

## †Electronic Supporting Information (ESI)

### Electrospun Polarity Controlled Molecular Orientation for Synergistic Performance of Artifact Free Piezoelectric Anisotropic Sensor †

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**Discussion D1: Estimating the value of dichroic ratio (R), minimum fraction of completely oriented dipoles ( $f_m$ ) and range of angle  $\delta$  formed by their long axis with transition dipole moment vector.<sup>1,2</sup>**

$$R = \frac{\Delta A_{parallel}}{\Delta A_{perpendicular}} \quad (1)$$

$$if R > 1: \cot^{-1}(\sqrt{R}/2); f_m = \frac{R-1}{R+2} \quad (2)$$

$$if R < 1: \cot^{-1}(\frac{\sqrt{R}}{2}) \leq \delta \leq 90^\circ; f_m = \frac{2(1-R)}{R+2} \quad (3)$$

Table S1. Variation of the dichroic ratio (R), the minimum fraction of completely oriented dipoles ( $f_m$ ) and range of angle  $\delta$  formed by their long axis with transition dipole moment vector for corresponding vibrational modes attached to the wavenumber in positive and negative electrospinning aligned and random fibers of P(VDF-CTFE).<sup>3</sup>

Fiber	$\nu$ (cm <sup>-1</sup> )	approximate normal mode assignment	R	$f_m$	Estimated $\alpha$ interval
PACF	1430	$\delta$ (CH <sub>2</sub> ) – w (CH <sub>2</sub> )	0.45	0.447	71.43° < $\alpha$ < 90°
PACF	1402	w (CH <sub>2</sub> ) + $\nu_s$ (CC)	2.24	0.292	0° < $\alpha$ < 53.18°
PACF	1280	$\nu_s$ (CF <sub>2</sub> ) + $\nu_s$ (CC) + $\delta$ (CCC)	0.64	0.270	68.16° < $\alpha$ < 90°
PACF	1182	$\nu_{as}$ (CF <sub>2</sub> ) + $\rho$ (CF <sub>2</sub> ) + $\rho$ (CH <sub>2</sub> )	1.02	0.008	0° < $\alpha$ < 63.16°
PACF	1073	$\nu_{as}$ (CC) + w (CF <sub>2</sub> ) + w (CH <sub>2</sub> )	2.09	0.267	0° < $\alpha$ < 54.11°
PACF	883	$\rho$ (CH <sub>2</sub> ) + $\nu_{as}$ (CF <sub>2</sub> ) + $\rho$ (CF <sub>2</sub> )	0.91	0.061	64.48° < $\alpha$ < 90°
PACF	841	$\nu_s$ (CF <sub>2</sub> ) + $\nu_s$ (CC)	0.78	0.157	66.15° < $\alpha$ < 90°
PRCF	1430	$\delta$ (CH <sub>2</sub> ) – w (CH <sub>2</sub> )	0.98	0.010	63.61° < $\alpha$ < 90°
PRCF	1402	w (CH <sub>2</sub> ) + $\nu_s$ (CC)	1.01	0.003	0° < $\alpha$ < 63.30°
PRCF	1280	$\nu_s$ (CF <sub>2</sub> ) + $\nu_s$ (CC) + $\delta$ (CCC)	0.95	0.033	64.01° < $\alpha$ < 90°
PRCF	1182	$\nu_{as}$ (CF <sub>2</sub> ) + $\rho$ (CF <sub>2</sub> ) + $\rho$ (CH <sub>2</sub> )	0.97	0.018	63.75° < $\alpha$ < 90°
PRCF	1073	$\nu_{as}$ (CC) + w (CF <sub>2</sub> ) + w (CH <sub>2</sub> )	0.99	0.002	63.45° < $\alpha$ < 90°
PRCF	883	$\rho$ (CH <sub>2</sub> ) + $\nu_{as}$ (CF <sub>2</sub> ) + $\rho$ (CF <sub>2</sub> )	0.95	0.027	63.90° < $\alpha$ < 90°
PRCF	841	$\nu_s$ (CF <sub>2</sub> ) + $\nu_s$ (CC)	0.96	0.021	63.61° < $\alpha$ < 90°
NACF	1430	$\delta$ (CH <sub>2</sub> ) – w (CH <sub>2</sub> )	0.24	0.679	76.24° < $\alpha$ < 90°
NACF	1402	w (CH <sub>2</sub> ) + $\nu_s$ (CC)	2.33	0.307	0° < $\alpha$ < 52.63°
NACF	1280	$\nu_s$ (CF <sub>2</sub> ) + $\nu_s$ (CC) + $\delta$ (CCC)	0.75	0.178	66.51° < $\alpha$ < 90°
NACF	1182	$\nu_{as}$ (CF <sub>2</sub> ) + $\rho$ (CF <sub>2</sub> ) + $\rho$ (CH <sub>2</sub> )	1.04	0.013	0° < $\alpha$ < 62.99°
NACF	1073	$\nu_{as}$ (CC) + w (CF <sub>2</sub> ) + w (CH <sub>2</sub> )	2.01	0.252	0° < $\alpha$ < 54.63°
NACF	883	$\rho$ (CH <sub>2</sub> ) + $\nu_{as}$ (CF <sub>2</sub> ) + $\rho$ (CF <sub>2</sub> )	0.92	0.052	64.34° < $\alpha$ < 90°
NACF	841	$\nu_s$ (CF <sub>2</sub> ) + $\nu_s$ (CC)	0.93	0.049	63.57° < $\alpha$ < 90°
NRCF	1430	$\delta$ (CH <sub>2</sub> ) – w (CH <sub>2</sub> )	0.98	0.008	64.28° < $\alpha$ < 90°
NRCF	1402	w (CH <sub>2</sub> ) + $\nu_s$ (CC)	0.92	0.056	64.40° < $\alpha$ < 90°
NRCF	1280	$\nu_s$ (CF <sub>2</sub> ) + $\nu_s$ (CC) + $\delta$ (CCC)	1.02	0.007	0° < $\alpha$ < 63.52°
NRCF	1182	$\nu_{as}$ (CF <sub>2</sub> ) + $\rho$ (CF <sub>2</sub> ) + $\rho$ (CH <sub>2</sub> )	0.99	0.005	63.43° < $\alpha$ < 90°
NRCF	1073	$\nu_{as}$ (CC) + w (CF <sub>2</sub> ) + w (CH <sub>2</sub> )	0.91	0.058	63.35° < $\alpha$ < 90°
NRCF	883	$\rho$ (CH <sub>2</sub> ) + $\nu_{as}$ (CF <sub>2</sub> ) + $\rho$ (CF <sub>2</sub> )	1.01	0.002	0° < $\alpha$ < 63.55°
NRCF	841	$\nu_s$ (CF <sub>2</sub> ) + $\nu_s$ (CC)	0.98	0.007	63.57° < $\alpha$ < 90°

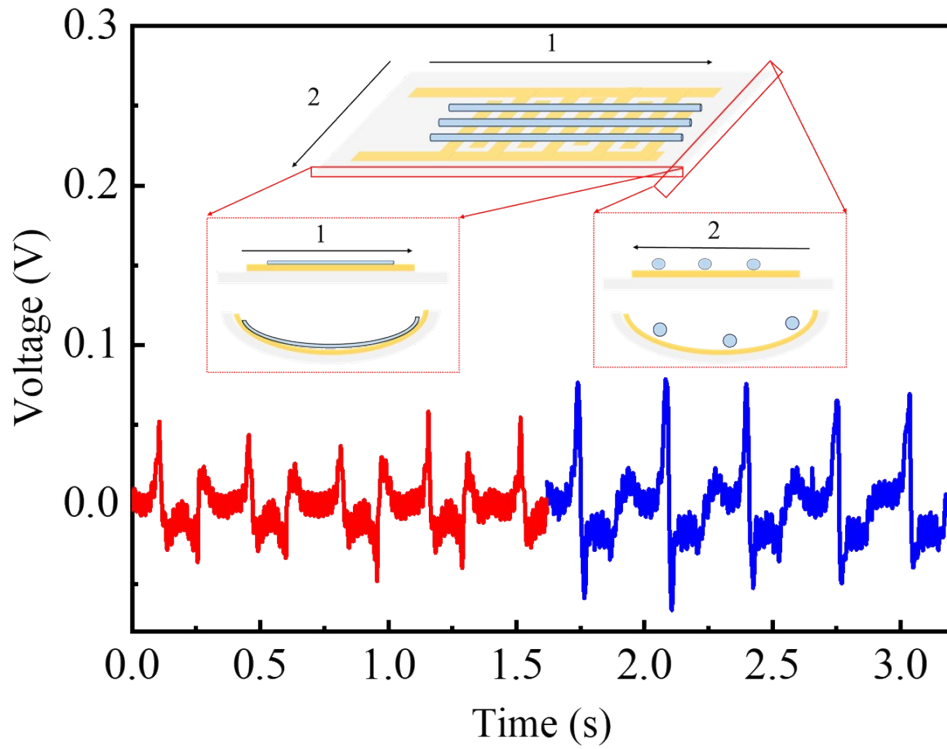


Figure S1. Voltage vs time response under different bending modes (bending angle  $60^\circ$ ) to investigate the lateral anisotropy with insets describing the corresponding bending along 1 and 2 axes.

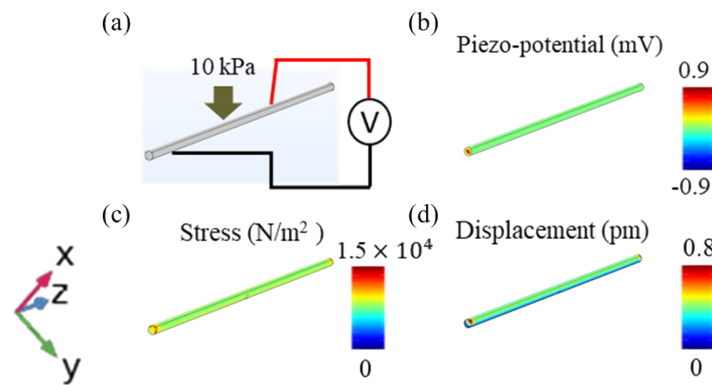


Figure S2. Finite element analysis (a) describing  $d_{32}$  mode fiber under stress with corresponding (b) piezo-potential, (c) distribution of stress and (d) displacement generated in the fiber.

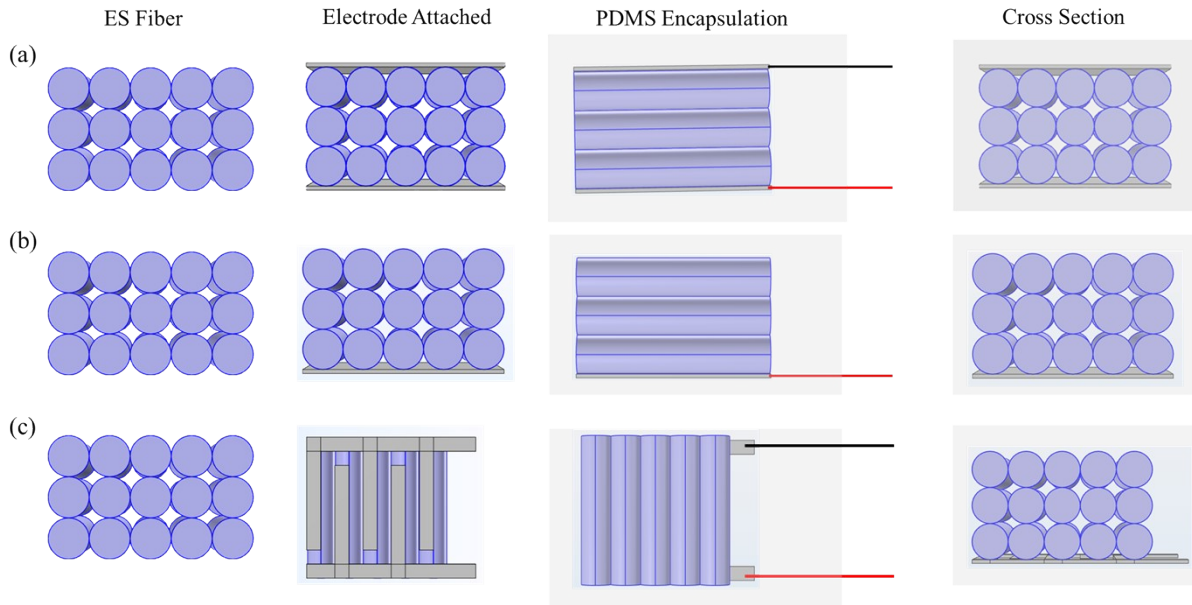


Figure S3. Schematic of the step-wise device fabrication for (a) ferroelectret, (b) triboelectric and (c) piezoelectric signal measurement. In particular, three principal steps of fabrication, viz., ES fiber arrangement, electrode attachment and PDMS encapsulation are shown. In each, the cross-section views are also illustrated to demonstrate three different types of devices, viz., ferroelectret, triboelectric and piezoelectric sensors.

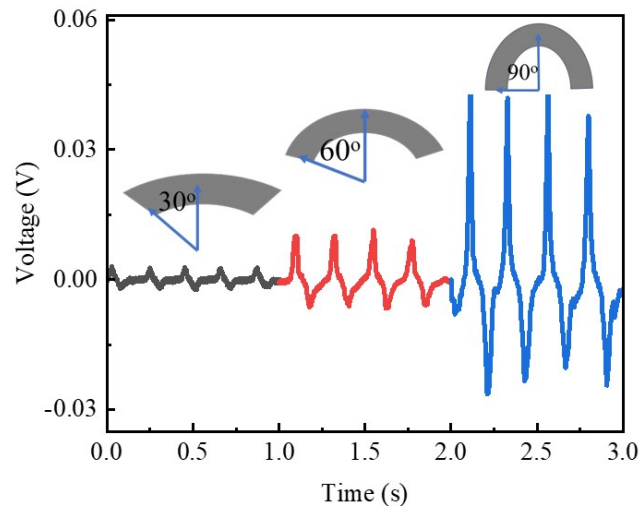


Figure S4. PENG response under different bending angles of 30°, 60° and 90°. The schematics of corresponding bending angles are shown in the inset.

## References:

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