

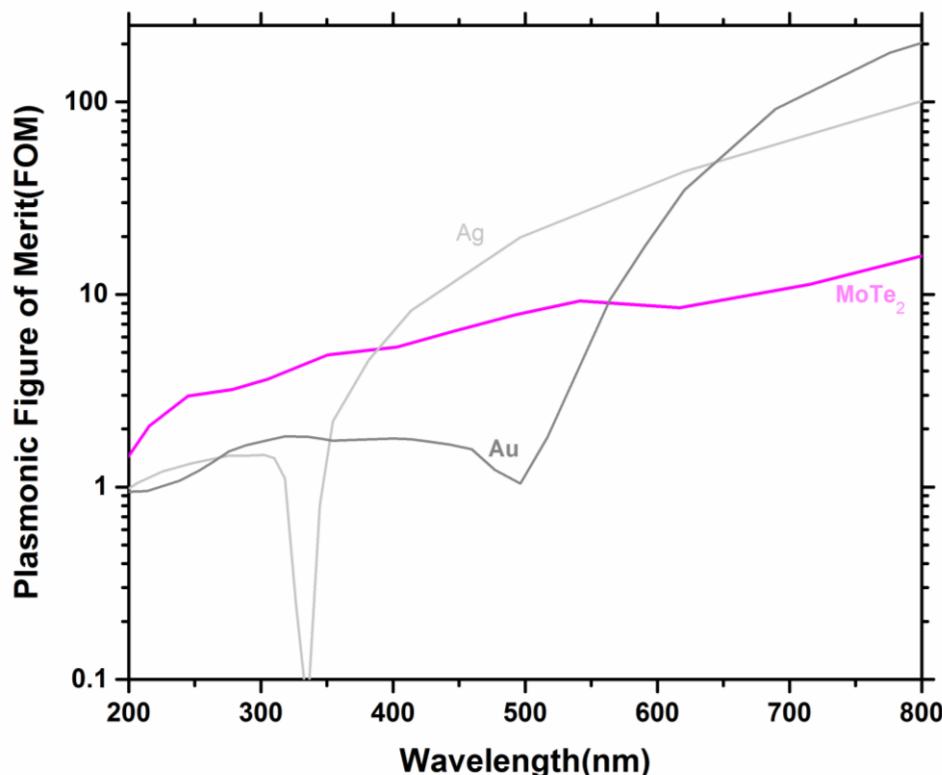
Optimization of plasmonic lens structure for maximum optical vortices induced on Weyl Semimetals Surface States

Ritwik Banerjee¹ and Tanmoy Maiti¹¹

¹ Plasmonics and Perovskites Laboratory, Indian Institute of Technology Kanpur, UP, 208016, India

Supporting information

S1. Comparison of figure of merit (FOM) between different materials



9 Figure S1: Comparison of figure of merits between MoTe_2 Weyl semimetal, Au and Ag

10 Type II Weyl semimetal surface state is prominent in MoTe₂. [1] The permittivity matrix for
 11 Weyl semimetals surface states can be represented as:

¹ Corresponding author Tel: +91-512-259-6599

Email address: tmaiti@iitk.ac.in (Tanmoy Maiti)

12

$$\varepsilon_{WS} = \begin{pmatrix} \varepsilon_{xx} & \varepsilon_{xy} & \varepsilon_{xz} \\ \varepsilon_{xy}^* & \varepsilon_{yy} & \varepsilon_{yz} \\ \varepsilon_{xz}^* & \varepsilon_{yz}^* & \varepsilon_{zz} \end{pmatrix}$$

13 Here, off diagonal elements ε_{xy}^* , ε_{xz}^* and ε_{yz}^* represents the complex conjugate of ε_{xy} , ε_{xz} and
14 ε_{yz} . The non-zero off-diagonal tensor elements originate from the non-vanishing Berry
15 curvature of the Weyl semimetals.

16 **S2. Analytical calculations of Electric field and phase maps under x-
17 polarized and y-polarized illumination for hexagonal lens:**

18 Further let's extend our calculation of electric field for linearly polarized lights. In case of x-
19 polarized light, $\varphi(\theta') = \theta'$ and $(\theta') = 0$.

20 $\omega(\phi(\theta'), \theta') = \phi(\theta') = 0$.

21 $A(\phi(\theta')) = A_0 \cos \varphi(\theta') = A_0 \cos \theta'$.

22 Plugging all the values in equation 3 and integrating it to 0 to 2π , we get-

23

$$E_z(\rho, \theta, z)_{\theta' \in [0, 2\pi]} = A_o e^{-k_a z} \left[\int_0^{\pi/3} \cos \theta' e^{jk_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{\pi}{6}) \cos(\theta - \theta')}} + \right.$$

24

$$\left. \int_{\pi/3}^{2\pi/3} \cos \theta' e^{jk_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{3\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{3\pi}{6}) \cos(\theta - \theta')}} + \right.$$

25

$$\left. \int_{2\pi/3}^{\pi} \cos \theta' e^{jk_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{5\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{5\pi}{6}) \cos(\theta - \theta')}} + \right.$$

26

$$\left. \int_{\pi}^{4\pi/3} \cos \theta' e^{jk_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{7\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{7\pi}{6}) \cos(\theta - \theta')}} + \right]$$

27
$$\int_{4\pi/3}^{5\pi/3} \cos \theta' e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{9\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{9\pi}{6}) \cos(\theta - \theta')}} +$$

28
$$\left. \int_{5\pi/3}^{2\pi} \cos \theta' e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{11\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{11\pi}{6}) \cos(\theta - \theta')}} \right] d\theta' \dots (S1)$$

29 For y-polarised light, $\varphi(\theta') = \frac{\pi}{2} - \theta'$ and $(\theta') = \frac{\pi}{2}$.

30 $\omega(\phi(\theta'), \theta') = \phi(\theta') = \frac{\pi}{2}$.

31 $A(\phi(\theta')) = A_0 \cos \varphi(\theta') = A_0 \cos(\frac{\pi}{2} - \theta') = A_0 \sin \theta'$.

32 Calculating electric field in z-direction for y-polarized light, we get-

33 $E_z(\rho, \theta, z)_{\theta' \in [0, 2\pi]}$

34 $= A_o e^{-k_a z} \left[\int_0^{\pi/3} \sin \theta' e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{\pi}{6}) \cos(\theta - \theta')}} \right.$

35 $+ \int_{\pi/3}^{2\pi/3} \sin \theta' e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{3\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{3\pi}{6}) \cos(\theta - \theta')}} \right]$

36 $+ \int_{2\pi/3}^{\pi} \sin \theta' e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{5\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{5\pi}{6}) \cos(\theta - \theta')}} \right]$

37 $+ \int_{\pi}^{4\pi/3} \sin \theta' e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{7\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{7\pi}{6}) \cos(\theta - \theta')}} \right]$

38 $+ \int_{4\pi/3}^{5\pi/3} \sin \theta' e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{9\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{9\pi}{6}) \cos(\theta - \theta')}} \right]$

39 $+ \left. \int_{5\pi/3}^{2\pi} \sin \theta' e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{11\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{11\pi}{6}) \cos(\theta - \theta')}} \right] d\theta' \dots (S2)$

40 $e^{-j\theta'}$ can be written as $(\cos \theta' - j \sin \theta')$. Therefore, equation 9 in the main manuscript,
41 electric field intensity for hexagonal lens, under RCP illumination can also be written as-
42 $E_z(\rho, \theta, z)_{\theta' \in [0, 2\pi]} =$

$$43 A_o e^{-k_a z} \left[\int_0^{\pi/3} \cos \theta' e^{jk_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{\pi}{6}) \cos(\theta - \theta')}} + \right.$$

$$44 \int_{\pi/3}^{2\pi/3} \cos \theta' e^{jk_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{3\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{3\pi}{6}) \cos(\theta - \theta')}} +$$

$$45 \int_{2\pi/3}^{\pi} \cos \theta' e^{jk_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{5\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{5\pi}{6}) \cos(\theta - \theta')}} +$$

$$46 \int_{\pi}^{4\pi/3} \cos \theta' e^{jk_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{7\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{7\pi}{6}) \cos(\theta - \theta')}} +$$

$$47 \int_{4\pi/3}^{5\pi/3} \cos \theta' e^{jk_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{9\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{9\pi}{6}) \cos(\theta - \theta')}} +$$

$$48 \int_{5\pi/3}^{2\pi} \cos \theta' e^{jk_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{11\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{11\pi}{6}) \cos(\theta - \theta')}} \Bigg\} -$$

$$49 j \left\{ \int_0^{\pi/3} \sin \theta' e^{jk_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{\pi}{6}) \cos(\theta - \theta')}} + \right.$$

$$50 \int_{\pi/3}^{2\pi/3} \sin \theta' e^{jk_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{3\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{3\pi}{6}) \cos(\theta - \theta')}} +$$

$$51 \int_{2\pi/3}^{\pi} \sin \theta' e^{jk_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{5\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{5\pi}{6}) \cos(\theta - \theta')}} +$$

52

$$\int_{\pi}^{4\pi/3} \sin\theta' e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{7\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{7\pi}{6}) \cos(\theta - \theta')}} +$$

53

$$\int_{4\pi/3}^{5\pi/3} \sin\theta' e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{9\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{9\pi}{6}) \cos(\theta - \theta')}} +$$

54

$$\left. \int_{5\pi/3}^{2\pi} \sin\theta' e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{11\pi}{6})\}^2 - 2\rho r_o \sec(\theta' - \frac{11\pi}{6}) \cos(\theta - \theta')}} \right\} d\theta' \dots (S3)$$

55 So, for hexagonal lens structures electric field under RCP polarization ($E_z(\rho, \theta, z)_{RCP}$) will
 56 be a combination of electric field due to x-polarized light ($E_z(\rho, \theta, z)_{x-P}$) and y polarized
 57 light ($E_z(\rho, \theta, z)_{y-P}$) and can be written as, $E_z(\rho, \theta, z)_{RCP} = E_z(\rho, \theta, z)_{x-P} -$
 58 $j E_z(\rho, \theta, z)_{y-P}$. Similarly electric field under LCP, $E_z(\rho, \theta, z)_{LCP} = E_z(\rho, \theta, z)_{x-P} +$
 59 $j E_z(\rho, \theta, z)_{y-P}$.

60 **S3. Analytical calculations for heptagonal lens under circular polarization:**

61 For non-symmetric Heptagonal plasmonic lens, the electric field for LCP similarly can be
 62 derived as follows-

63 $[E_z(\rho, \theta, z)_{\theta' \in [0, 2\pi]}]_{LCP} =$

64 $A_o e^{-k_a z} \left[\int_0^{2\pi/7} e^{j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{\pi}{7})\}^2 - 2\rho r_o \sec(\theta' - \frac{\pi}{7}) \cos(\theta - \theta')}} + \right.$

65 $\int_{2\pi/7}^{4\pi/7} e^{j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{3\pi}{7})\}^2 - 2\rho r_o \sec(\theta' - \frac{3\pi}{7}) \cos(\theta - \theta')}} +$

66 $\int_{4\pi/7}^{6\pi/7} e^{j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{5\pi}{7})\}^2 - 2\rho r_o \sec(\theta' - \frac{5\pi}{7}) \cos(\theta - \theta')}} +$

67 $\left. \int_{6\pi/7}^{8\pi/7} e^{j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{7\pi}{7})\}^2 - 2\rho r_o \sec(\theta' - \frac{7\pi}{7}) \cos(\theta - \theta')}} \right]$

68
$$\int_{8\pi/7}^{10\pi/7} e^{j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{9\pi}{7})\}^2 - 2\rho r_o \sec(\theta' - \frac{9\pi}{7}) \cos(\theta - \theta')}} +$$

69
$$\int_{10\pi/7}^{12\pi/7} e^{j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{11\pi}{7})\}^2 - 2\rho r_o \sec(\theta' - \frac{11\pi}{7}) \cos(\theta - \theta')}} +$$

70
$$\int_{12\pi/7}^{2\pi} e^{j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{13\pi}{7})\}^2 - 2\rho r_o \sec(\theta' - \frac{13\pi}{7}) \cos(\theta - \theta')}} \Bigg] d\theta' ... (S4)$$

71 **S4. Analytical calculations for octagonal lens under circular polarization:**

72 From equation 10 derived in the main manuscript, Electric field under RCP polarisation for
 73 octagonal plasmonic lens can also be written as-

74
$$E_z(\rho, \theta, z)_{\theta' \in [0, 2\pi]} = A_o e^{-k_a z} \left[\int_0^{\pi/4} e^{-j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{\pi}{8})\}^2 - 2\rho r_o \sec(\theta' - \frac{\pi}{8}) \cos(\theta - \theta')}} + \right.$$

75
$$\int_{\pi/4}^{\pi/2} e^{-j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{3\pi}{8})\}^2 - 2\rho r_o \sec(\theta' - \frac{3\pi}{8}) \cos(\theta - \theta')}} +$$

76
$$\int_{\pi/2}^{3\pi/4} e^{-j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{5\pi}{8})\}^2 - 2\rho r_o \sec(\theta' - \frac{5\pi}{8}) \cos(\theta - \theta')}} +$$

77
$$\int_{3\pi/4}^{\pi} e^{-j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{7\pi}{8})\}^2 - 2\rho r_o \sec(\theta' - \frac{7\pi}{8}) \cos(\theta - \theta')}} +$$

78
$$\int_{\pi}^{5\pi/4} e^{-j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{9\pi}{8})\}^2 - 2\rho r_o \sec(\theta' - \frac{9\pi}{8}) \cos(\theta - \theta')}} +$$

79
$$\int_{5\pi/4}^{3\pi/2} e^{-j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{11\pi}{8})\}^2 - 2\rho r_o \sec(\theta' - \frac{11\pi}{8}) \cos(\theta - \theta')}} +$$

80
$$\int_{3\pi/2}^{7\pi/4} e^{-j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{13\pi}{8})\}^2 - 2\rho r_o \sec(\theta' - \frac{13\pi}{8}) \cos(\theta - \theta')}} +$$

81
$$\left. \int_{7\pi/4}^{2\pi} e^{-j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{15\pi}{8})\}^2 - 2\rho r_o \sec(\theta' - \frac{15\pi}{8}) \cos(\theta - \theta')}} \right] d\theta' \dots (S5)$$

82 Similarly for octagonal lens, Electric field due to LCP can be found out as-

83
$$E_z(\rho, \theta, z)_{\theta' \in [0, 2\pi]} = A_o e^{-k_a z} \left[\int_0^{\pi/4} e^{j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{\pi}{8})\}^2 - 2\rho r_o \sec(\theta' - \frac{\pi}{8}) \cos(\theta - \theta')}} + \right.$$

84
$$\left. \int_{\pi/4}^{\pi/2} e^{j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{3\pi}{8})\}^2 - 2\rho r_o \sec(\theta' - \frac{3\pi}{8}) \cos(\theta - \theta')}} + \right.$$

85
$$\left. \int_{\pi/2}^{3\pi/4} e^{j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{5\pi}{8})\}^2 - 2\rho r_o \sec(\theta' - \frac{5\pi}{8}) \cos(\theta - \theta')}} + \right.$$

86
$$\left. \int_{3\pi/4}^{\pi} e^{j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{7\pi}{8})\}^2 - 2\rho r_o \sec(\theta' - \frac{7\pi}{8}) \cos(\theta - \theta')}} + \right.$$

87
$$\left. \int_{\pi}^{5\pi/4} e^{j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{9\pi}{8})\}^2 - 2\rho r_o \sec(\theta' - \frac{9\pi}{8}) \cos(\theta - \theta')}} + \right.$$

88
$$\left. \int_{5\pi/4}^{3\pi/2} e^{j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{11\pi}{8})\}^2 - 2\rho r_o \sec(\theta' - \frac{11\pi}{8}) \cos(\theta - \theta')}} + \right.$$

89
$$\left. \int_{3\pi/2}^{7\pi/4} e^{j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{13\pi}{8})\}^2 - 2\rho r_o \sec(\theta' - \frac{13\pi}{8}) \cos(\theta - \theta')}} + \right.$$

90
$$\left. \int_{7\pi/4}^{2\pi} e^{j\theta'} e^{jk_{spp}\sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{15\pi}{8})\}^2 - 2\rho r_o \sec(\theta' - \frac{15\pi}{8}) \cos(\theta - \theta')}} \right] d\theta' \dots (S6)$$

91 **S5. Generalized equation of electric field for polygonal lens with sides p**
 92 **under linear polarisation (x-P and y-P):**

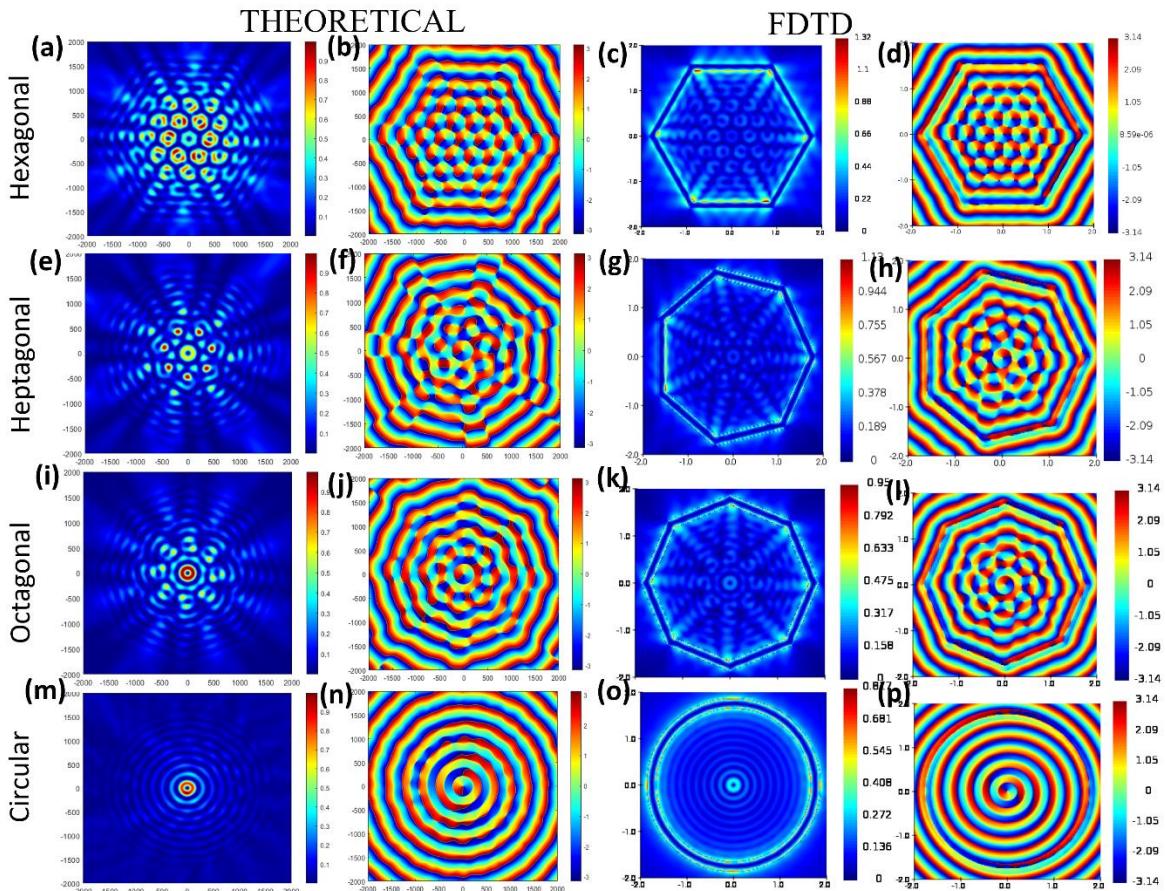
$$93 [E_z(\rho, \theta, z)_{\theta' \in [0, 2\pi]}]_{\text{Polygonal}, xP}$$

$$94 = \sum_{n=1}^p A_o e^{-k_a z} \int_{\frac{2(n-1)\pi}{p}}^{\frac{2n\pi}{p}} \cos \theta e^{jk_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{(2n-1)\pi}{p})\}^2 - 2\rho r_o \sec(\theta' - \frac{(2n-1)\pi}{p}) \cos(\theta - \theta')}} d\theta' \dots (S7)$$

$$95 [E_z(\rho, \theta, z)_{\theta' \in [0, 2\pi]}]_{\text{Polygonal}, yP}$$

$$96 = \sum_{n=1}^p A_o e^{-k_a z} \int_{\frac{2(n-1)\pi}{p}}^{\frac{2n\pi}{p}} \sin \theta e^{jk_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{(2n-1)\pi}{p})\}^2 - 2\rho r_o \sec(\theta' - \frac{(2n-1)\pi}{p}) \cos(\theta - \theta')}} d\theta' \dots (S8)$$

97 **S6. MATLAB and FDTD plots of Electric field and phase of different**
 98 **plasmonic lens structure under LCP:**



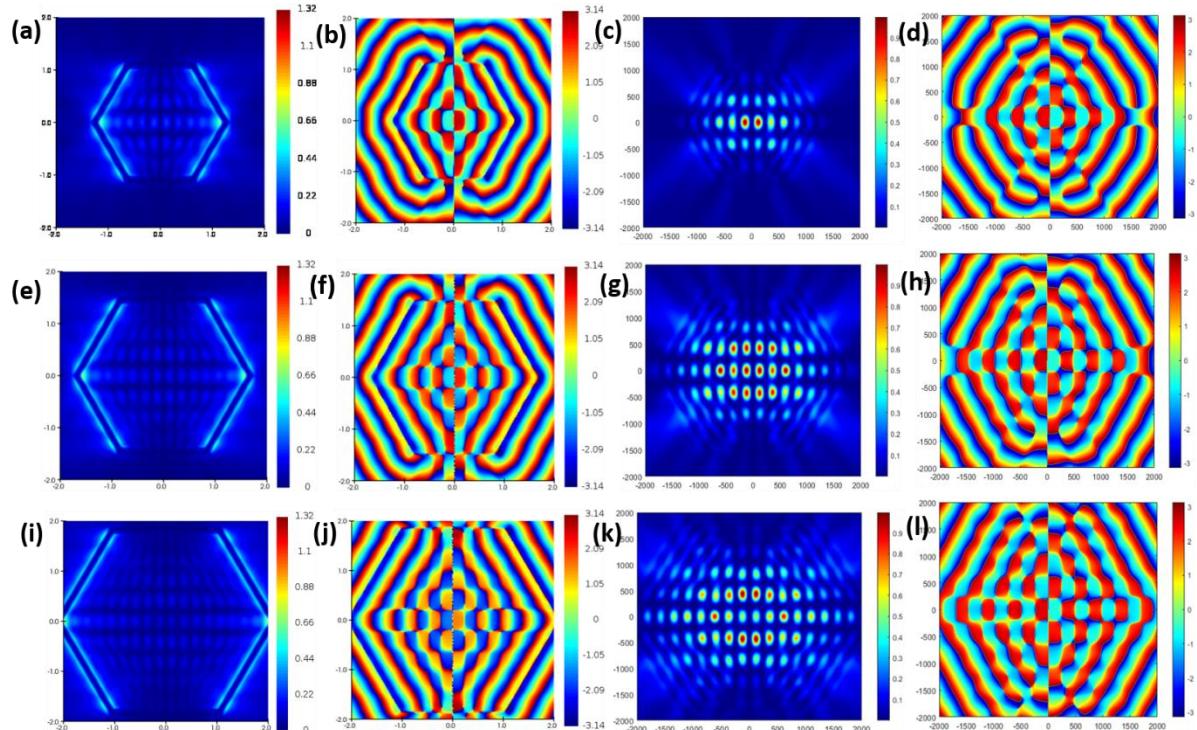
99

100 *Figure S2. MATLAB plots and FDTD simulations of intensity and phase distribution of*
 101 *different lens structure, i.e., hexagonal lens (a, b, c, d), heptagonal lens (e, f, g, h), octagonal*
 102 *lens (i, j, k, l) and circular lens (m, n, o, p) for LCP polarization at 415 nm wavelength.*

103 **S7. Effect of size of lens for linearly polarised illumination in intensity and**
 104 **phase:**

105 In figure S3 and S4, the effect of linearly polarised lights on hexagonal lens has been shown
 106 through FDTD simulations and MATLAB plots. No bright spots have been obtained at the
 107 centre of the hexagonal lens for both x-polarised and y-polarised illuminations. A “scaling

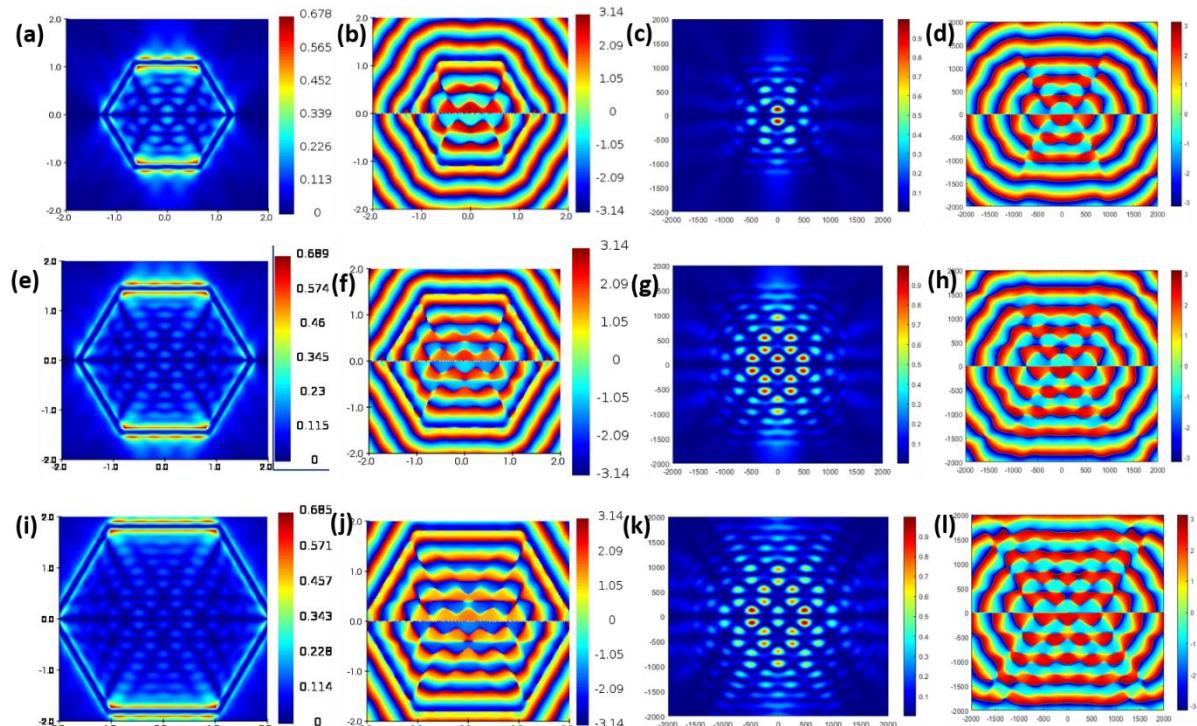
108 behaviour" is also obtained in figure S3 and S4 for both x-polarised and y-polarised light.



109

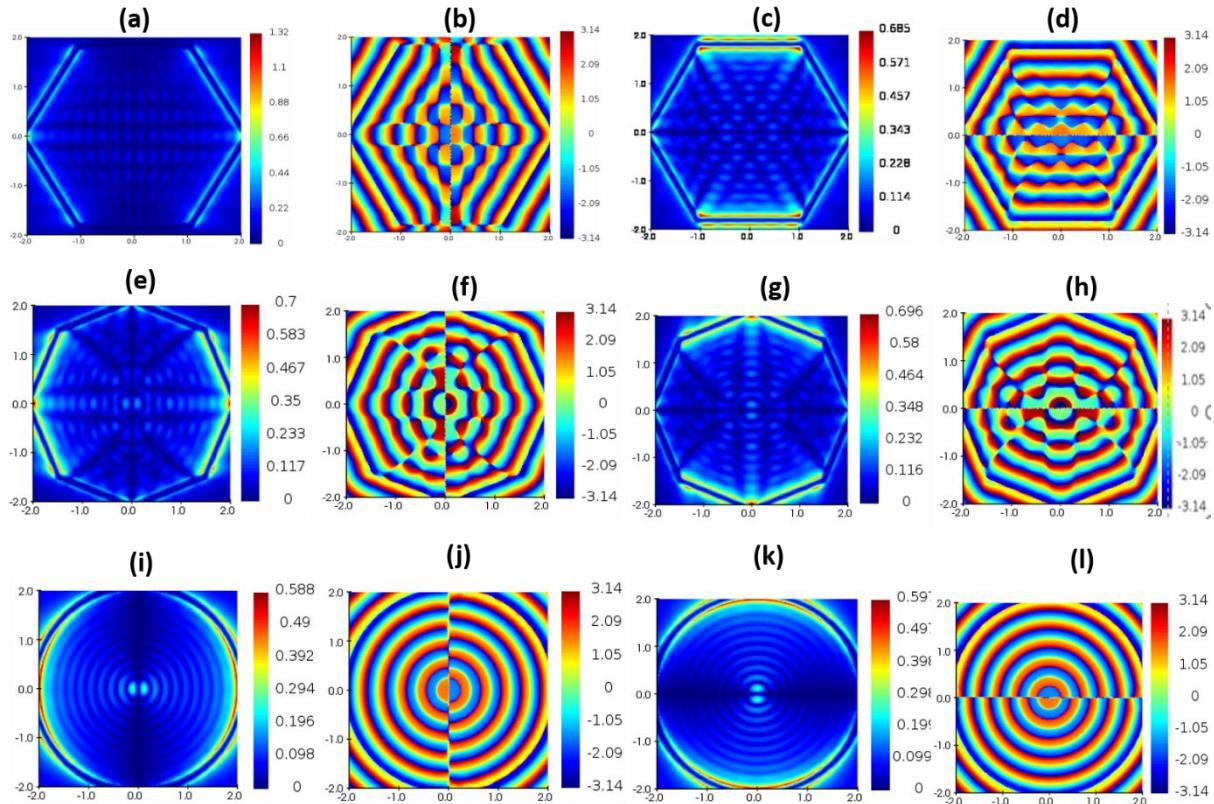
110 *Figure.S3. Intensity and phase distribution of Hexagonal lens in FDTD simulation and in*
111 *MATLAB for $r_0 = 3 \lambda_{spp}$ (a, b, c, d), $4 \lambda_{spp}$ (e, f, g, h) and $5 \lambda_{spp}$ (i, j, k, l) for x-polarized*
112 *illumination.*

113



114

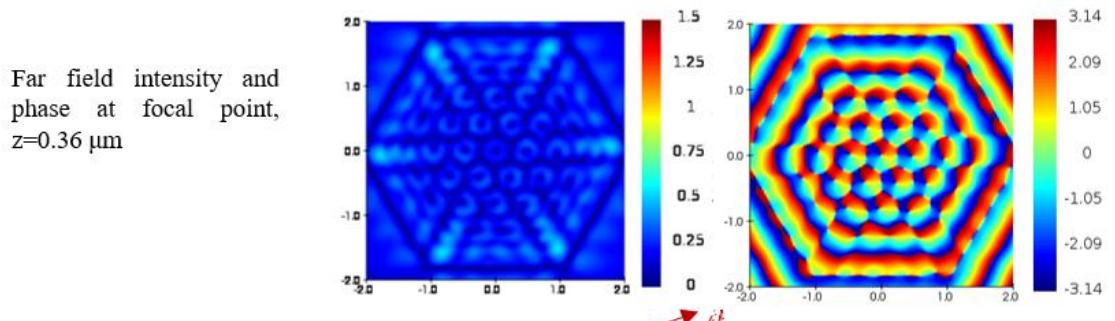
115 *Figure.S4. Intensity and phase distribution of Hexagonal lens in FDTD simulation and in*
 116 *MATLAB for $r_0 = 3 \lambda_{spp}$ (a, b, c, d), $4 \lambda_{spp}$ (e, f, g, h) and $5 \lambda_{spp}$ (i, j, k, l) for y-polarized*
 117 *illumination.*



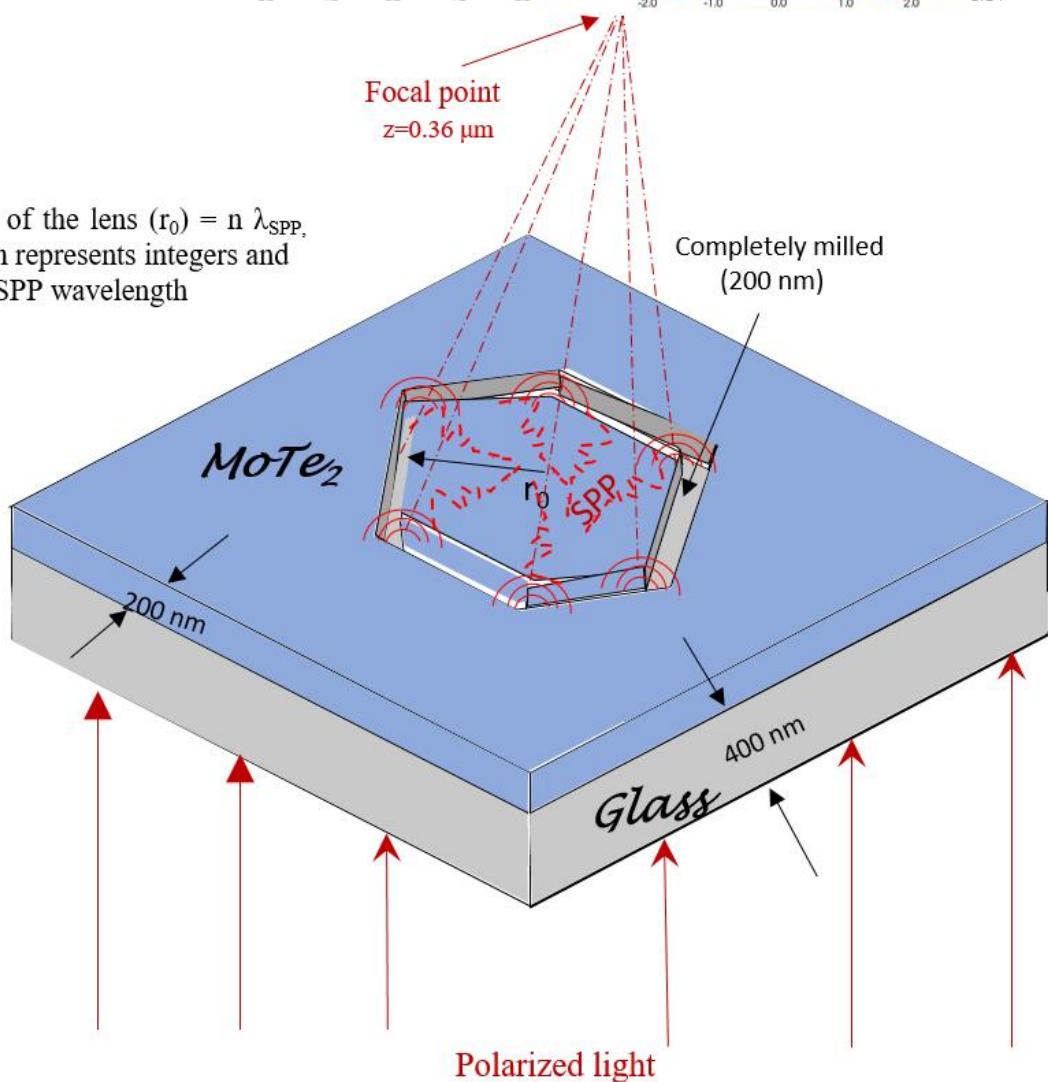
118 *Figure.S5. Intensity and phase distribution of hexagonal lens(a, b, c, d), octagonal lens (e, f,*
 119 *g, h) and circular lens (i, j, k, l) in FDTD simulation for x-polarized(1st 2nd column) and y-*
 120 *polarized (3rd and 4th column) for radius=5 λ_{spp} and illumination wavelength 415 nm in*
 121 *FDTD simulation.*

123 **S8. Design features and far-field plots of hexagonal lens:**

124 Far-field studies and design features of best performing plasmonic lens structure has been
 125 shown in figure S6. Polarized light is being impinged perpendicularly from the below (the
 126 glass side). After generating plasmons in the 2-d surface, the waves get focused at the far-
 127 field at focal point at approximately $0.36 \mu\text{m}$.^{1, 2} The focal point has been determined by far-
 128 field super focusing equations.² The design parameters of hexagonal lens has been shown
 129 schematically in figure S6.



Radius of the lens (r_0) = $n \lambda_{\text{SPP}}$,
where n represents integers and
 λ_{SPP} is SPP wavelength



130

131 *Figure S6: Design features and far field studies of hexagonal plasmonic lens*

132

133 **S9. Investigation of the reasons behind the optical singularities of different**
134 **plasmonic structures and the algorithm behind the MATLAB plots:**

135 The electrical field equation for polygonal lens structure having number of sides p , has been
136 derived in the manuscript, as:

137 $[E_z(\rho, \theta, z)_{\theta' \in [0, 2\pi]}]_{\text{Polygonal, RCP}}$

138 $= \sum_{n=1}^p A_o e^{-k_a z} \int_{\frac{2(n-1)\pi}{p}}^{\frac{2n\pi}{p}} e^{-j\theta'} e^{jk_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{(2n-1)\pi}{p})\}^2 - 2\rho r_o \sec(\theta' - \frac{(2n-1)\pi}{p}) \cos(\theta - \theta')}} d\theta' \dots (S9),$

139 The equation has been written in a more expanded form.

140 $= A_o e^{-k_a z} \left[\int_0^{\frac{2\pi}{p}} e^{-j\left(\theta' - k_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{\pi}{p})\}^2 - 2\rho r_o \sec(\theta' - \frac{\pi}{p}) \cos(\theta - \theta')}\right)} + \right.$

141 $\int_{\frac{2\pi}{p}}^{\frac{4\pi}{p}} e^{-j\left(\theta' - k_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{3\pi}{p})\}^2 - 2\rho r_o \sec(\theta' - \frac{3\pi}{p}) \cos(\theta - \theta')}\right)} +$

142 $\int_{\frac{4\pi}{p}}^{\frac{6\pi}{p}} e^{-j\left(\theta' - k_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{5\pi}{p})\}^2 - 2\rho r_o \sec(\theta' - \frac{5\pi}{p}) \cos(\theta - \theta')}\right)} +$

143 $\dots \dots \dots + \int_{\frac{2(p-1)\pi}{p}}^{2\pi} e^{-j\left(\theta' - k_{spp} \sqrt{\rho^2 + \{r_o \sec(\theta' - \frac{(2p-1)\pi}{p})\}^2 - 2\rho r_o \sec(\theta' - \frac{(2p-1)\pi}{p}) \cos(\theta - \theta')}\right)} \right] d\theta' \dots (S10)$

144 At any certain position inside the lens structure ρ and θ are constant and r_o, p takes a certain
 145 value when the particular lens structure is envisioned. Consequently, it is now obvious that
 146 the value of E_z at a particular point (ρ, θ) is obtained after a single integration by solving
 147 Equation 9 while holding (ρ, θ) constant. We have to conduct this process relentlessly in as
 148 many points as possible in the output monitor range or on to the range we want to investigate
 149 to get a clearer image of intensity map. However, we were unable to discover any analytical
 150 solutions for the definite integral and had to resort to numerical methods, such as, Simpson's
 151 3/8 rule. The plots agree well with the FDTD simulations.

152 $e^{-j(\theta' + f(\theta'))}$ is replaced as $\cos(\theta' + f(\theta')) - j \sin(\theta' + f(\theta'))$ in equation S11 and written
 153 as below:

154 $[E_z(\rho, \theta, z)_{\theta' \in [0, 2\pi]}]_{PolygonaL, RCP} = A_o e^{-k_a z} \left\{ \int_0^{\frac{2\pi}{p}} \cos(\theta' + f_1(\theta')) - j \sin(\theta' + f_1(\theta')) + \right.$

155 $\int_{\frac{2\pi}{p}}^{\frac{4\pi}{p}} \cos(\theta' + f_2(\theta')) - j \sin(\theta' + f_2(\theta')) + \int_{\frac{4\pi}{p}}^{\frac{6\pi}{p}} \cos(\theta' + f_3(\theta')) - j \sin(\theta' + f_3(\theta')) + \dots + \int_{\frac{2(p-1)\pi}{p}}^{\frac{2\pi}{p}} \cos(\theta' + f_p(\theta')) - j \sin(\theta' + f_p(\theta')) \right\} d\theta' \quad (S11)$

157 Let's say after integration, the cosine functions produce the values C_1, C_2, C_3, \dots etc. and the
158 sine functions S_1, S_2 and S_3 for any particular p .

159 According to the definition, in the co-ordinates of optical singularity points, both the real part
160 and imaginary part of the electric field of the wave are zero turning the phase at those
161 singular points undefined. Mathematically it can be expressed as,

162 Phase (Z)_{singularity points} = $\tan^{-1} \left[-\frac{S_1 + S_2 + S_3 + \dots + S_p}{C_1 + C_2 + C_3 + \dots + C_p} \right]$ = undefined.

163 For any structure at ($\rho, \theta = 0$), $S_1 + S_2 + S_3 + \dots + S_p = 0$ and $C_1 + C_2 + C_3 + \dots + C_p = 0$.

164 For hexagonal lens, at ($\rho, \theta = \pm \lambda_{spp}, \pm \frac{\pi}{3}$ and 0) singularity points are obtained for LCP.

165 When the radius of the lens is increased, singularity points are obtained at $\rho = n\lambda_{spp}$. For
166 RCP also, singularities are obtained at only those coordinates only. At those coordinates,
167 electric field at z direction (E_z)=0.

168 For, circular lens, $E_z = 0$ occurs only at $\rho, \theta = 0, 0$.

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172 **References:**

173 S1. J. Miao, Y. Wang, C. Guo, Y. Tian, J. Zhang, Q. Liu, Z. Zhou and H. Misawa, *Plasmonics*, 2012,
174 **7**, 377-381.

175 S2. Y. Liu, H. Xu, F. Stief, N. Zhitenev and M. Yu, *Optics express*, 2011, **19**, 20233-20243.

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