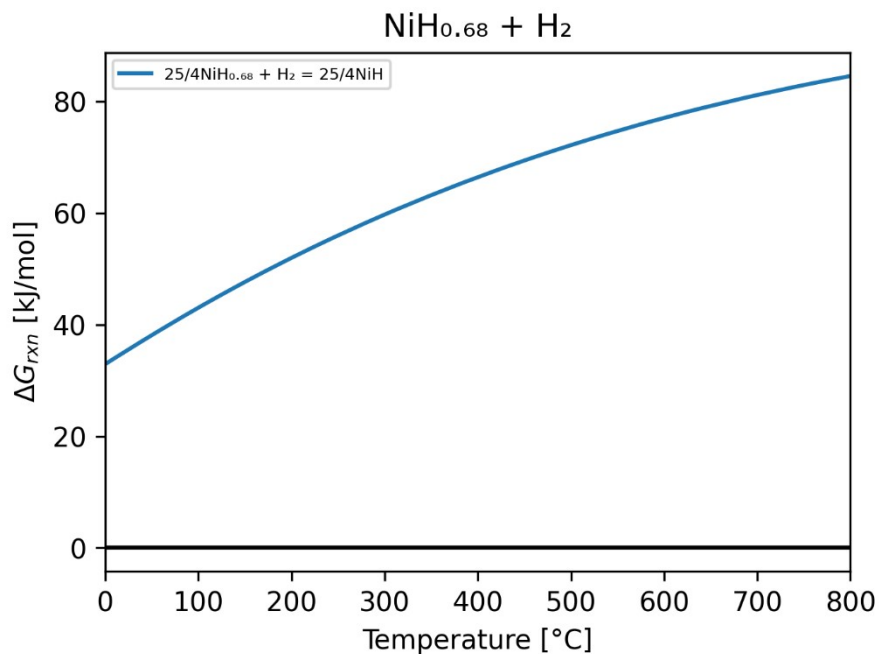


Figure S104: Ellingham diagram of the NiH<sub>0.68</sub> hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

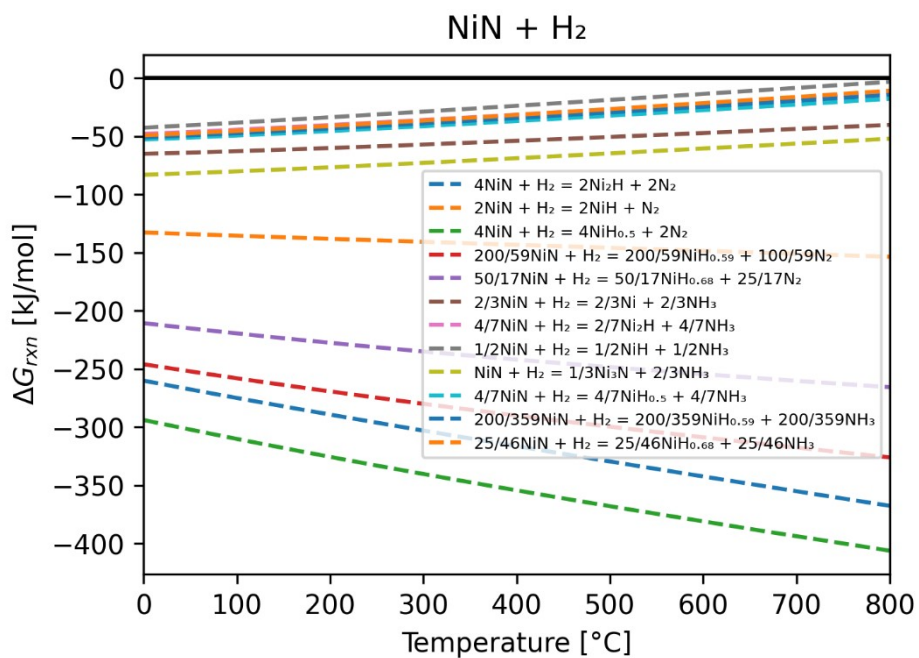


Figure S105: Ellingham diagram of the NiN hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

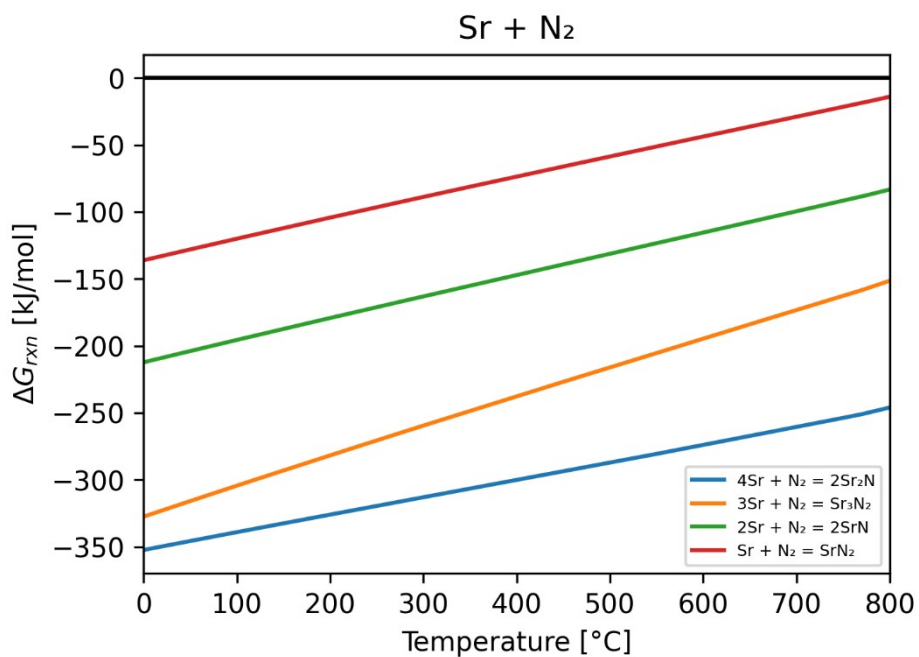


Figure S106: Ellingham diagram of the Sr nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

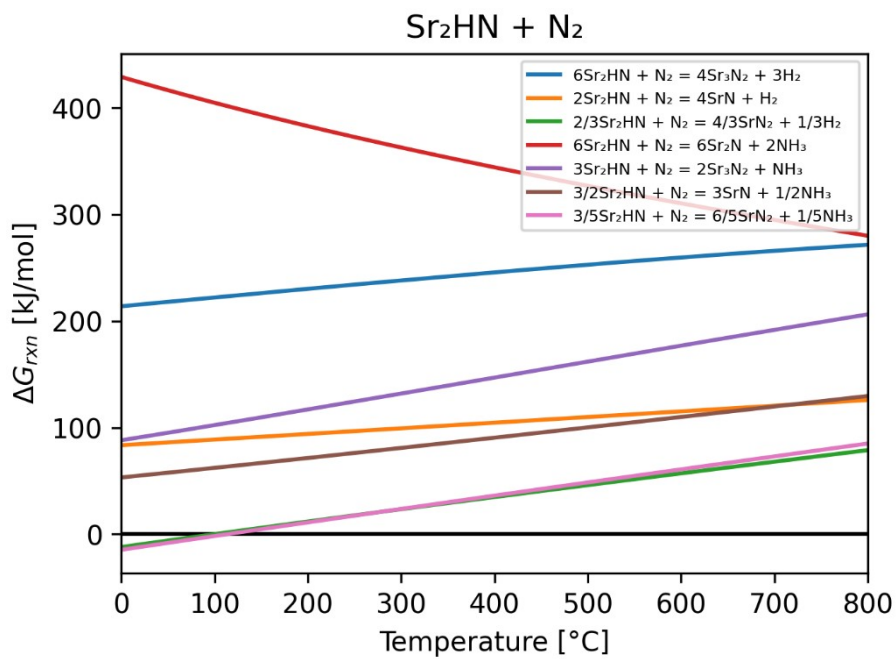


Figure S107: Ellingham diagram of the Sr<sub>2</sub>HN nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

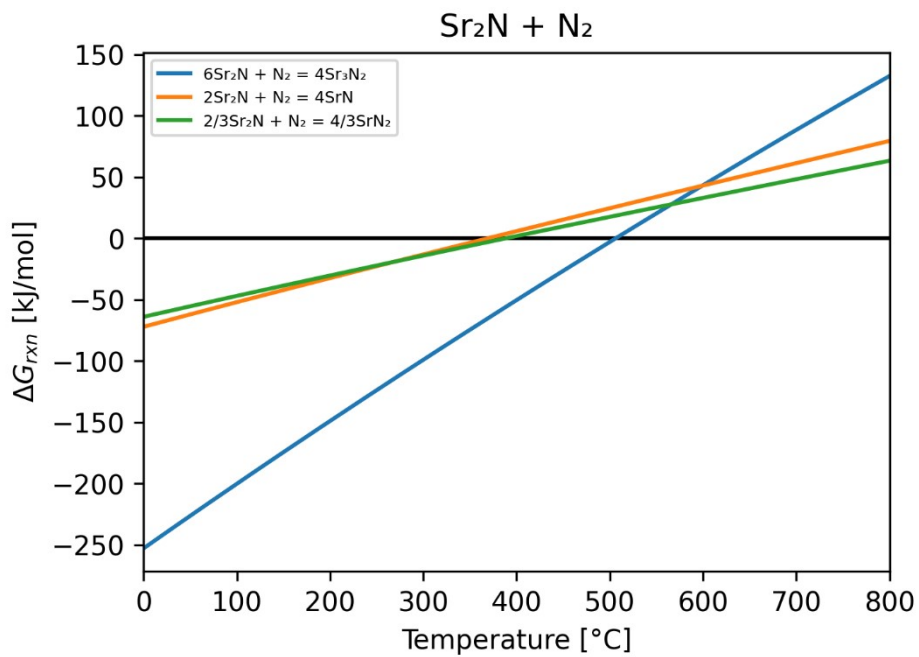


Figure S108: Ellingham diagram of the Sr<sub>2</sub>N nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

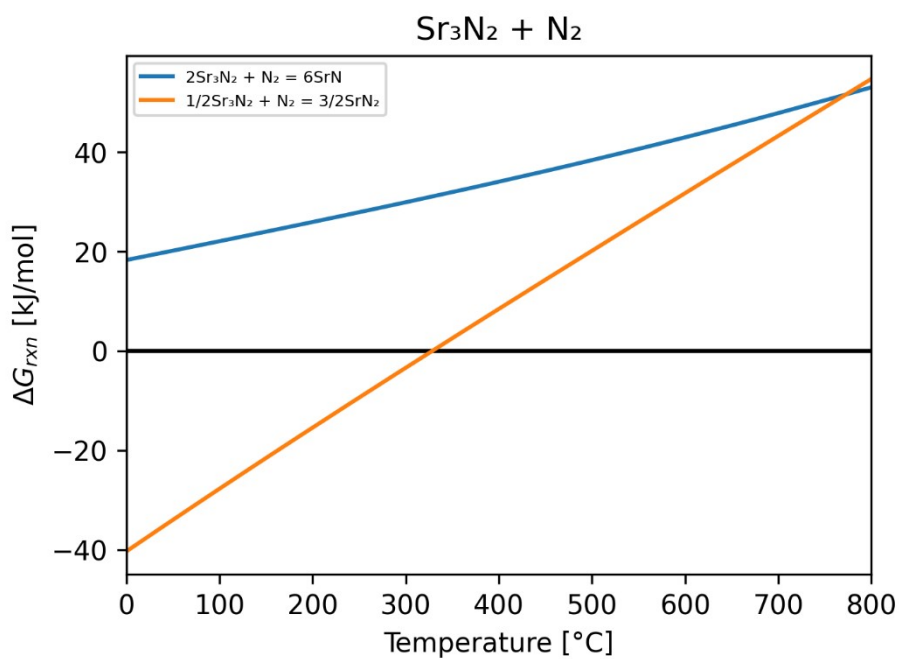


Figure S109: Ellingham diagram of the Sr<sub>3</sub>N<sub>2</sub> nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

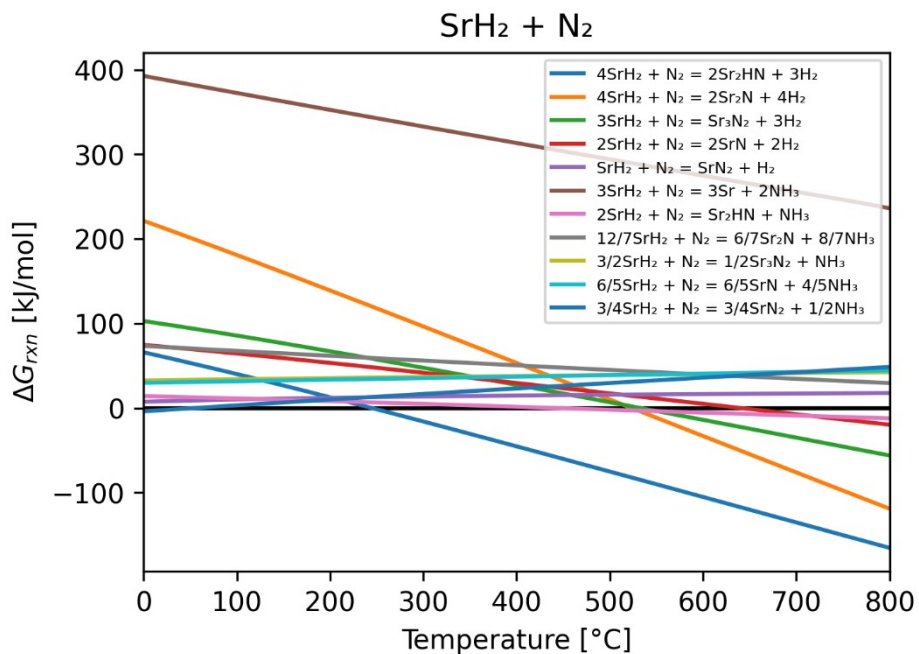


Figure S110: Ellingham diagram of the SrH<sub>2</sub> nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

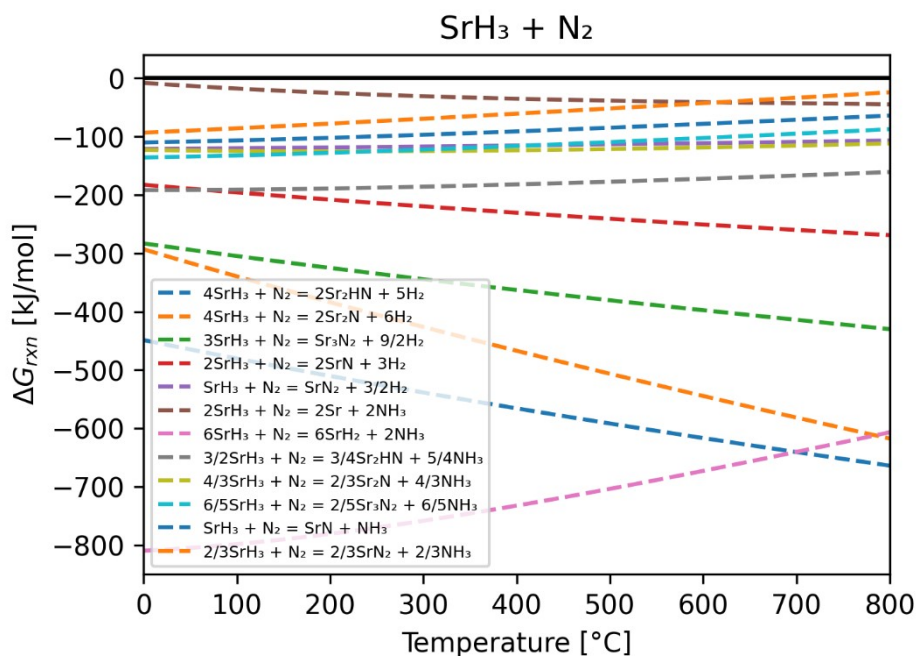


Figure S111: Ellingham diagram of the SrH<sub>3</sub> nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

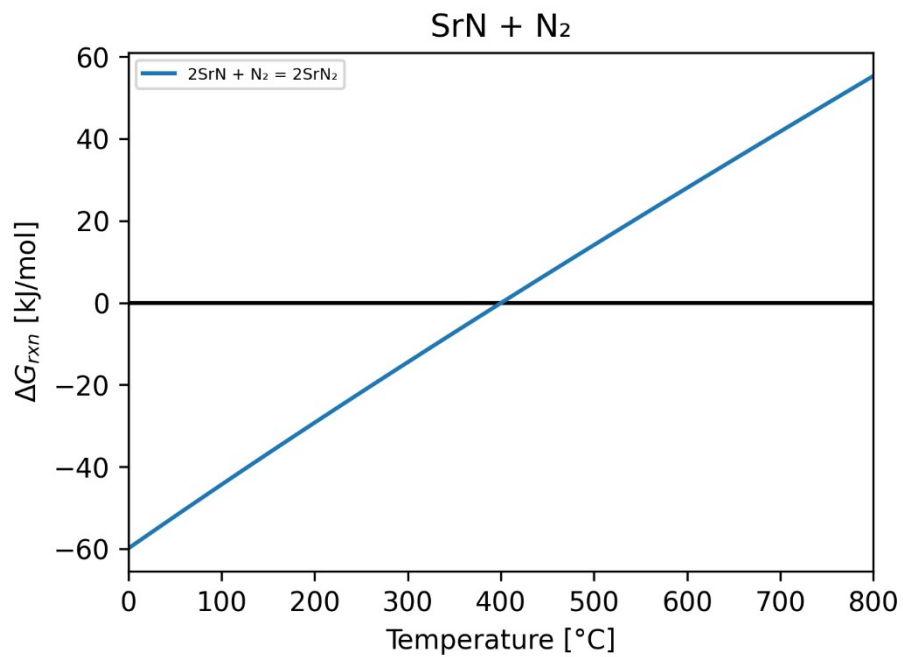


Figure S112: Ellingham diagram of the SrN nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

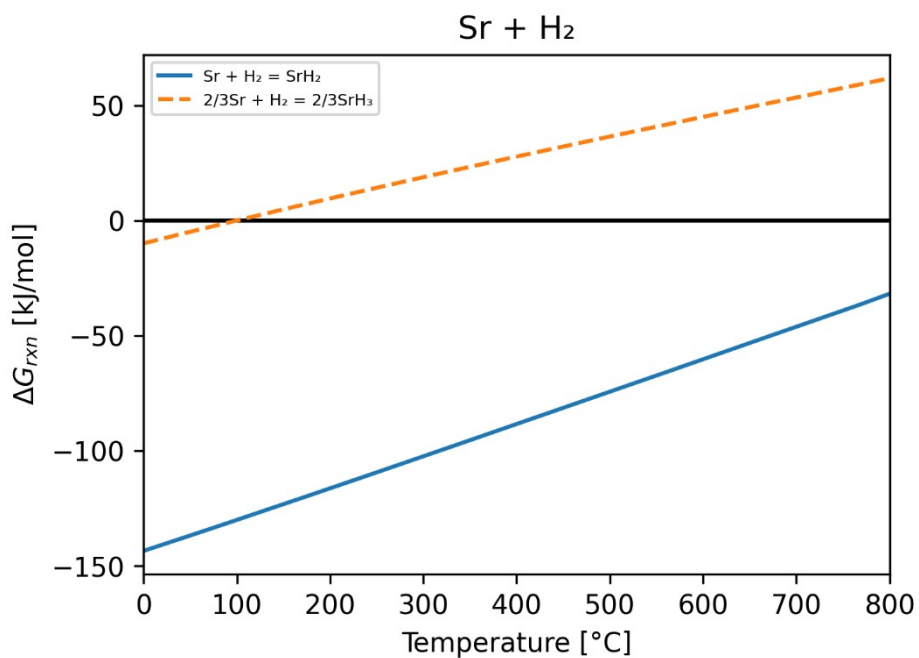


Figure S113: Ellingham diagram of the Sr hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

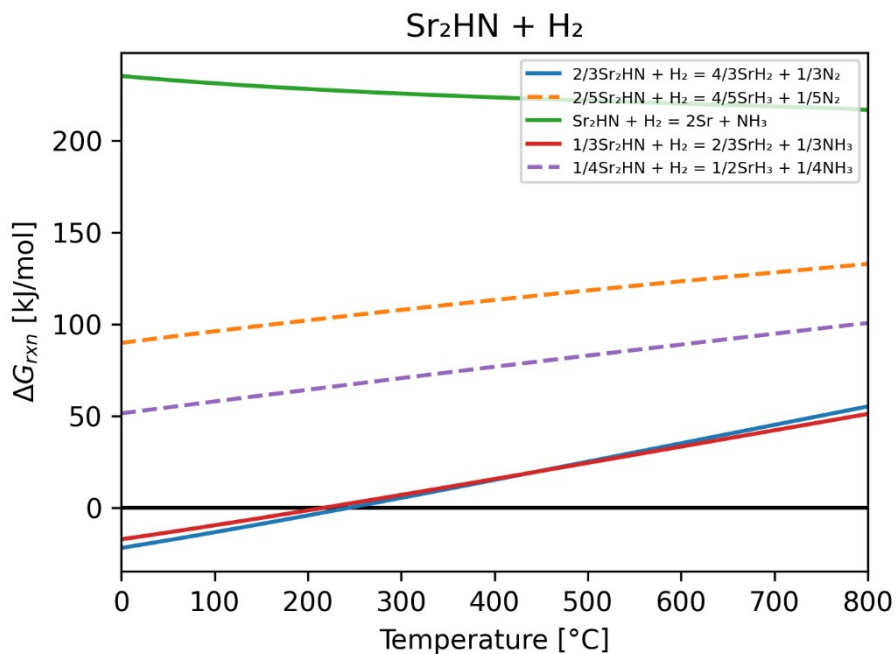


Figure S114: Ellingham diagram of the Sr<sub>2</sub>HN hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

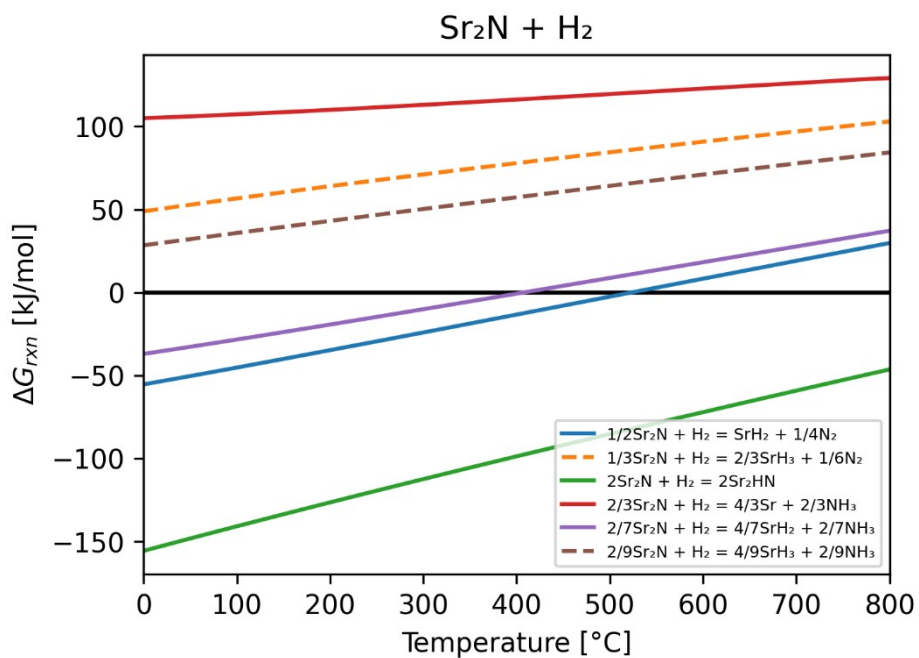


Figure S115: Ellingham diagram of the Sr<sub>2</sub>N hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.



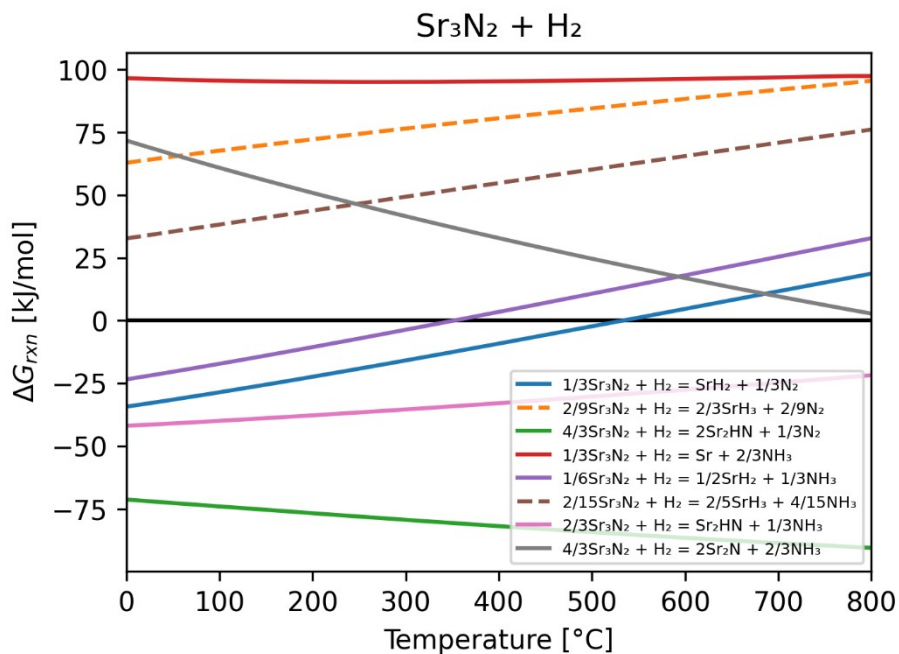


Figure S116: Ellingham diagram of the  $\text{Sr}_3\text{N}_2$  hydrogenation step: standard Gibbs free energy change per mol  $\text{H}_2$  as a function of temperature.

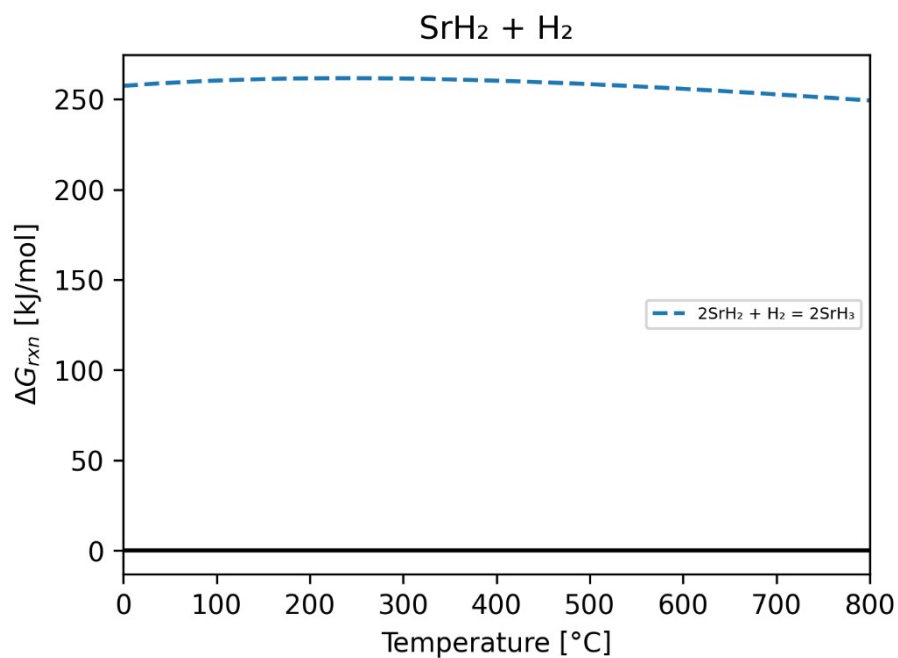


Figure S117: Ellingham diagram of the  $\text{SrH}_2$  hydrogenation step: standard Gibbs free energy change per mol  $\text{H}_2$  as a function of temperature.

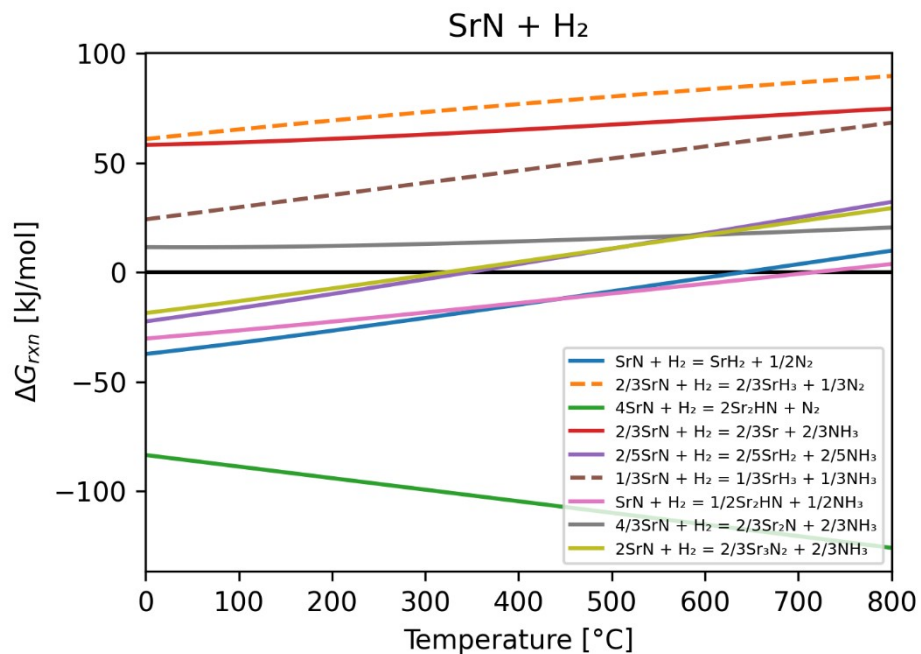


Figure S118: Ellingham diagram of the SrN hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

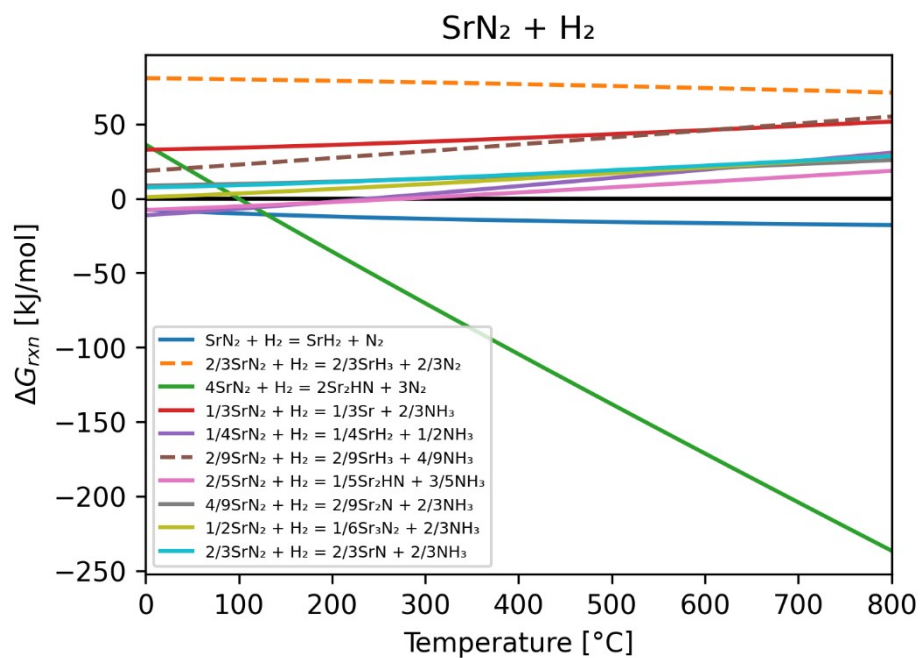


Figure S119: Ellingham diagram of the SrN<sub>2</sub> hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

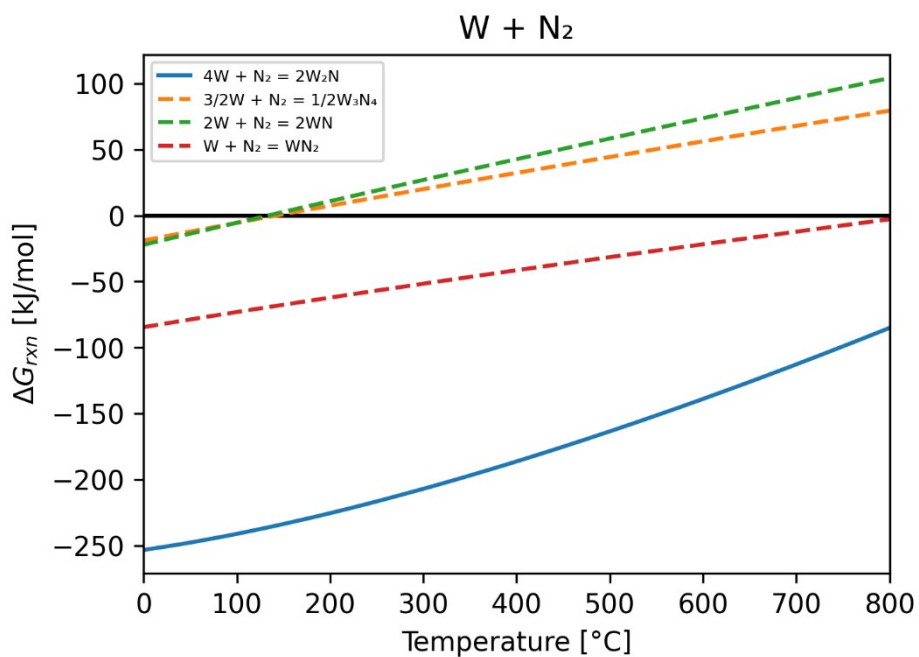


Figure S120: Ellingham diagram of the W nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

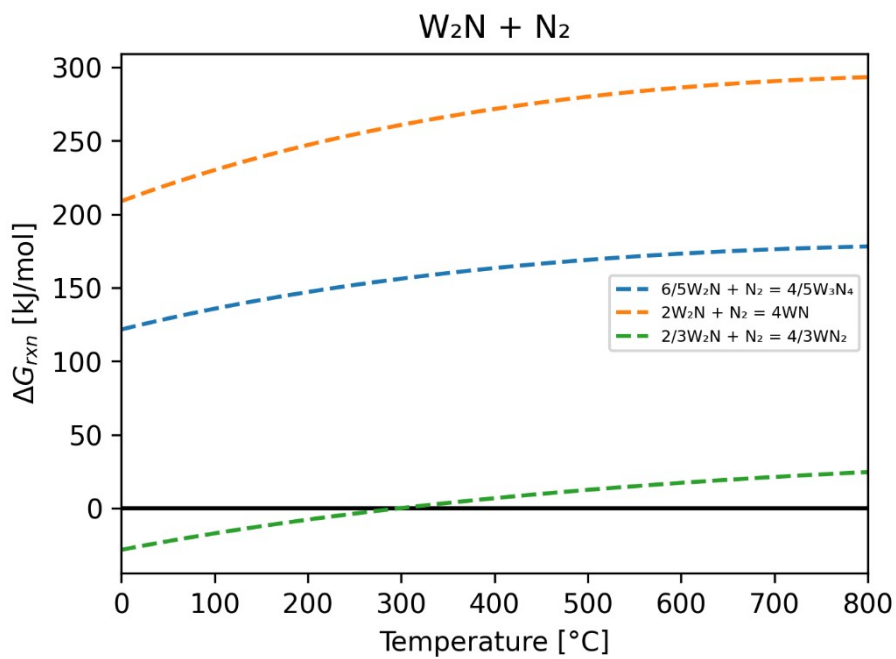


Figure S121: Ellingham diagram of the W<sub>2</sub>N nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

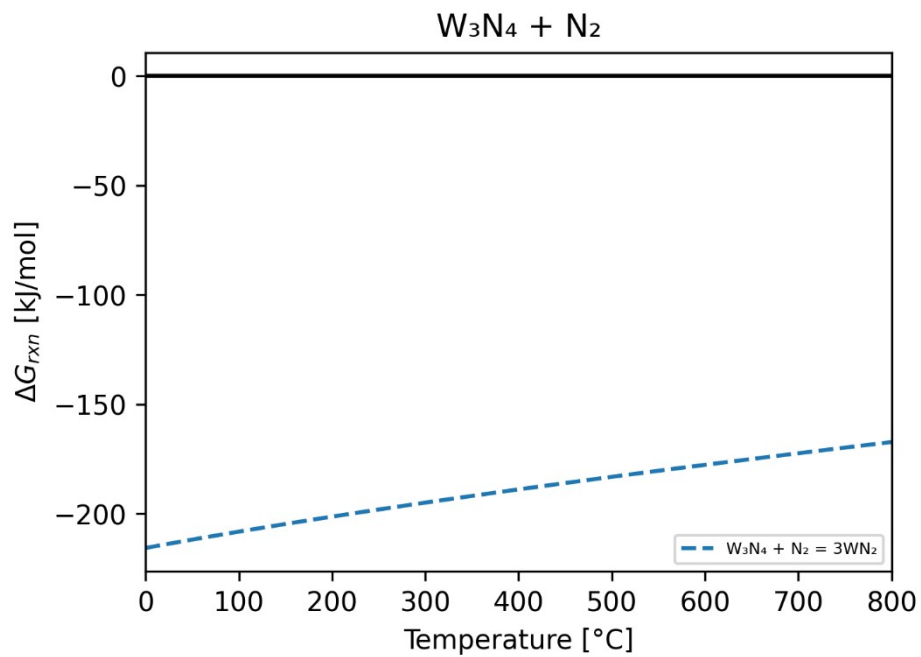


Figure S122: Ellingham diagram of the  $W_3N_4$  nitridation step: standard Gibbs free energy change per mol  $N_2$  as a function of temperature.

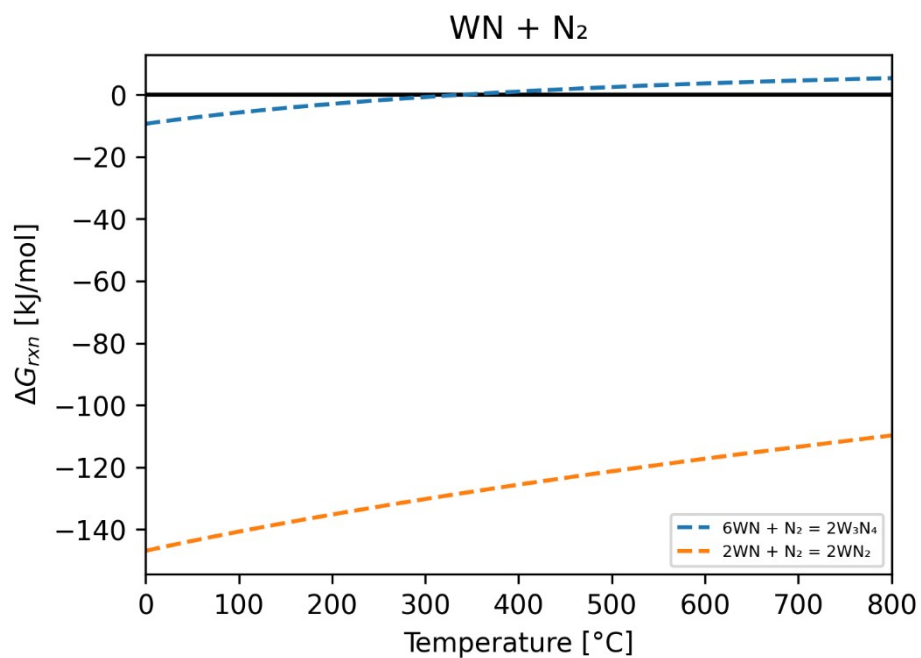


Figure S123: Ellingham diagram of the  $WN$  nitridation step: standard Gibbs free energy change per mol  $N_2$  as a function of temperature.

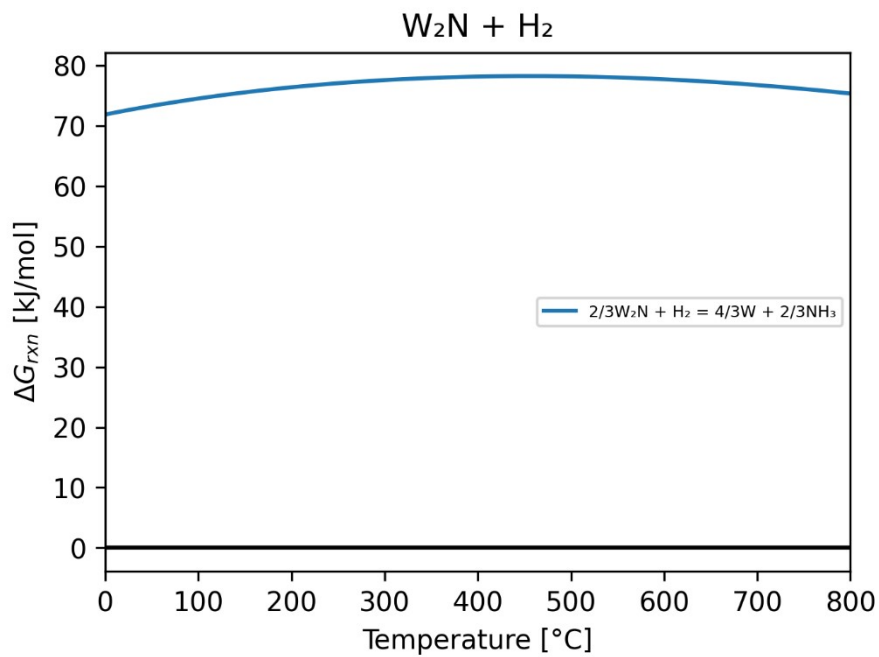


Figure S124: Ellingham diagram of the  $W_2N$  hydrogenation step: standard Gibbs free energy change per mol  $H_2$  as a function of temperature.

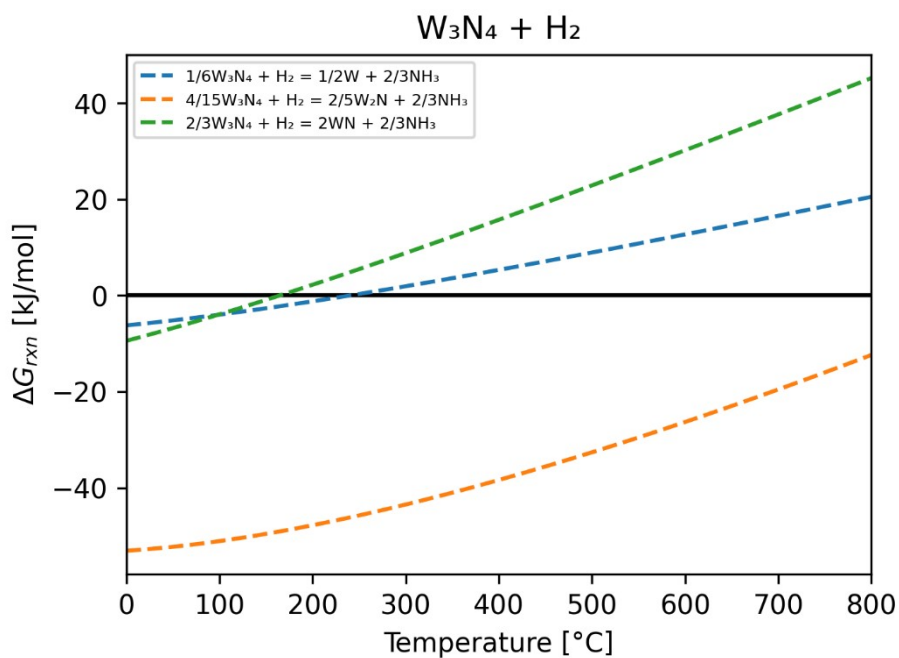


Figure S125: Ellingham diagram of the  $W_3N_4$  hydrogenation step: standard Gibbs free energy change per mol  $H_2$  as a function of temperature.

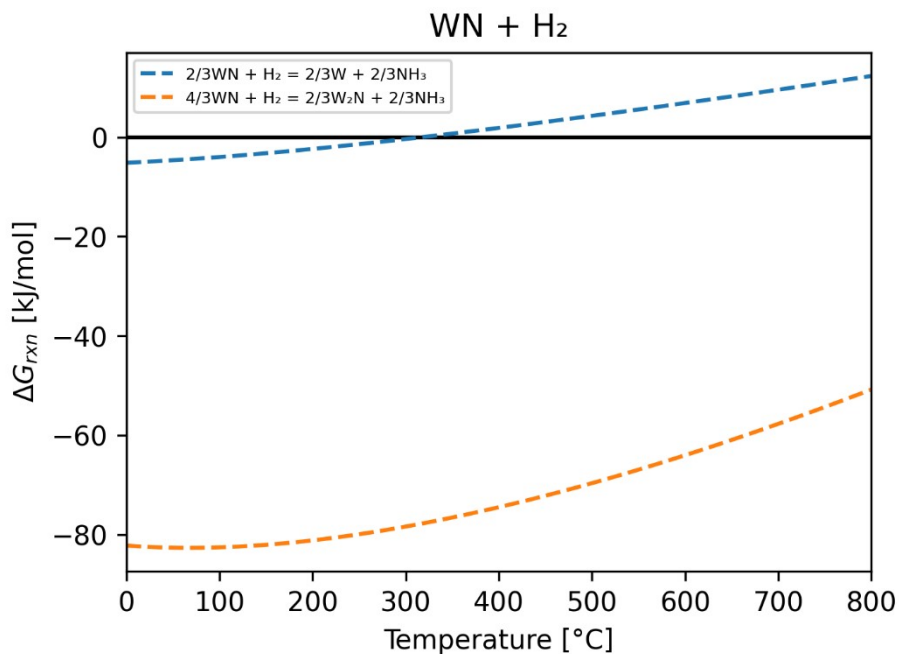


Figure S126: Ellingham diagram of the WN hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

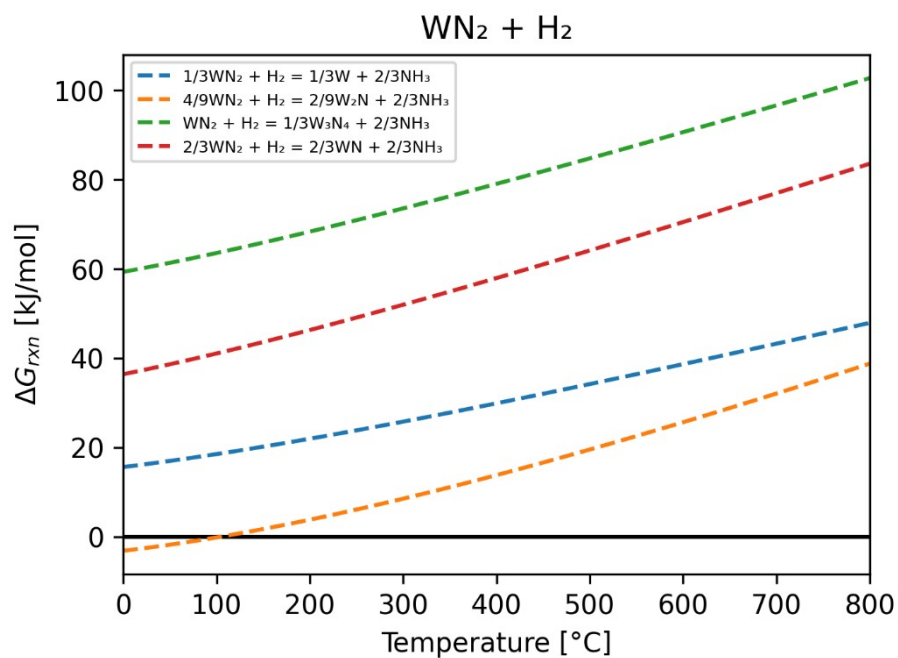


Figure S127: Ellingham diagram of the WN<sub>2</sub> hydrogenation step: standard Gibbs free energy change per mol H<sub>2</sub> as a function of temperature.

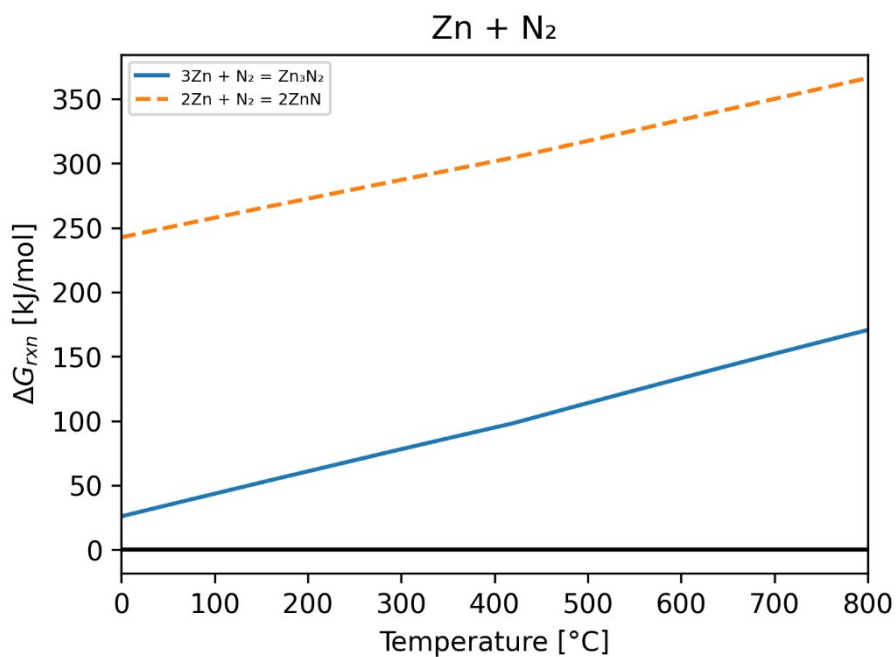


Figure S128: Ellingham diagram of the Zn nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

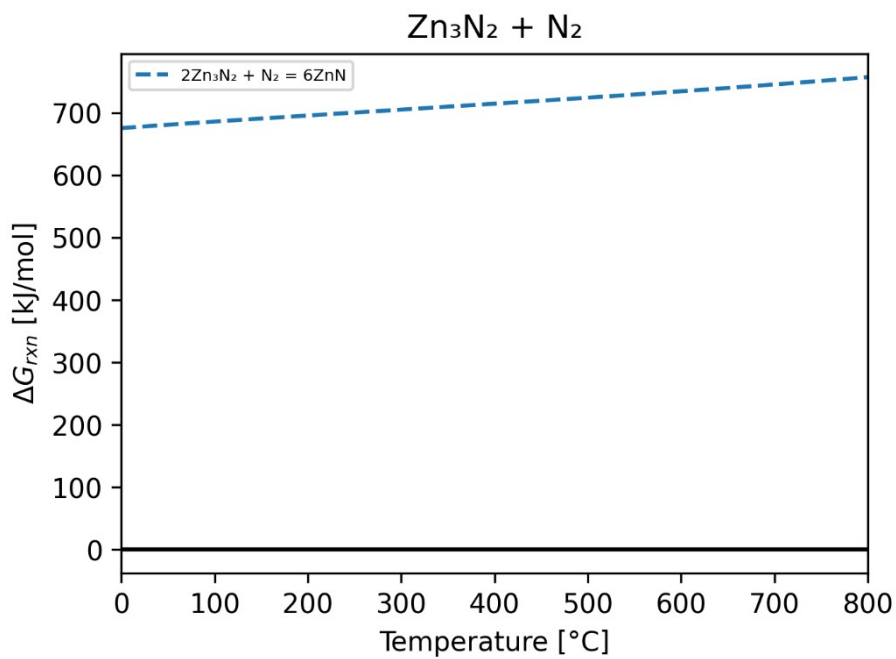


Figure S129: Ellingham diagram of the Zn<sub>3</sub>N<sub>2</sub> nitridation step: standard Gibbs free energy change per mol N<sub>2</sub> as a function of temperature.

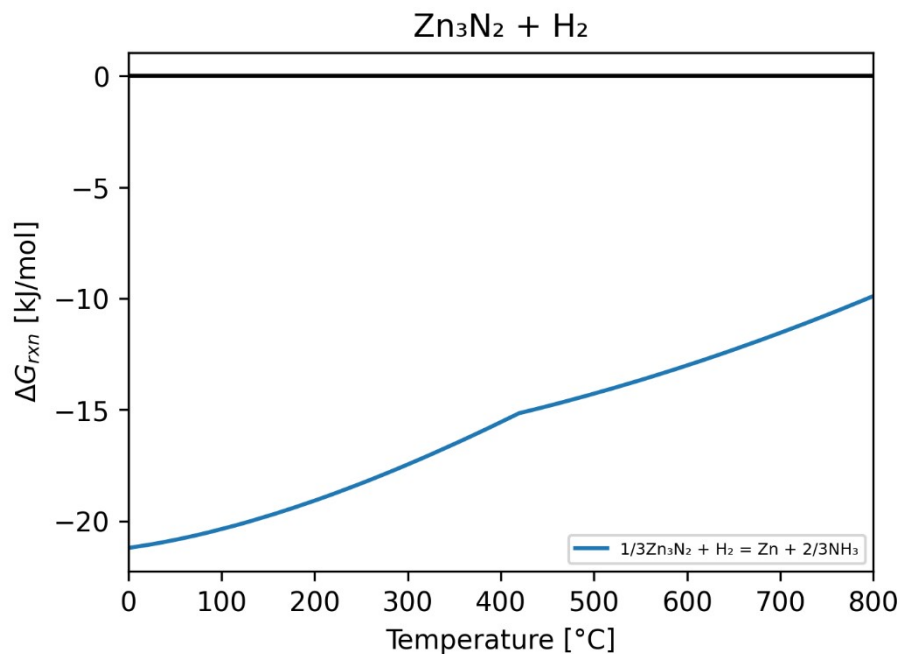


Figure S130: Ellingham diagram of the  $\text{Zn}_3\text{N}_2$  hydrogenation step: standard Gibbs free energy change per mol  $\text{H}_2$  as a function of temperature.

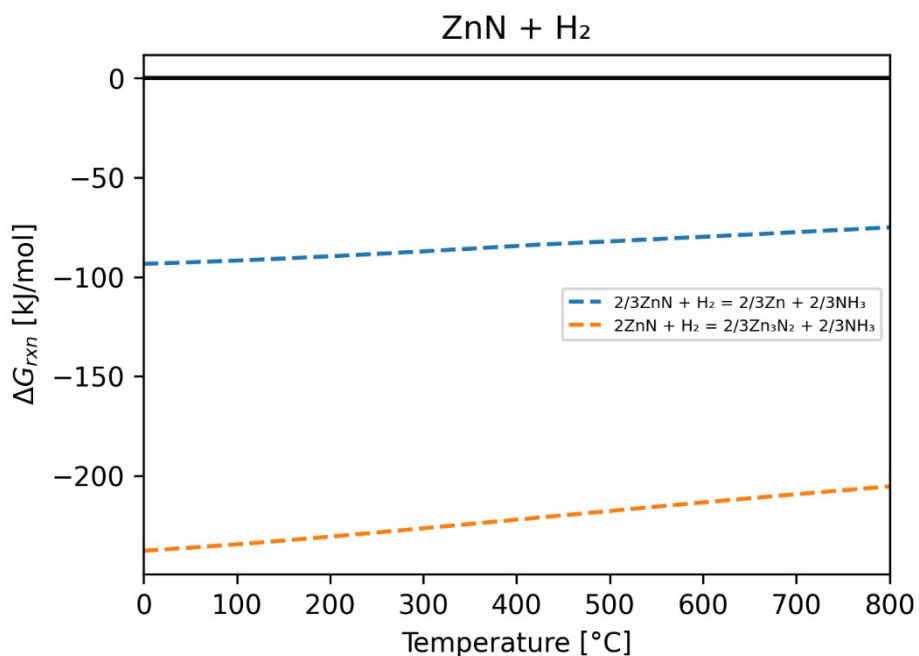


Figure S131: Ellingham diagram of the  $\text{ZnN}$  hydrogenation step: standard Gibbs free energy change per mol  $\text{H}_2$  as a function of temperature.

## 2. Experimental Screening

Experimental screening was performed by thermogravimetric runs. The plots show the variation of mass and temperature (recorded by the TGA), ion current (recorded by the mass spectrometer), and were applicable the  $\text{NH}_3$  concentration (recorded by the  $\text{NH}_3$  analyzer) as a function of time. The materials used in the experiments are shown in Table S29.



Table S29: List of materials used in TGA experiments.

Material	Form	Size	Purity [%]	Supplier
Sr	Random pieces	Flakes in mm-range size	99	Sigma-Aldrich (Merck)
Sr	Granules	mm-range size	99	Sigma-Aldrich (Merck)
Mn	Powder	-325 mesh	99.3	Alfa Aesar
Ca	Granules	-16 mesh	99.5	Alfa Aesar
Cr	Powder	APS <10 micron	99.2	Alfa Aesar
Cu	Powder	-625 mesh	99	Alfa Aesar
W	Powder	APS 1-5 micron	99.9	Alfa Aesar
Ni	Powder	APS 3-7 micron	99.9	Alfa Aesar
Mo	Powder	APS 2-4 micron	99.9	Alfa Aesar
Fe	Powder	APS <10 micron	99.9+	Alfa Aesar
Zn	Powder	Average 4-7 micron	97.5	Alfa Aesar
Co	Powder	APS 1.6 micron	99.8	Alfa Aesar
Al	Powder	APS 3 micron	99.9	Nanografi Nano Technology
Li	Granules	4-10 mesh	99	Sigma-Aldrich (Merck)

*The Al-based system*

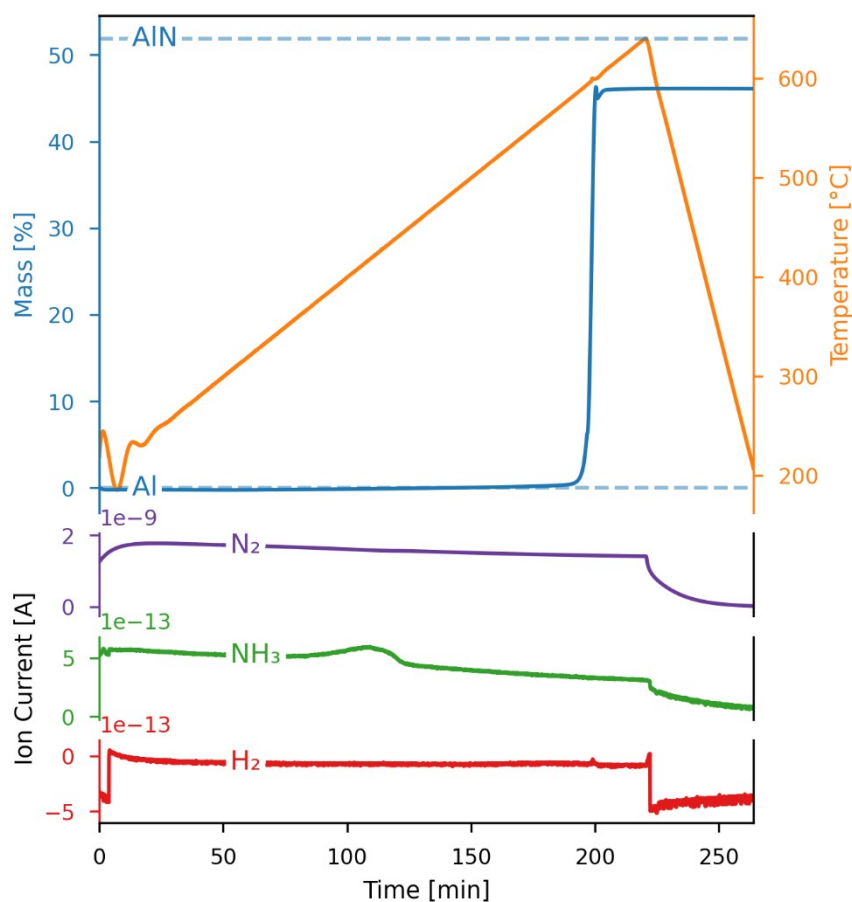


Figure S132: Variations of mass and temperature (recorded by the TGA) and ion current (recorded by the mass spectrometer) as a function of time for the Al-nitridation under 100% N<sub>2</sub>. Blue dashed lines: theoretical mass changes for no conversion (0%) and full conversion to AlN (51.91%). The ion current signals correspond to N<sub>2</sub> (purple), NH<sub>3</sub> (green), and H<sub>2</sub> (red). Sample was heated from 200-640°C at a rate of 2°C/min in 100% N<sub>2</sub> and cooled down back to 200°C in 100% Ar. Al reacted to AlN, in agreement with the Ellingham diagram (

Table S1).

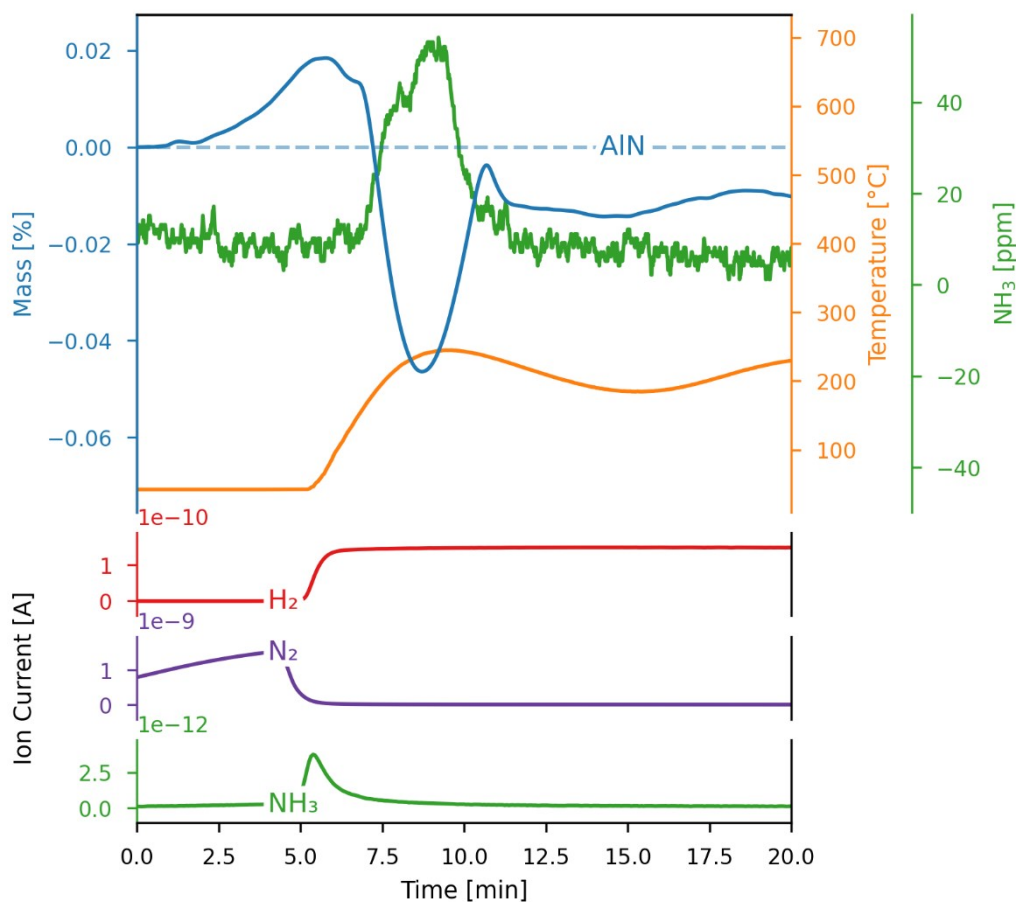


Figure S133: Variations of mass and temperature (recorded by the TGA), ion current (recorded by the mass spectrometer), and  $\text{NH}_3$  concentration (recorded by the  $\text{NH}_3$  analyzer) as a function of time for the AlN-hydrogenation under 5%  $\text{H}_2$  in Ar. Blue dashed line: theoretical mass changes for no conversion (0%). The ion current signals correspond to  $\text{N}_2$  (purple),  $\text{NH}_3$  (green), and  $\text{H}_2$  (red). Sample was heated from 200-700°C at a rate of 2°C/min in 5%  $\text{H}_2$  in Ar (shown is a cropped version of the run to focus on the part with  $\text{NH}_3$  production). Upon switching from a 100%  $\text{N}_2$  flow to the 5%  $\text{H}_2$  flow at around 10 minutes, the  $\text{NH}_3$  analyzer registers a peak of  $\text{NH}_3$  (approximately 40 ppm in the unfiltered signal).

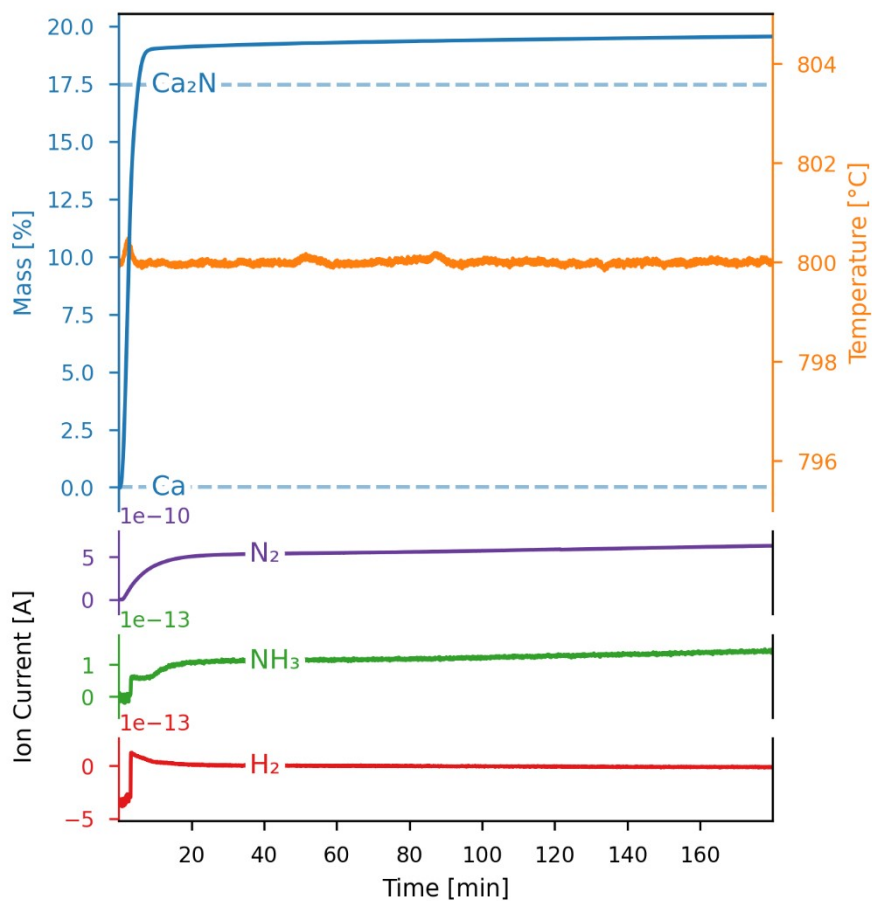


Figure S134: Variations of mass and temperature (recorded by the TGA) and ion current (recorded by the mass spectrometer) as a function of time for the Ca-nitridation under 100% N<sub>2</sub>. Blue dashed lines: theoretical mass changes for no conversion (0%) and full conversion to Ca<sub>2</sub>N (17.47%). The ion current signals correspond to N<sub>2</sub> (purple), NH<sub>3</sub> (green), and H<sub>2</sub> (red). Sample was heated to 800°C in Ar, then switched to 100% N<sub>2</sub>. Ca reacted to Ca<sub>2</sub>N, in agreement with the Ellingham diagram (Figure S6).

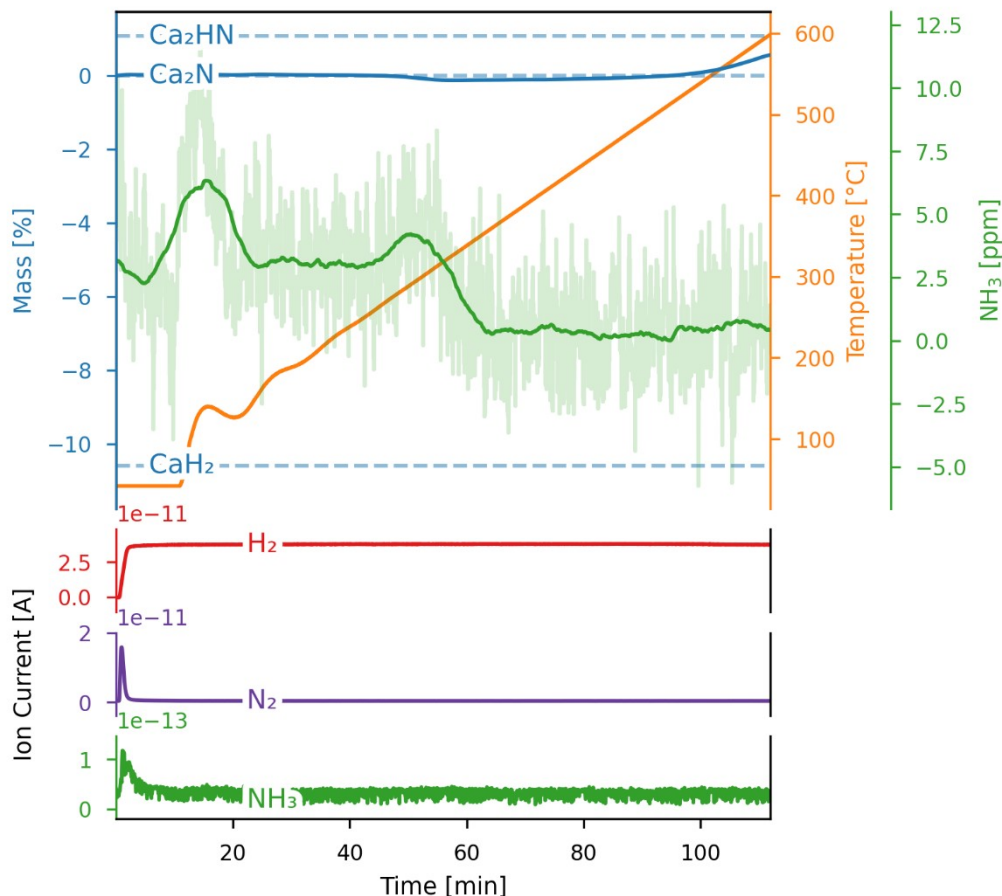


Figure S135: Variations of mass and temperature (recorded by the TGA), ion current (recorded by the mass spectrometer), and  $\text{NH}_3$  concentration (recorded by the  $\text{NH}_3$  analyzer) as a function of time for the  $\text{Ca}_2\text{N}$ -hydrogenation under 5%  $\text{H}_2$  in Ar. Blue dashed line: theoretical mass changes for no conversion (0%), full conversion to  $\text{CaH}_2$  (-10.59%), and full conversion to  $\text{Ca}_2\text{HN}$  (1.67%). The ion current signals correspond to  $\text{N}_2$  (purple),  $\text{NH}_3$  (green), and  $\text{H}_2$  (red). Two peaks of  $\text{NH}_3$  are visible in the filtered  $\text{NH}_3$  signal, albeit very small (same order magnitude as the noise). The first peak is not accompanied by a change in the mass signal. The second peak, shortly before 300 $^{\circ}\text{C}$ , is accompanied by a minor decrease in mass. According to the Ellingham diagram in Figure S12, the formation of  $\text{CaH}_2$  with either  $\text{N}_2$  or  $\text{NH}_3$  from the hydrogenation of  $\text{Ca}_2\text{N}$  is spontaneous up to approximately that temperature.

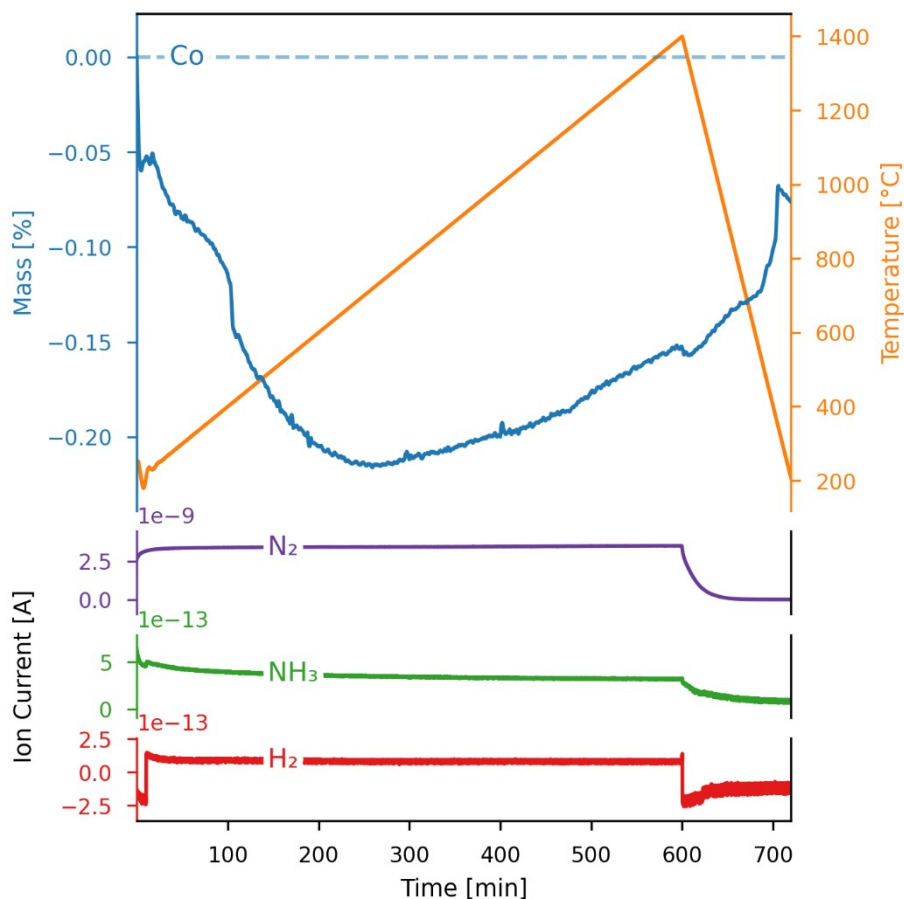


Figure S136: Variations of mass and temperature (recorded by the TGA) and ion current (recorded by the mass spectrometer) as a function of time for the Co-nitridation under 100% N<sub>2</sub>. Blue dashed lines: theoretical mass changes for no conversion (0%). The ion current signals correspond to N<sub>2</sub> (purple), NH<sub>3</sub> (green), and H<sub>2</sub> (red). Sample was heated from 200-1400°C at a rate of 2°C/min in 100% N<sub>2</sub> and cooled down back to 200°C in 100% Ar. No significant reaction was measurable, in agreement with the Ellingham diagram (Figure S16).

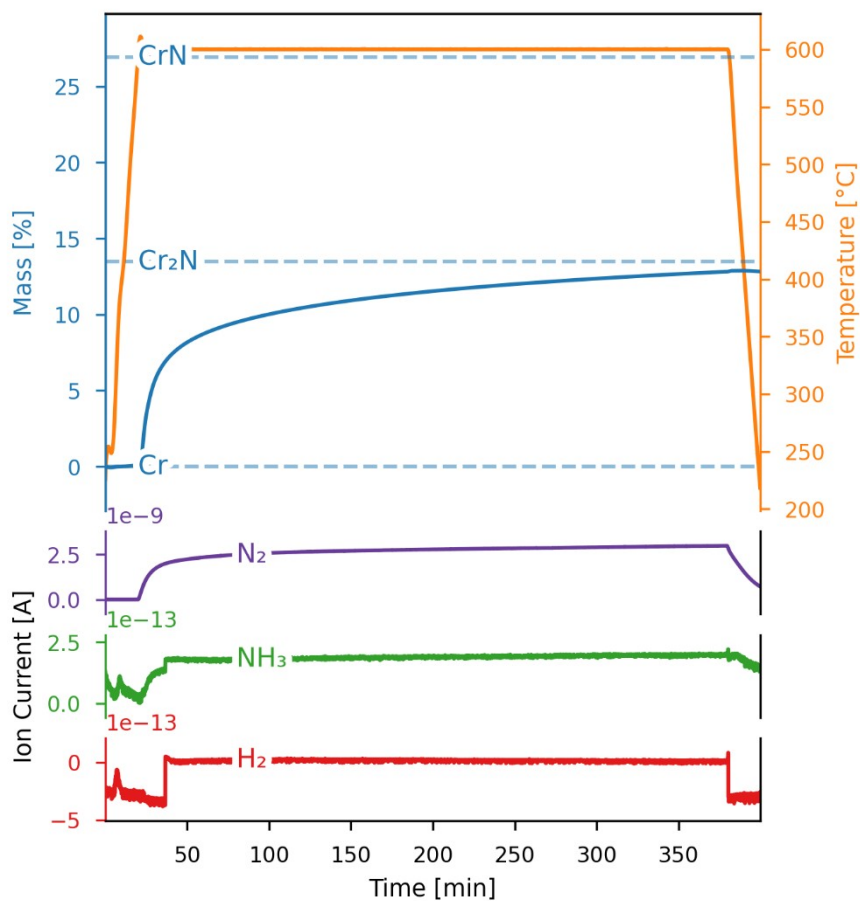


Figure S137: Variations of mass and temperature (recorded by the TGA) and ion current (recorded by the mass spectrometer) as a function of time for the Cr-nitridation under 100% N<sub>2</sub>. Blue dashed lines: theoretical mass changes for no conversion (0%), full conversion to Cr<sub>2</sub>N (13.47%), and full conversion to CrN (26.94%). The ion current signals correspond to N<sub>2</sub> (purple), NH<sub>3</sub> (green), and H<sub>2</sub> (red). Sample was heated to 600°C in Ar, then switch to 100% N<sub>2</sub>. Cr reacted to Cr<sub>2</sub>N, in agreement with the Ellingham diagram (Figure S24).

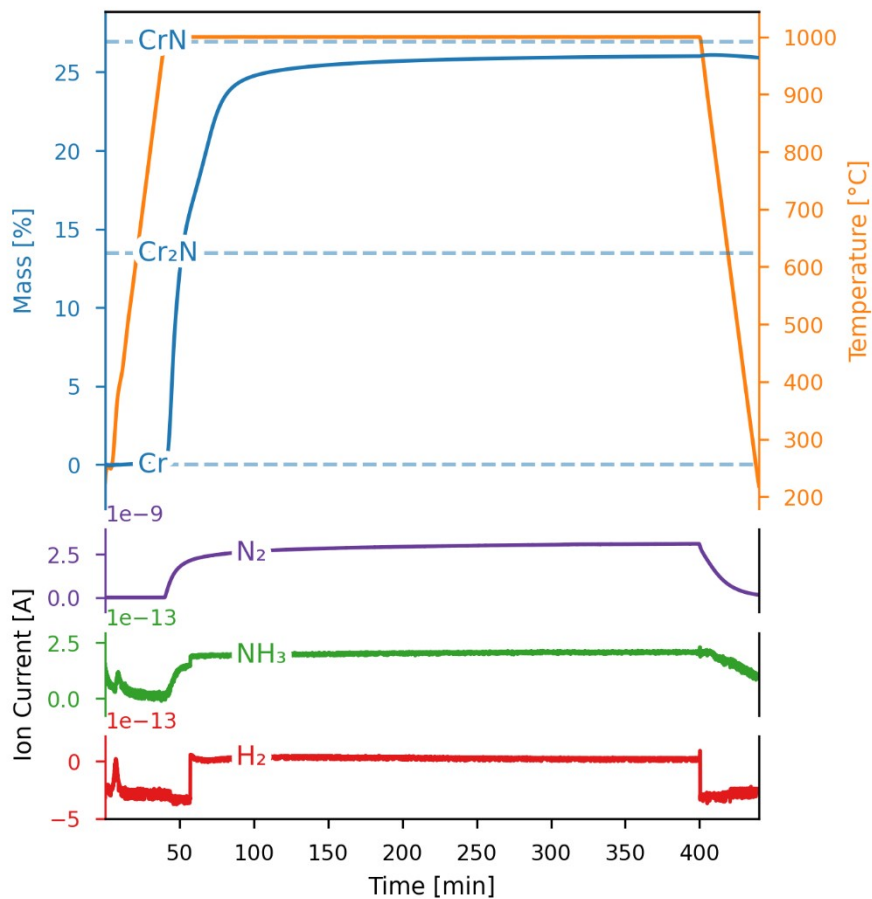


Figure S138: Variations of mass and temperature (recorded by the TGA) and ion current (recorded by the mass spectrometer) as a function of time for the Cr-nitridation under 100% N<sub>2</sub>. Blue dashed lines: theoretical mass changes for no conversion (0%), full conversion to Cr<sub>2</sub>N (13.47%), and full conversion to CrN (26.94%). The ion current signals correspond to N<sub>2</sub> (purple), NH<sub>3</sub> (green), and H<sub>2</sub> (red). Sample was heated to 600°C in Ar, then switch to 100% N<sub>2</sub>. Cr reacted to CrN. According to the Ellingham diagram (Figure S24), the formation of Cr<sub>2</sub>N should be more favourable in this temperature range.

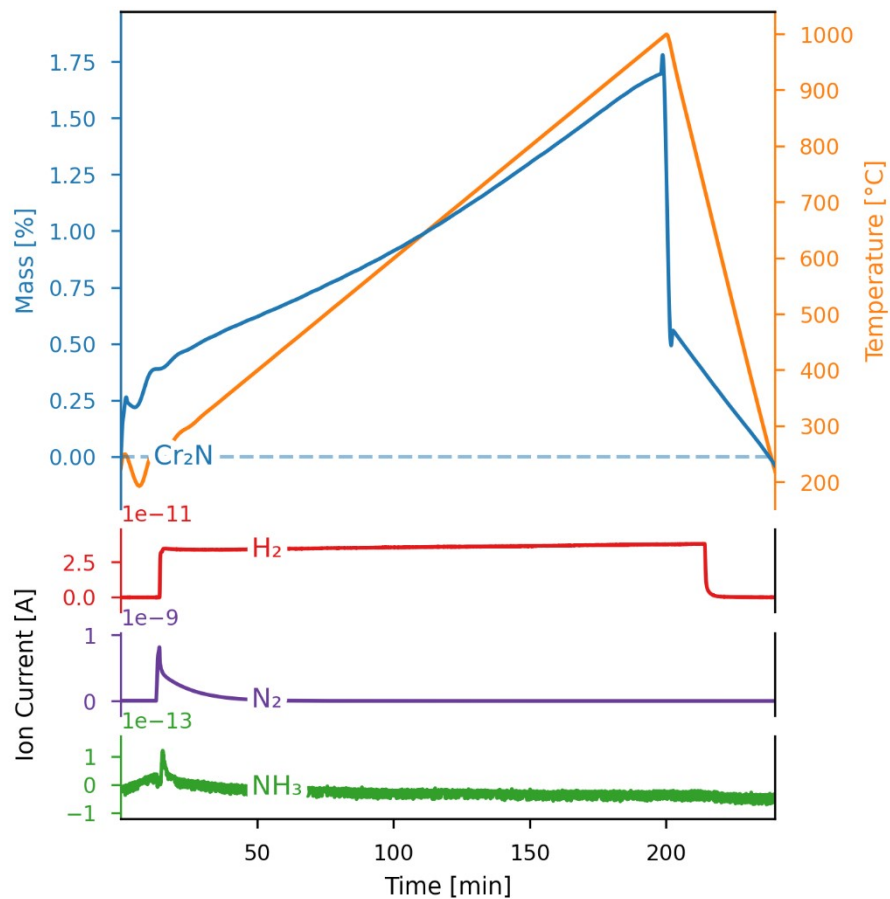


Figure 139: Variations of mass and temperature (recorded by the TGA) and ion current (recorded by the mass spectrometer) as a function of time for the  $\text{Cr}_2\text{N}$ -hydrogenation under 5%  $\text{H}_2$  in Ar. Blue dashed lines: theoretical mass changes for no conversion (0%). The ion current signals correspond to  $\text{N}_2$  (purple),  $\text{NH}_3$  (green), and  $\text{H}_2$  (red). Sample was heated from 200-1000°C at a rate of 4°C/min in 5%  $\text{H}_2$  in Ar and cooled down back to 200°C in 100% Ar. No significant reaction was measurable, in agreement with the Ellingham diagram (Figure S31).



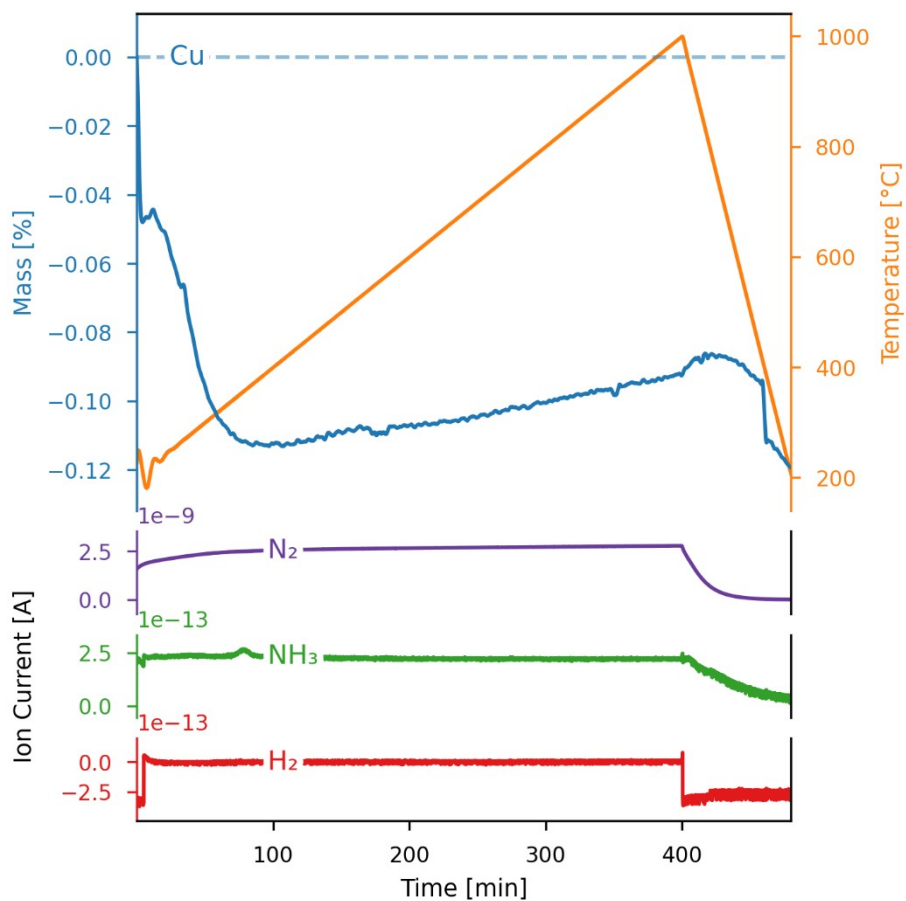


Figure S140: Variations of mass and temperature (recorded by the TGA) and ion current (recorded by the mass spectrometer) as a function of time for the Cu-nitridation under 100% N<sub>2</sub>. Blue dashed lines: theoretical mass changes for no conversion (0%). The ion current signals correspond to N<sub>2</sub> (purple), NH<sub>3</sub> (green), and H<sub>2</sub> (red). Sample was heated from 200-1000°C at a rate of 2°C/min in 100% N<sub>2</sub> and cooled down back to 200°C in 100% Ar. No significant reaction was measurable, in agreement with the Ellingham diagram (Figure S36).

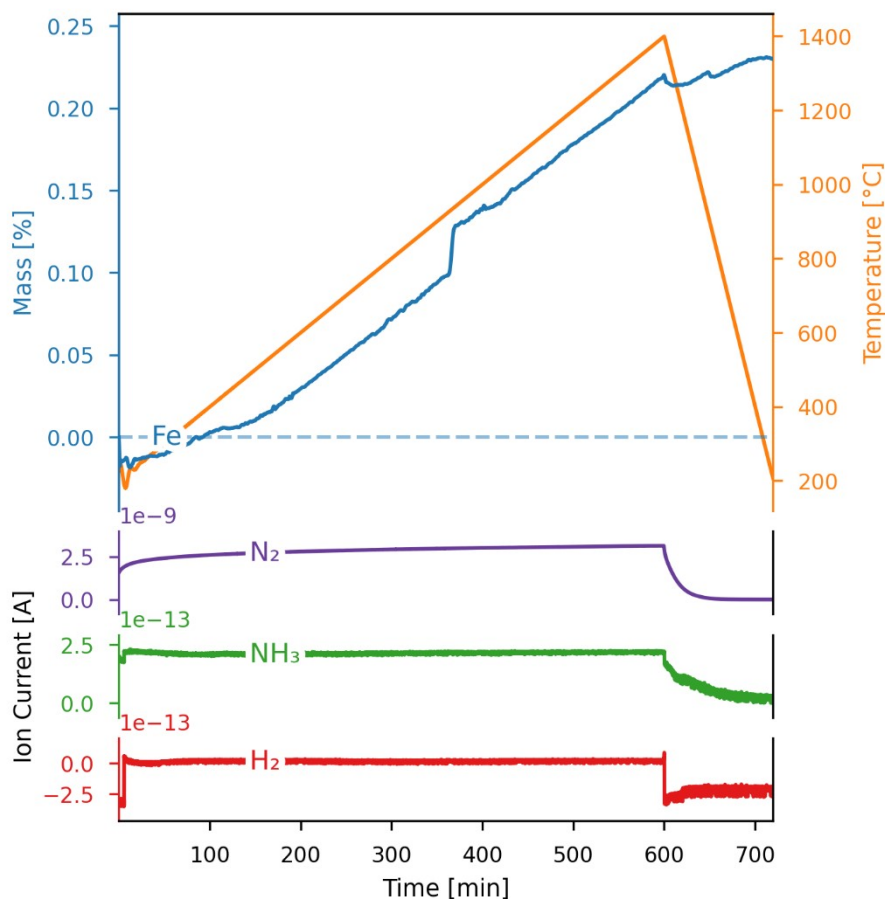


Figure S141: Variations of mass and temperature (recorded by the TGA) and ion current (recorded by the mass spectrometer) as a function of time for the Fe-nitridation under 100% N<sub>2</sub>. Blue dashed lines: theoretical mass changes for no conversion (0%). The ion current signals correspond to N<sub>2</sub> (purple), NH<sub>3</sub> (green), and H<sub>2</sub> (red). Sample was heated from 200-1400°C at a rate of 2°C/min in 100% N<sub>2</sub> and cooled down back to 200°C in 100% Ar. No significant reaction was measurable. According to the Ellingham diagram (Figure S46), the formation of Fe<sub>3</sub>N and FeN should be favourable up to 220°C and 450°C, respectively.

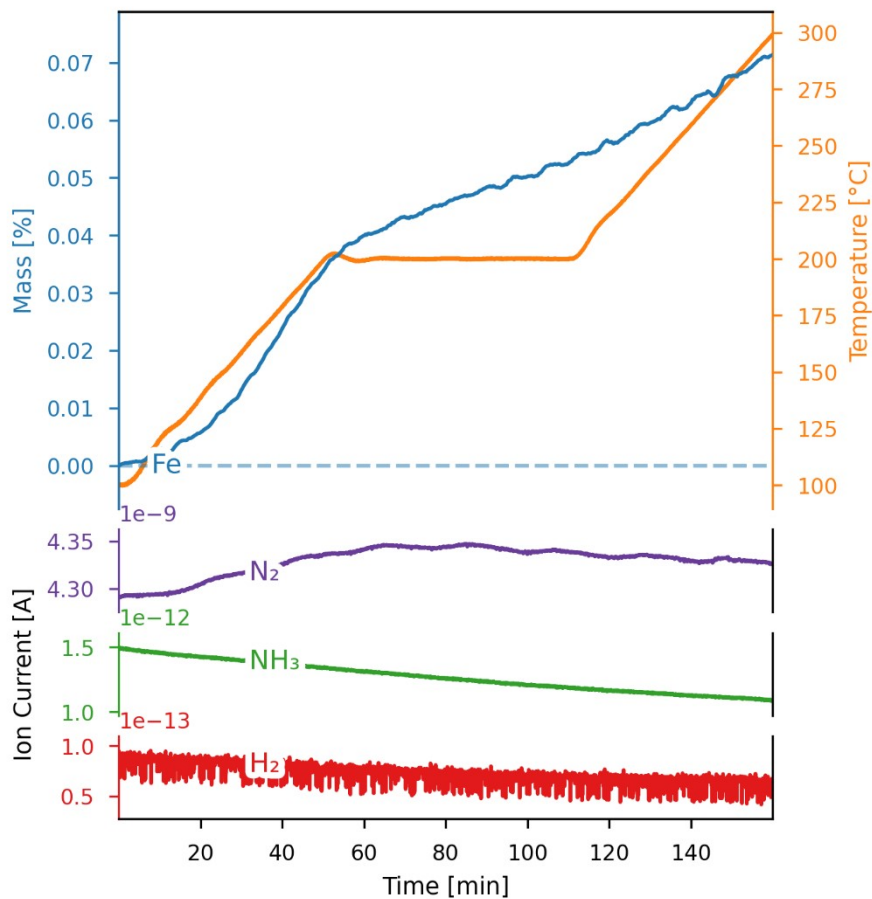


Figure S142: Variations of mass and temperature (recorded by the TGA) and ion current (recorded by the mass spectrometer) as a function of time for the Fe-nitridation under 100% N<sub>2</sub>. Blue dashed lines: theoretical mass changes for no conversion (0%). The ion current signals correspond to N<sub>2</sub> (purple), NH<sub>3</sub> (green), and H<sub>2</sub> (red). Sample was heated from 100-300°C at a rate of 2°C/min in 100% N<sub>2</sub> with an isothermal section of 60 min at 200°C in between. No significant reaction was measurable. According to the Ellingham diagram (Figure S46), the formation of Fe<sub>3</sub>N and FeN should be favourable up to 220°C and 450°C, respectively.

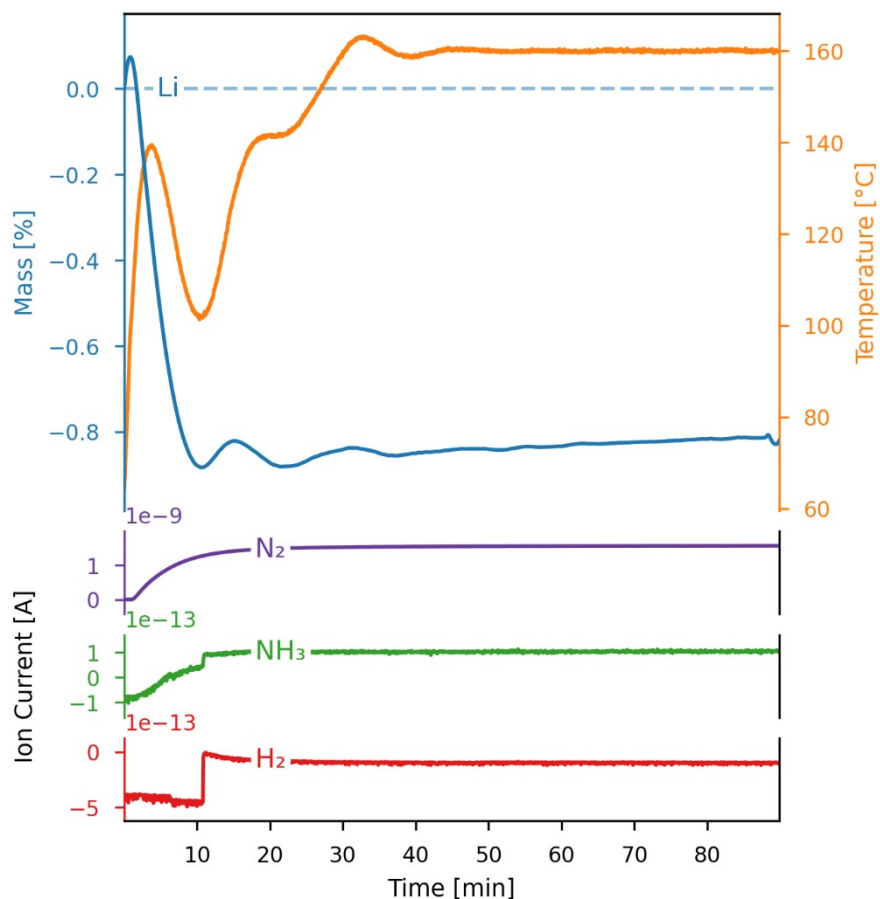


Figure S143: Variations of mass and temperature (recorded by the TGA) and ion current (recorded by the mass spectrometer) as a function of time for the Li-nitridation under 100% N<sub>2</sub>. Blue dashed lines: theoretical mass changes for no conversion (0%). The ion current signals correspond to N<sub>2</sub> (purple), NH<sub>3</sub> (green), and H<sub>2</sub> (red). Sample was heated to 160°C in Ar, then switched to 100% N<sub>2</sub>. No significant reaction was measurable. According to the Ellingham diagram (Figure S62), the formation of Li<sub>3</sub>N should be favourable at that temperature. The low temperature seems to prevent the reaction from proceeding. Due to the Li melting point of 180.5°C at 1 bar, higher temperatures are not feasible.

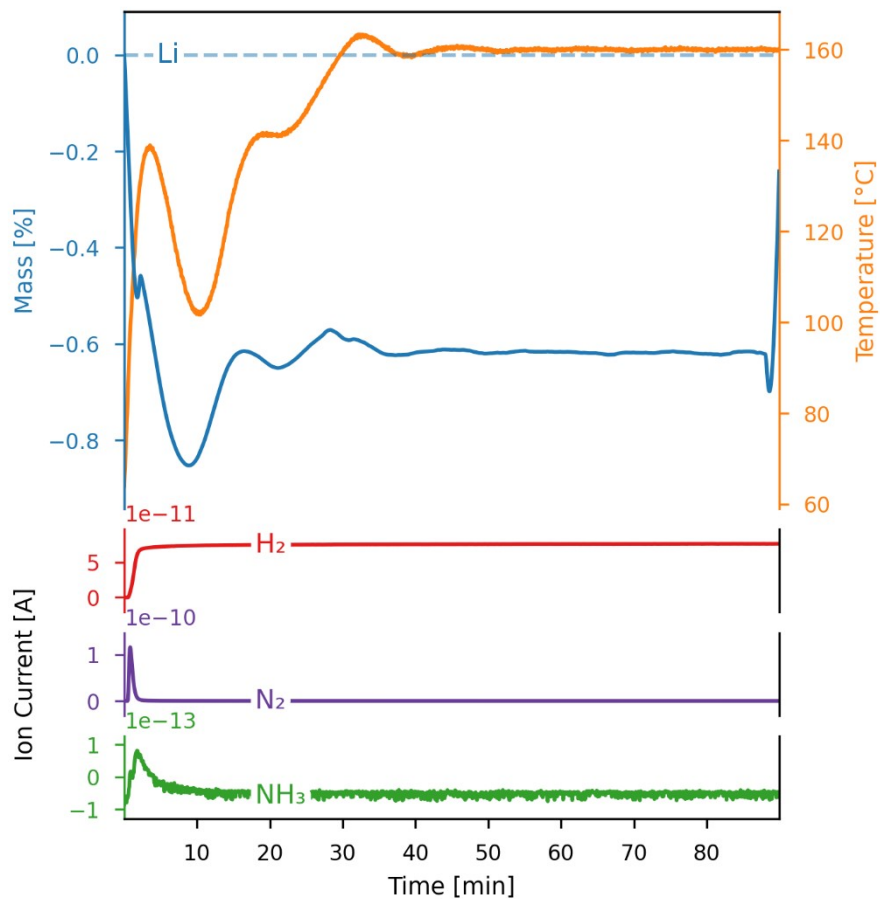


Figure S144: Variations of mass and temperature (recorded by the TGA) and ion current (recorded by the mass spectrometer) as a function of time for the Li-hydrogenation under 5% H<sub>2</sub> in Ar. Blue dashed lines: theoretical mass changes for no conversion (0%). The ion current signals correspond to N<sub>2</sub> (purple), NH<sub>3</sub> (green), and H<sub>2</sub> (red). Sample was heated to 160°C in Ar, then switched to 5% H<sub>2</sub> in Ar. No significant reaction was measurable. According to the Ellingham diagram (Figure S66), the formation of LiH should be favourable at that temperature. The low temperature seems to prevent the reaction from proceeding. Due to the Li melting point of 180.5°C at 1 bar, higher temperatures are not feasible.

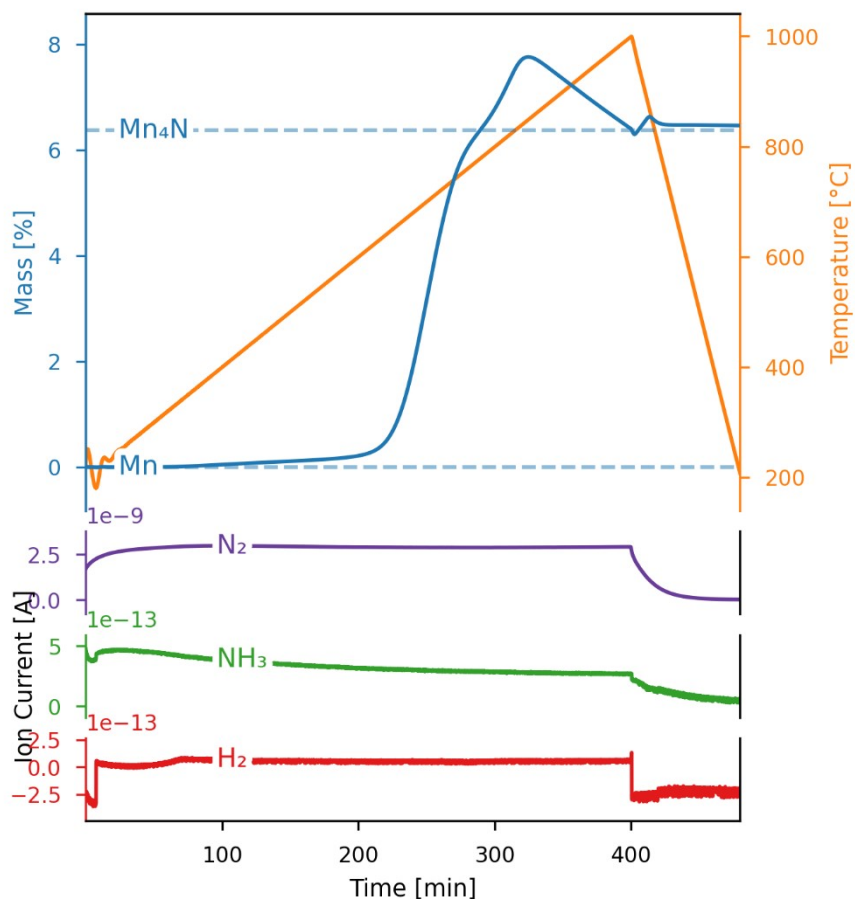


Figure S145: Variations of mass and temperature (recorded by the TGA) and ion current (recorded by the mass spectrometer) as a function of time for the Mn-nitridation under 100% N<sub>2</sub>. Blue dashed lines: theoretical mass changes for no conversion (0%) and full conversion to Mn<sub>4</sub>N (6.37%). The ion current signals correspond to N<sub>2</sub> (purple), NH<sub>3</sub> (green), and H<sub>2</sub> (red). Sample was heated from 200-1000°C at a rate of 2°C/min in 100% N<sub>2</sub> and cooled down back to 200°C in 100% Ar. Mn reacted to Mn<sub>4</sub>N, in agreement with the Ellingham diagram (Figure S70).

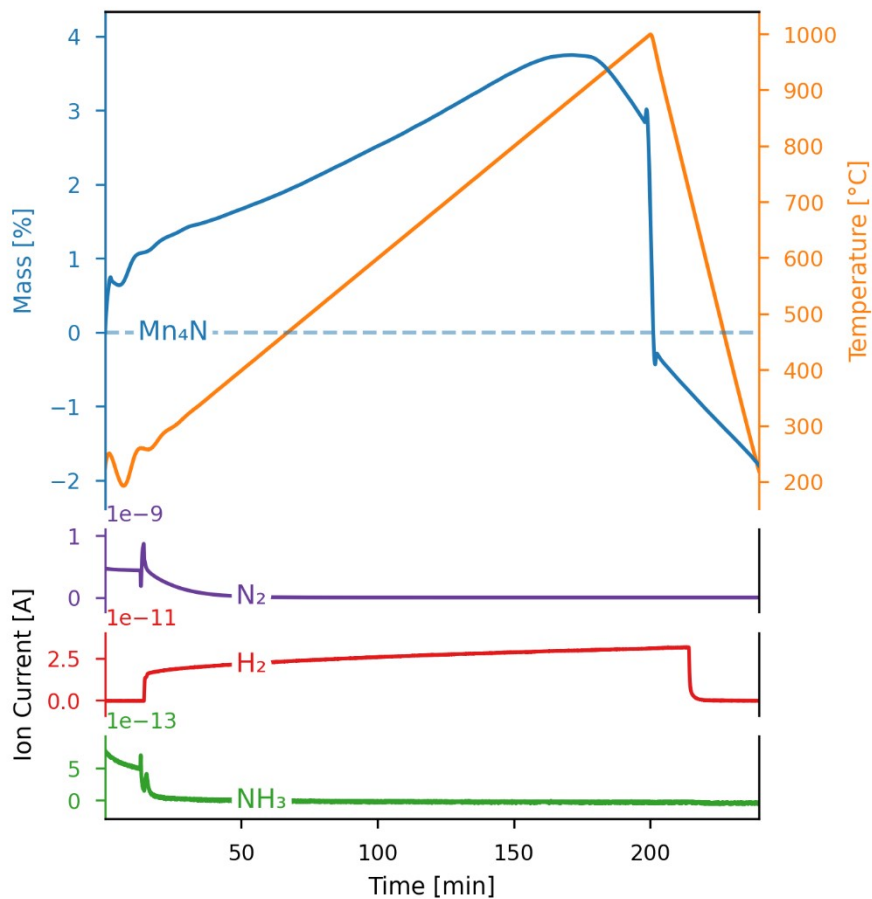


Figure S146: Variations of mass and temperature (recorded by the TGA) and ion current (recorded by the mass spectrometer) as a function of time for the  $\text{Mn}_4\text{N}$ -hydrogenation under 5%  $\text{H}_2$  in Ar. Blue dashed lines: theoretical mass changes for no conversion (0%). The ion current signals correspond to  $\text{N}_2$  (purple),  $\text{NH}_3$  (green), and  $\text{H}_2$  (red). Sample was heated from 200-1000°C at a rate of 4°C/min in 5%  $\text{H}_2$  in Ar and cooled down back to 200°C in 100% Ar. A mass increase was measurable up until 900°C, above that the mass decreases. The Ellingham diagram (Figure S77) and none of the reactions (Table S21) can help explain this behaviour.

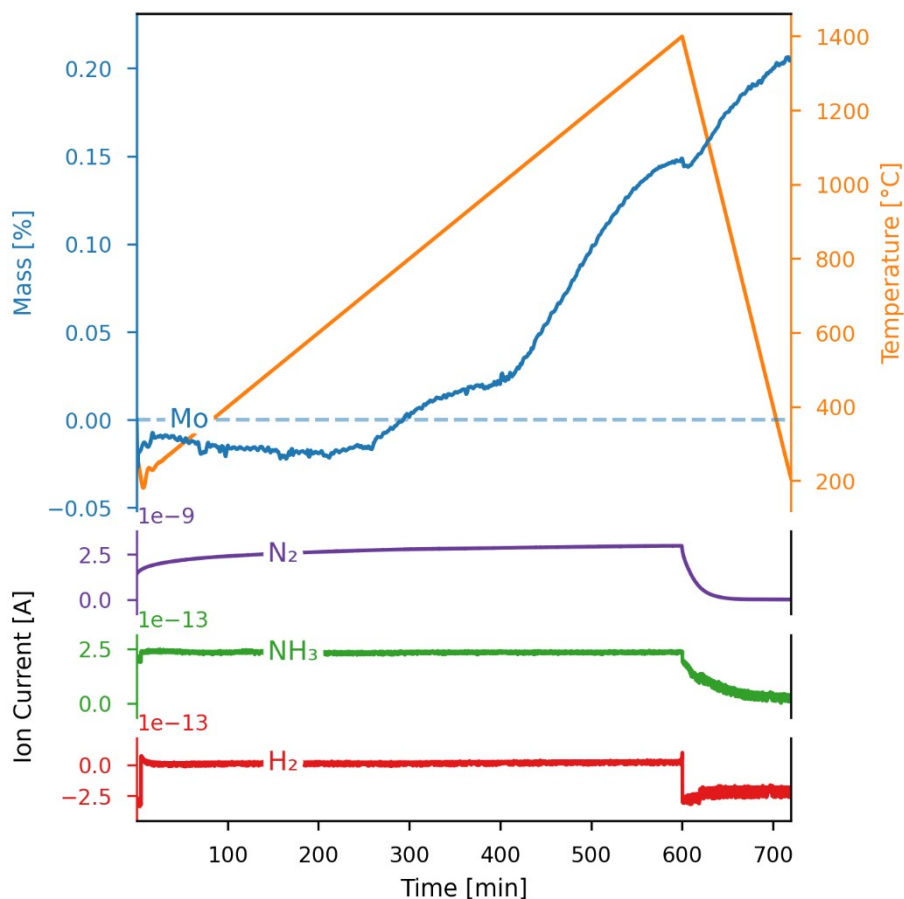


Figure S147: Variations of mass and temperature (recorded by the TGA) and ion current (recorded by the mass spectrometer) as a function of time for the Mo-nitridation under 100% N<sub>2</sub>. Blue dashed lines: theoretical mass changes for no conversion (0%). The ion current signals correspond to N<sub>2</sub> (purple), NH<sub>3</sub> (green), and H<sub>2</sub> (red). Sample was heated from 200-1400°C at a rate of 2°C/min in 100% N<sub>2</sub> and cooled down back to 200°C in 100% Ar. No significant reaction was measurable. According to the Ellingham diagram (Figure S80), the formation of Mo<sub>2</sub>N should be favourable below 680°C.



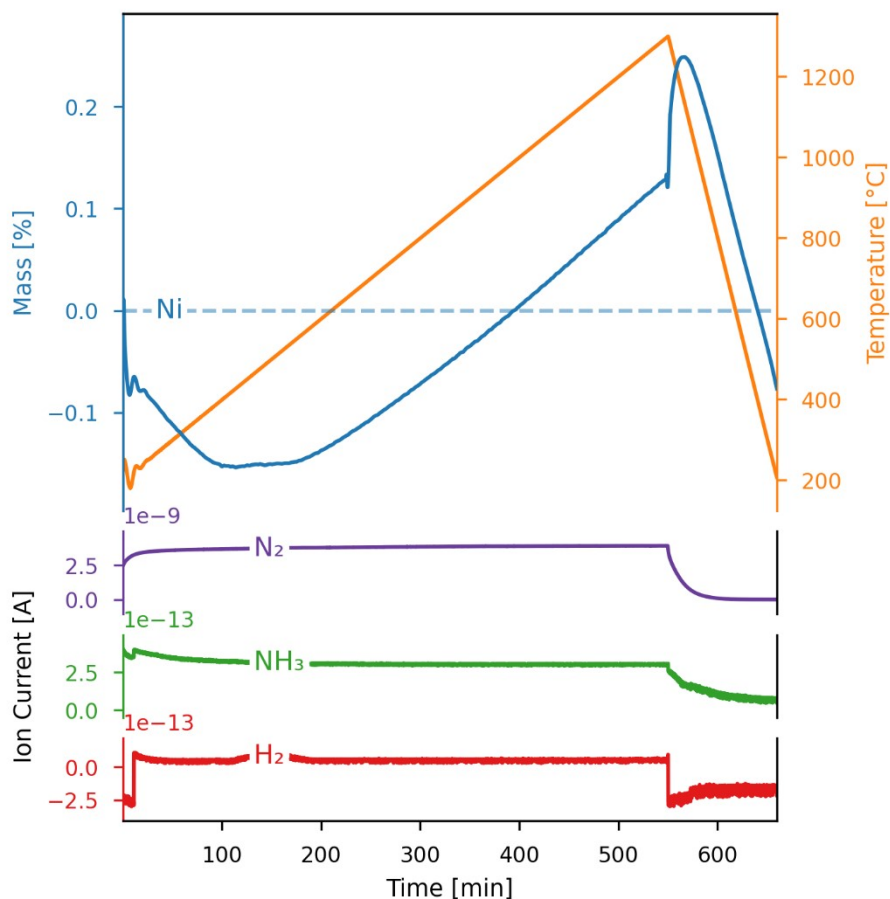


Figure S148: Variations of mass and temperature (recorded by the TGA) and ion current (recorded by the mass spectrometer) as a function of time for the Ni-nitridation under 100% N<sub>2</sub>. Blue dashed lines: theoretical mass changes for no conversion (0%). The ion current signals correspond to N<sub>2</sub> (purple), NH<sub>3</sub> (green), and H<sub>2</sub> (red). Sample was heated from 200-1300°C at a rate of 2°C/min in 100% N<sub>2</sub> and cooled down back to 200°C in 100% Ar. No significant reaction was measurable, in agreement with the Ellingham diagram (Figure S92).

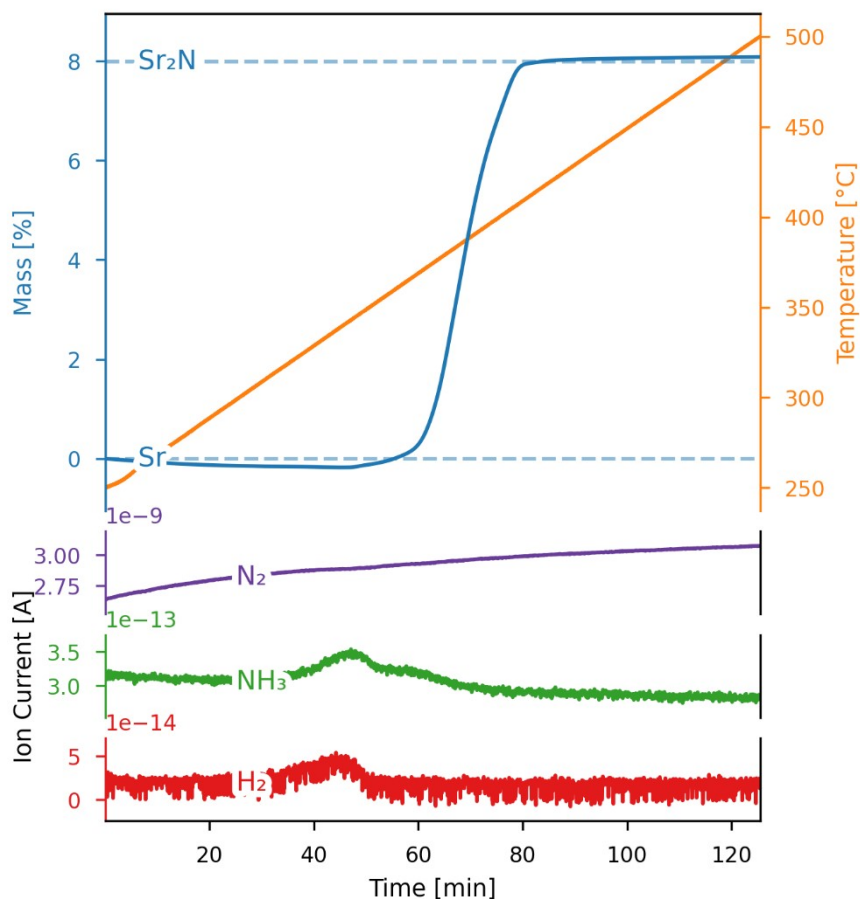


Figure S149: Variations of mass and temperature (recorded by the TGA) and ion current (recorded by the mass spectrometer) as a function of time for the Sr (granules)-nitridation under 100% N<sub>2</sub>. Blue dashed lines: theoretical mass changes for no conversion (0%) and full conversion to Sr<sub>2</sub>N (7.99%). The ion current signals correspond to N<sub>2</sub> (purple), NH<sub>3</sub> (green), and H<sub>2</sub> (red). Sample was heated from 200-500°C at a rate of 2°C/min in 100% N<sub>2</sub>. Sr reacted to Sr<sub>2</sub>N, in agreement with the Ellingham diagram (Figure S106).

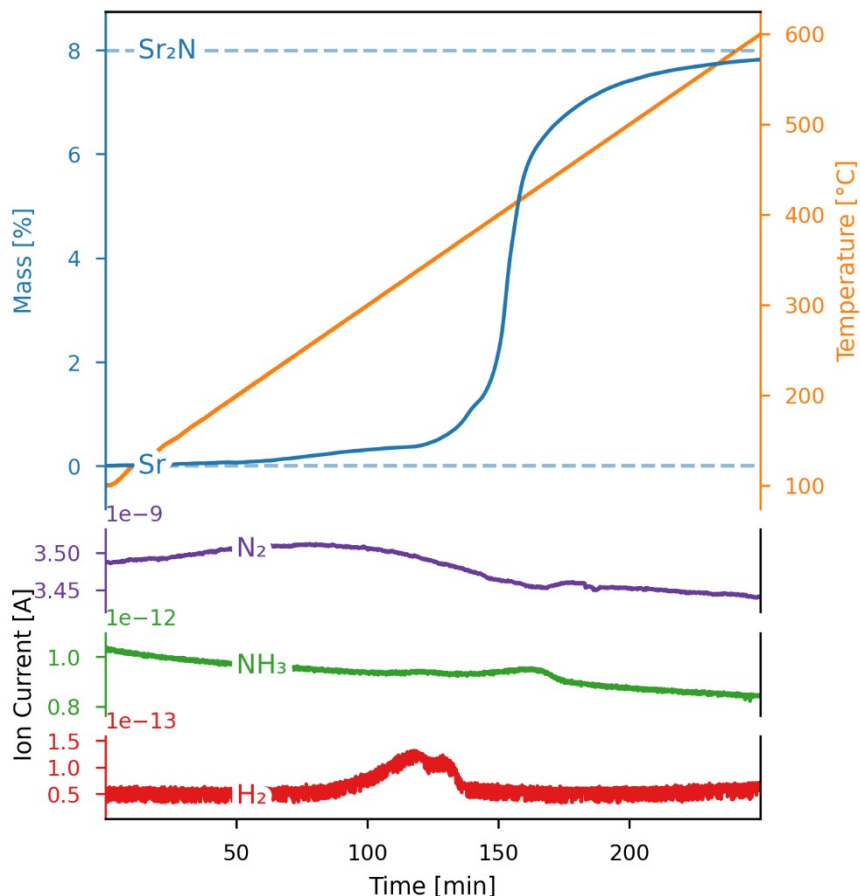


Figure S150: Variations of mass and temperature (recorded by the TGA) and ion current (recorded by the mass spectrometer) as a function of time for the Sr (random pieces)-nitridation under 100% N<sub>2</sub>. Blue dashed lines: theoretical mass changes for no conversion (0%) and full conversion to Sr<sub>2</sub>N (7.99%). The ion current signals correspond to N<sub>2</sub> (purple), NH<sub>3</sub> (green), and H<sub>2</sub> (red). Sample was heated from 100-600°C at a rate of 2°C/min in 100% N<sub>2</sub>. Sr reacted to Sr<sub>2</sub>N, in agreement with the Ellingham diagram (Figure S106). This TGA run is also shown in Figure 6.

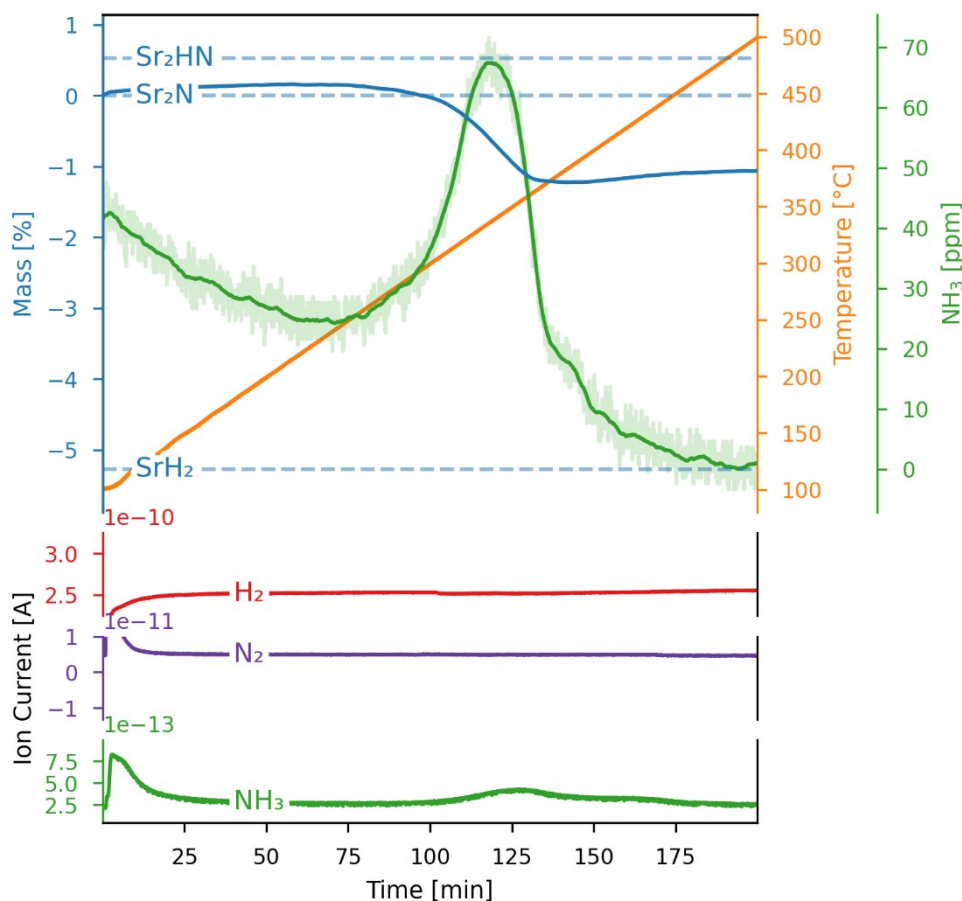


Figure S151: Variations of mass and temperature (recorded by the TGA), ion current (recorded by the mass spectrometer), and NH<sub>3</sub> concentration (recorded by the NH<sub>3</sub> analyzer) as a function of time for the Sr-nitridation under 5% H<sub>2</sub> in Ar. Blue dashed lines: theoretical mass changes for no

conversion (0%), full conversion to SrH<sub>2</sub> (-5.27%), and full conversion to Sr<sub>2</sub>HN (0.53%). The ion current signals correspond to N<sub>2</sub> (purple), NH<sub>3</sub> (green), and H<sub>2</sub> (red). Sample was heated from 100-500°C at a rate of 2°C/min in 5% H<sub>2</sub> in Ar. Sr reacted to a mixture of Sr<sub>2</sub>HN and SrH<sub>2</sub> in agreement with the Ellingham diagrams (Figure S114 and Figure S115). The NH<sub>3</sub> peak reached its maximum at 339°C. This TGA run is also shown in Figure 7.

*The W-based system*

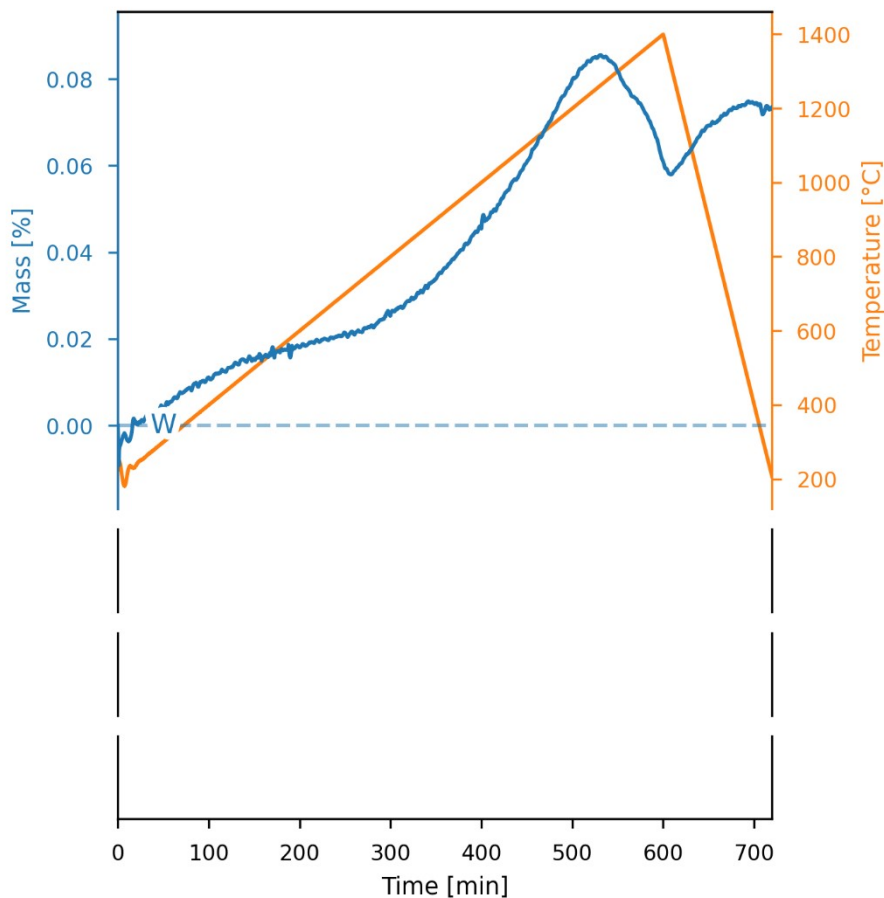


Figure S152: Variations of mass and temperature (recorded by the TGA) as a function of time for the W-nitridation under 100% N<sub>2</sub>. Blue dashed lines: theoretical mass changes for no conversion (0%). Sample was heated from 200-1400°C at a rate of 2°C/min in 100% N<sub>2</sub> and cooled down back to 200°C in 100% Ar. No significant reaction was measurable. According to the Ellingham diagram (Figure S120), the formation of W<sub>2</sub>N should be favourable in this temperature range.

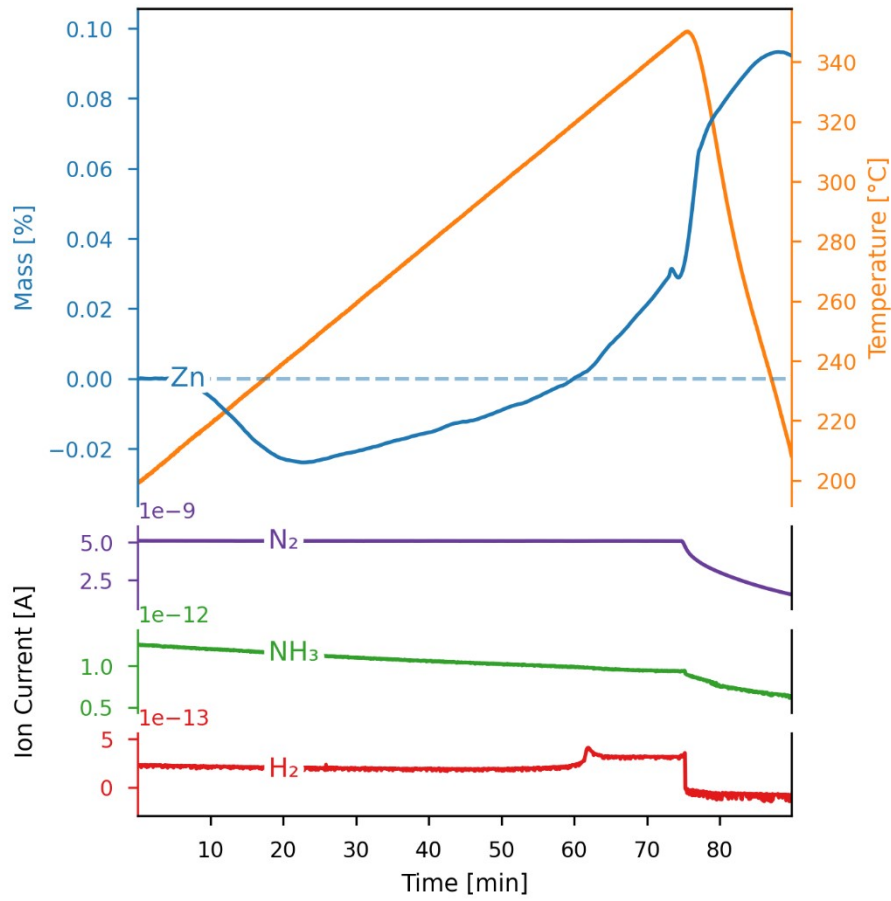


Figure S153: Variations of mass and temperature (recorded by the TGA) and ion current (recorded by the mass spectrometer) as a function of time for the Zn-nitridation under 100% N<sub>2</sub>. Blue dashed lines: theoretical mass changes for no conversion (0%). The ion current signals correspond to N<sub>2</sub> (purple), NH<sub>3</sub> (green), and H<sub>2</sub> (red). Sample was heated from 200-350°C at a rate of 2°C/min in 100% N<sub>2</sub> and cooled down back to 200°C in 100% Ar. No significant reaction was measurable, in agreement with the Ellingham diagram (Figure S128).

### 2.1 Converting ppm to mg/s for mass balance

The NH<sub>3</sub> concentration  $c_{NH_3, ppm}$  in ppm was recorded by the ABB Advance Optima AO2020 analyzer. The gas flow properties, temperature  $T$  in K, pressure  $P$  in Pa, and volumetric flow  $V$  in ml/min, were recorded by the Mesa Labs DryCal Defender 530+ Low Flow flow meter.

By definition, the concentration  $c_{NH_3, ppm}$  is defined as the moles of NH<sub>3</sub>  $n_{NH_3}$  over 1'000'000 moles in the total gas flow  $n_{gas}$ , i.e.

$$1 \text{ ppm of } NH_3 = \frac{1 \text{ mol of } NH_3}{1\,000\,000 \text{ moles of gas}}$$

The mass of NH<sub>3</sub>  $m_{NH_3}$  in g is calculated as

$$m_{NH_3} = n_{NH_3} \cdot M_{NH_3}$$

where  $M_{NH_3}$  is the molar mass of NH<sub>3</sub> in g/mol. The volume  $V$  in m<sup>3</sup> that 1'000'000 moles of gas occupy is calculated according to the ideal gas law:

$$V = \frac{1\,000\,000 \text{ mol} \cdot R \cdot T}{P}$$

where  $R$  is the universal gas constant in J/mol/K.

The mass flow of NH<sub>3</sub>  $\dot{m}_{NH_3}$  in mg/s is then given as:

$$\dot{m}_{NH_3} = \frac{m_{NH_3} \cdot 1000 \frac{mg}{g}}{V \cdot 1\,000\,000 \frac{ml}{m^3}} \cdot \frac{V}{60 \frac{s}{min}}$$

### 2.2 Solid Characterization by XRD

Figure S154 shows the XRD pattern of Kapton tape. Patterns were obtained by a Bruker AXS D2 Phaser diffractometer operated at 30 kV and 10 mA (Cu K $\alpha$ ) at  $2\theta = 5-105^\circ$ . The scanning step size and duration were 0.012° and 0.5 s, respectively. The background and K $\alpha_2$  were stripped using Bruker's DIFFRAC.EVA V3.1.

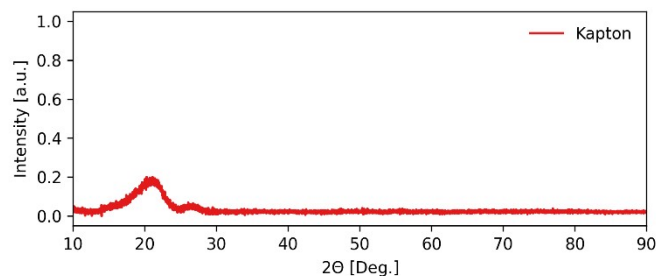


Figure S154: XRD patterns of Kapton tape. Peak intensities have been scaled to match with intensities observed in runs with a sample.

Figure S155 shows the XRD patterns of the Sr random pieces (Sigma-Aldrich, 99%, flakes in mm-range size). The sample was enclosed between two layers of Kapton tape. Patterns were obtained by a Bruker AXS D8 Advance diffractometer operated at 40 kV and 30 mA (Cu  $K\alpha$ ) at  $2\theta = 10\text{--}100^\circ$ . The scanning step size and duration were  $0.01^\circ$  and 0.5 s, respectively. The background and  $K\alpha_2$  were stripped using Bruker's DIFFRAC.EVA V7.0.

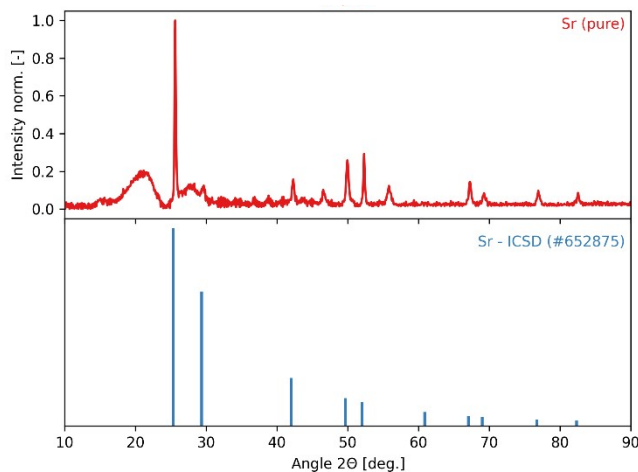


Figure S155: XRD patterns of the pure Sr. Peak intensities have been normalized.

### 3. References

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