

Supplemental Information

Multifunctional Strain-activated Liquid-metal Composite Film with Electromechanical Decoupling for Stretchable Electromagnetic Shielding

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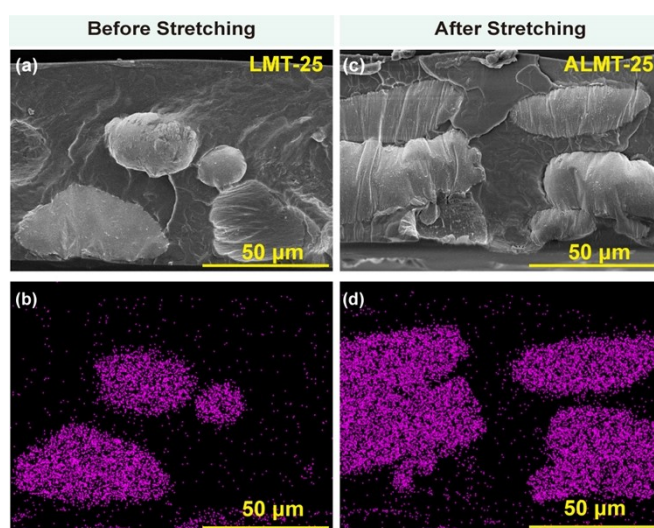


Figure S1. SEM images of LMT-25 (a, b) and ALMT-25 (c,d) with corresponding EDS elemental mapping results for Ga.

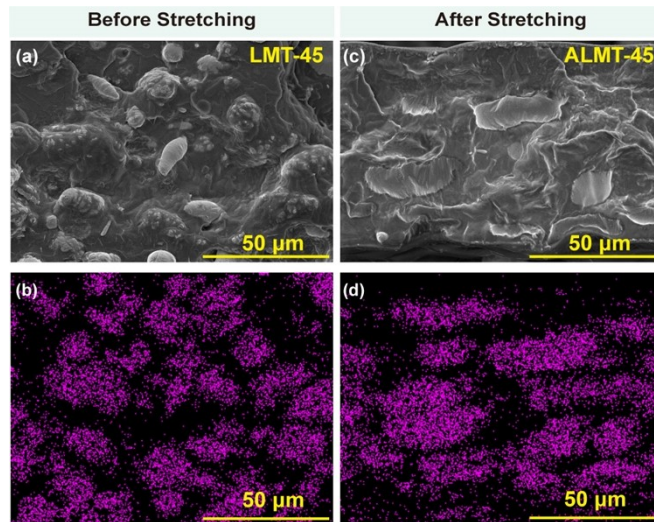


Figure S2. SEM images of LMT-45 (a, b) and ALMT-45 (c,d) with corresponding EDS elemental mapping results for Ga.

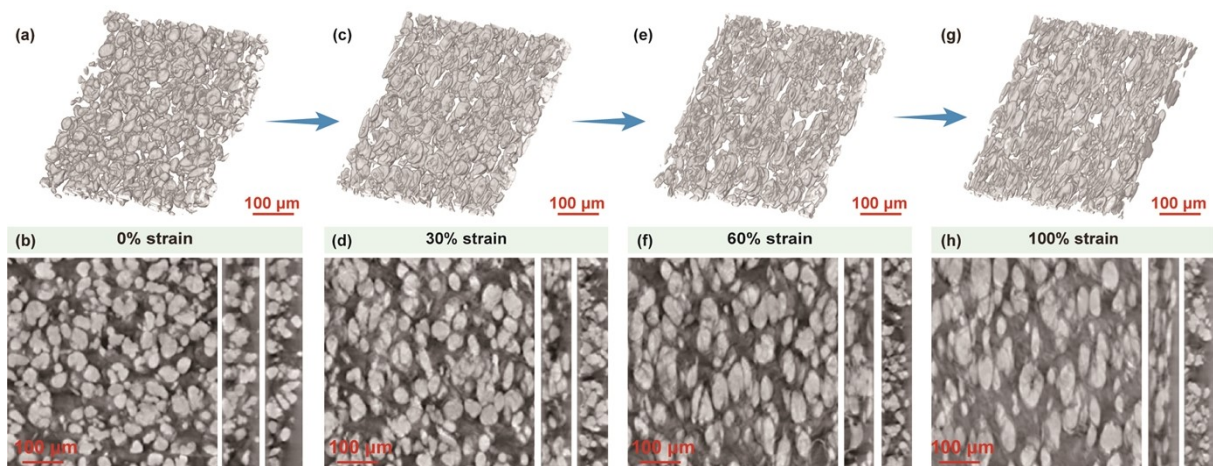


Figure S3. Micro-CT image of LMT-35 during stretching.

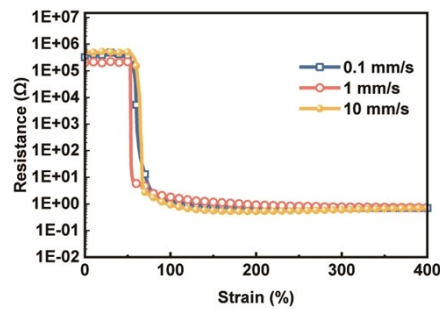


Figure S4. Resistance versus strain of LMT-35 (rate = 0.1, 1, and 10 mm/s).

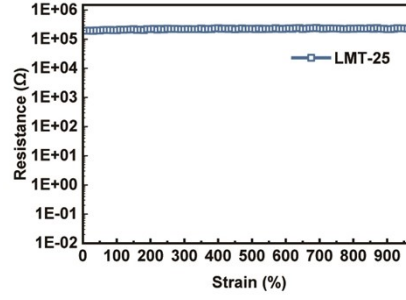


Figure S5. Resistance versus strain of LMT-25 (rate = 0.1 mm/s).

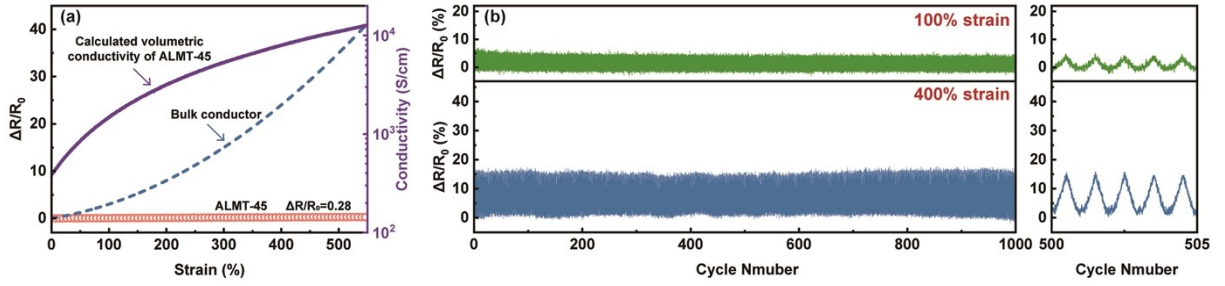


Figure S6. (a) Relative change in resistance and corresponding volumetric conductivity of ALMT-45 under strains of up to 550%, and theoretical relative change in resistance of the bulk conductor. (b) Relative change in resistance of ALMT-45 over 1000 cycles to 100% and 400% strain. (c) Relative change in resistance of ALMT-45 over 500 cycles to 100% and 400% strain.

Assume that the resistance, thickness, widths, length, volume, electrical resistivity, and conductivity of the sample at time t is R_t , T_t , W_t , L_t , $V_t = W_t T_t L_t$, ρ_t , and σ_t , respectively.

At $t = 0$,

$$R_0 = \frac{\rho_0 L_0}{S_0} = \frac{\rho_0 L_0}{W_0 T_0} = \rho_0 \frac{L_0^2}{V_0} = \frac{1}{\sigma_0} \frac{L_0^2}{V_0}$$

At $t = t$,

$$\varepsilon_t = \frac{L_t - L_0}{L_0}$$

$$R_t = \frac{\rho_t L_t}{W_t T_t} = \rho_t \frac{L_t^2}{V_t} = \frac{1}{\sigma_t} \frac{L_t^2}{V_t} = \frac{1}{\sigma_t} \frac{(1 + \varepsilon_t)^2 L_0^2}{V_t}$$

$$\frac{R_t}{R_0} = \frac{\sigma_0 V_0}{\sigma_t V_t} (1 + \varepsilon_t)^2$$

The volume of the sample is assumed to be constant during stretching ($V_0 = V_t$),

$$\frac{R_t}{R_0} = \frac{\sigma_0}{\sigma_t} (1 + \varepsilon_t)^2$$

(a) If the conductivity of the sample remains constant during stretching ($\sigma_0 = \sigma_t$),

$$\frac{R_t}{R_0} = (1 + \varepsilon_t)^2$$

(b) If conductivity changes with strain,

$$\sigma_t = \frac{\sigma_0 (1 + \varepsilon_t)^2 R_0}{R_t}$$

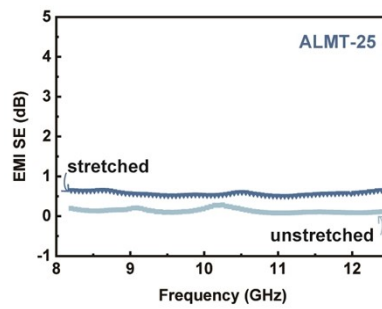


Figure S7. The EMI SE curves of ALMT-25.

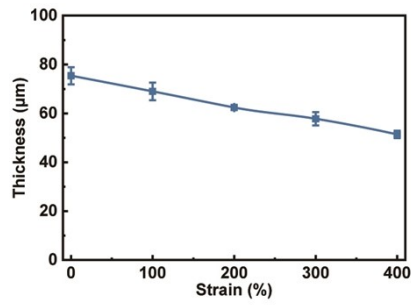


Figure S8. Thickness variation of ALMT-35 under different strains.

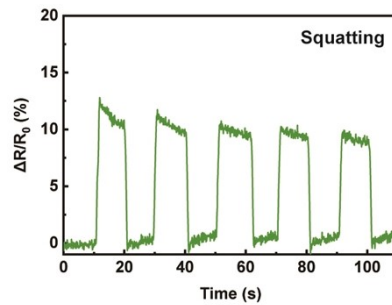


Figure S9. Relative resistance change of the ALMT sensor at the knee joint during squatting.**Table S1.** Comparisons of stretchable conductors reported in recent literature.

| Type | Filler | Matrix | ϵ_{\max} | σ_0 (S/cm) | $\Delta R_t/R_0$ at max strain | σ_t (S/cm) | QF | Ref. |
|----------------------|--------------------------|--|-------------------|-------------------|--|--------------------------|---|------------------|
| Liquid metal fillers | EGaInSn (35 vol%) | TPU | 700% | 266 | 0.57@700% | 14000@700% | 12@700% | This work |
| | EGaInSn (45 vol%) | TPU | 550% | 378 | 0.28@550% | 12700@550% | 20@550% | |
| | EGaInSn and Fe particles | Ecoflex | 600% | / | / | 25000@400% | / | 1 |
| | 3D EGaIn network | Ecoflex | 510% | 5300 | / | 11000@510% | / | 2 |
| | EGaIn | SBS | 1800% | 100 | 0.04@1800% | / | 2-441@1800% | 3 |
| | EGaIn | VHB | ~1200% | 20600 | ~3.5 @1200% | / | ~3.4@1200% | 4 |
| | EGaIn + Ag | SIS | ~1200% | 8210 | 40~70 @1200% | / | 0.3~3@1200% | 5 |
| | EGaIn | 11-PUA | 744% | 2500 | 0.85@700% | 20000@700% | 8.2@700% | 6 |
| | EGaIn | TPU | 1000% | 4200 | 20@1000% | 11100@300% 3800@1000% | 0.5@1000% | 7 |
| | EGaIn | TPU | 2260% | 22532 | 0.34@1000% 1.59@1600% 31.6@2266% | / | 29.4@1000% 10.06@1600% 0.74@2266% | 8 |
| | EGaIn | TPU | 4100 | 21000 | 19.8@4100% | / | 9.3@4100% | 9 |
| | EGaIn | PVDF | 740% | 435 | 4@740% | / | 1.85@740% | 10 |
| | EGaIn + Ag | EVA | 1000% | 8331 | 10@1000% | / | 1@1000% | 11 |
| | EGaIn + Ag | SIS | 100% | 6380 | 6.78@1000% | / | 1.47@1000% | 12 |
| | EGaIn + Ag | PUA | 2500% | 6250 | 9@2500% | / | 2.78@2500% | 13 |
| | EGaIn + Ni | P(AAm-co-MAAc) | 630% | 2000 | 5.4@630% | / | 1.17@630% | 14 |
| | EGaIn | SEBS | 900% | 34000 | 39@700% | / | 0.2@700% | 15 |
| EGaIn | PVP | 800% | 6900 | 60@800% | 100 | ~0.13@800% | 16 | |
| EGaIn | SIS | 2500% | 30000 | 37@2500% | / | ~0.68@2500% | 17 | |
| Rigid metal fillers | AgNPs | SEBS | 180% | 11.4 | 1.05@180% | 84.6@180% | 1.7@180% | 18 |
| | Ag flakes | Fluorine rubber | 215% | 738 | ~39.2@215% | ~180@215% | ~0.055 | 19 |
| Rigid metal fillers | Ag flakes | Fluorine rubber PAAm alginate hydrogel | 400% | 4000 | ~106 @ 400% | 950@400% | ~0.038 | 20 |
| | Ag flakes | Fluorine rubber PAAm alginate hydrogel | 250% | 374 | 70 @250% | / | ~0.036 | 21 |
| | Ag flakes | Ecoflex | 1780% | ~133 | 153 @ 1780% | / | ~0.12 | 22 |
| | AuNPs | TPU | 115% | 11000 | ~20.2 @115% | 210@110% | ~0.057 | 23 |
| | AgNW | PNIPAM | 800% | 93 | 3@700% | / | ~2.3@700% | 24 |
| | AgNW/Au | SBS | 840% | 30000 | ~2649 @840% | 3000@840% | ~0.003 | 25 |
| | Cu | rubber | 100% | 215 | / | 2@100% | / | 26 |

| Type | Filler | Matrix | ϵ_{max} | σ_0 (S/cm) | $\Delta R_t/R_0$ at max strain | σ_t (S/cm) | QF | Ref. |
|------------------|----------|-----------------|------------------|-------------------|--------------------------------|-------------------|-------------|------|
| Carbon materials | CNT+AgNW | PVDF | 140% | 5710 | ~1306 @140% | 20 | ~0.001@140% | 27 |
| | CNT | Fluorine rubber | 118% | 10 | ~3.75@118% | 10 | ~0.3@118% | 28 |
| | CNT | Fluorine rubber | 134% | 57 | ~51@134% | 6 | ~0.026@134% | 29 |
| | CNT | PDMS | 150% | 1100 | 4@150% | / | 0.375@150% | 30 |
| | CNT | PU | 300% | 0.05-1 | 3.2@300% | / | 0.9@300% | 31 |

SBS: poly(styrene-block-butadiene-block-styrene)

VHB: 3M VHB tape

SIS: Styrene-isoprene block copolymers

11-PUA: 11-(phosphonoundecyl)acrylate

PVDF: polyvinylidene difluoride

EVA: Ethylene-Vinyl Acetate

PUA: polyurethane acrylate

P(AAm-co-MAAc): Poly(acrylamide-co-methacrylic acid)

SEBS: poly[styrene-*b*-(ethylene-co-butylene)-*b*-styrene]

PVP: Polyvinyl pyrrolidone

PAAm: polyacrylamide

PAM: Polyacrylamide

PNIPAM: poly(N-isopropyl acrylamide)

PU: polyurethane

Table S2. Comparisons of stretchable EMI shielding materials reported in recent literature.

| Type | Filler | Matrix | Strain (%) | Thickness (mm) | SE (dB) | SSE (dB/mm) | Ref. |
|----------------------|--------------------------|-----------------|------------|----------------|-----------|-------------|------------------|
| Liquid metal fillers | EgInSn (35 vol%) | TPU | 0-400% | 0.075-0.051 | 58.1-63.8 | 774-1241 | This work |
| | EgInSn (45 vol%) | TPU | / | 0.094 | 80.9 | 860.6 | |
| | EGaInSn and Fe particles | Ecoflex | 0-400% | 0.8-0.2 | 20.6-80.7 | 25.8-404 | 1 |
| | 3D EBiInSn network | Ecoflex | 0-400% | 2-3.6 | 57.0-85.0 | 15.8-42.5 | 32 |
| Liquid metal fillers | 3D EGaIn network | Ecoflex | 0-400% | 2-1 | 41.5-81.6 | 20.8-81.6 | 2 |
| | EGaIn | PDMS | 0-50% | 2.4 | 50.0-43.5 | 20.8-18.1 | 33 |
| | EGaIn | PDMS | 0-100% | 3 | ~37.0 | 12.3 | 34 |
| | EGaInSn | PDMS | 0-75% | 0.15-0.11 | 43.2-44.2 | 288-401 | 35 |
| | EGaInSn | PDMS/Textile | 0-50% | 0.35 | 72.6-52.4 | 149.7-207.4 | 36 |
| | EGaIn and CNT | PAM and gelatin | 0-200% | 1-0.22 | 17.7-37.4 | 17.7-170.0 | 37 |
| | ESnBi | PVDF | / | 2 | 68.8 | 34.4 | 38 |
| EGaIn | CNF | / | 0.1 | 40.5 | 405.0 | 39 | |
| EGaIn | EM | / | 1 | 90.6 | 90.6 | 40 | |

| Type | Filler | Matrix | Strain (%) | Thickness (mm) | SE (dB) | SSE (dB /mm) | Ref. |
|---------------------|------------------|--------|------------|----------------|-----------|--------------|------|
| | EGaIn and Ag NPs | SEBS | 300% | 0.2 | 73.5 | 367.5 | 41 |
| | EGaIn foam | / | / | 5 | 65.0 | 13.0 | 42 |
| Rigid metal fillers | AgNPs | SEBS | 0-100% | 2.84 | 28.0-55.0 | 19.4-9.9 | 18 |
| | AgNWs | PU | 0-30% | 0.6 | 63.9-56.2 | 106.5-93.7 | 43 |
| | Cu | rubber | 0-75% | 0.4 | 35.7-10.7 | 89-26.7 | 26 |
| Carbon materials | CNT | PU | 0-30% | 2.9 | 36.4-20.2 | 12.6-7.0 | 44 |
| | CNT | TPU | 0-200% | 2-1.56 | 34.6-12.8 | 17.3-8.2 | 45 |
| | rGO | PDMS | 0-100% | 2.4 | 25.0-18.0 | 10.5-7.5 | 46 |
| | MXene | PU | 0-30% | 0.2 | 22.0 | 105.0 | 47 |
| | MXene | TPU | 0-70% | 0.3 | 31.4-22.0 | 104.7-73.3 | 48 |

PDMS: Polydimethylsiloxane

CNF: Cellulose nanofibers

EM: expandable microsphere

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