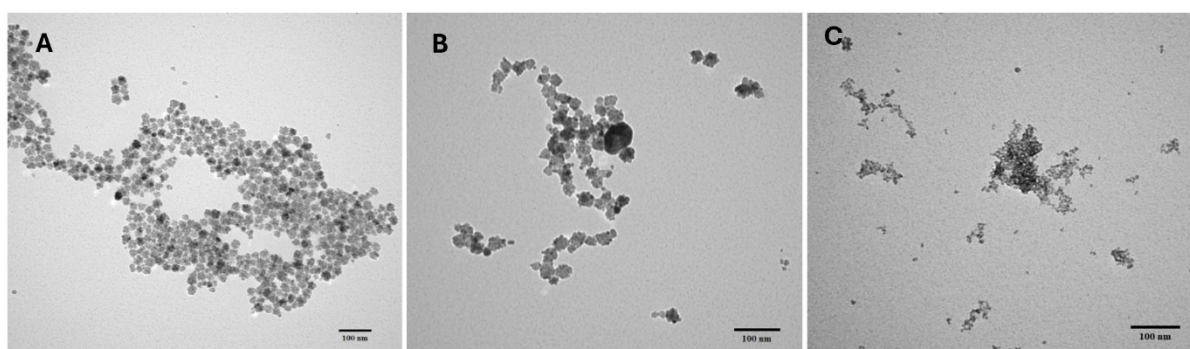


## Supplementary Information

### MPI Performance of Magnetic Nanoparticles Depends on Matrix Composition and Temperature: Implications for in Vivo MPI Signal Amplitude and Spatial Resolution

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#### Transmission electron microscopy of MNPs



**Supplementary Figure 1.** Transmission Electron Microscopy (TEM) images of (A) NF, (B) GIONF, and (C) ferucarbotran MNP formulations used in this study. Scale bars represent 100 nm.

#### Physicomagnetic properties of MNPs

**Supplementary Table 1.** Physicomagnetic characterization of NF, GIONF, and ferucarbotran.

MNP	Core size (nm) from TEM	Hydrodynamic size (nm) from DLS	Saturation magnetization $M_s$ (emu.g <sup>-1</sup> ) *	Susceptibility $\chi$ *
NF	43.9	177±64	69	128
GIONF	50	160±76	69	128
Ferucarbotran	14.2	69±29	96	0.135

\*Extracted from references [1-3].

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## MNP signal amplitude and FWHM values of MNPs

**Supplementary Table 2.** Signal amplitude and FWHM values for different MNPs in water (0% gelatin or 0% BSA).

MNP	Concentration (µg/mL)	Quantity (µg)	Signal amplitude (a.u.)	SD	FWHM (mT)	SD
NF	25	12.5	1.28	0.29	12	0.1
	50	25	2.8	0.27	11	0.3
	100	50	4.33	0.59	12	1.5
GIONF	25	12.5	1.42	0.01	12	0.04
	50	25	2.74	0.01	12	0.1
	100	50	4.4	0.02	14	0.1
Ferucarbotran	25	12.5	0.68	0.01	11	0.1
	50	25	1.26	0.04	11	1.3
	100	50	2.74	0.03	12	0.03
GIONF*	50	5	0.51	0.02	10	0.2
Ferucarbotran*	100	10	0.62	0.02	13	0.4

\*Baseline measurements in water (0% BSA content).

### Compressibility error calculations

When a “quantity” depends on measured variables, the uncertainty (standard deviation) in the quantity can be estimated by considering how sensitive the quantity is to changes in those variables, and then combining the uncertainties in the variables [4, 5].

### Compressibility formula

The compressibility  $\beta_s$  is given by:

$$\beta_s = \frac{1}{C^2 \times \rho} \quad (1)$$

Where C is the velocity and  $\rho$  is the density.

### Error propagation

For a function  $\beta_s(C, \rho)$ , the uncertainty in  $\beta_s$  due to uncertainties in C and  $\rho$  can be estimated using the partial derivatives with respect to each variable:

$$\sigma_{\beta_s}^2 = \left(\frac{\partial \beta_s}{\partial C}\right)^2 \sigma_C^2 + \left(\frac{\partial \beta_s}{\partial \rho}\right)^2 \sigma_\rho^2 \quad (2)$$

where  $\sigma_C$  is the standard deviation in velocity and  $\sigma_\rho$  is the standard deviation in density.

### Partial derivatives

1. The partial derivative with respect to C is:

$$\frac{\partial \beta_s}{\partial C} = \frac{\partial}{\partial C} \left( \frac{1}{C^2 \times \rho} \right) = -\frac{2}{C^3 \times \rho} \quad (3)$$

2. The partial derivative with respect to  $\rho$  is:

$$\frac{\partial \beta_s}{\partial \rho} = \frac{\partial}{\partial \rho} \left( \frac{1}{C^2 \times \rho} \right) = -\frac{1}{C^2 \times \rho^2}, \quad \frac{\partial \beta_s}{\partial \rho} = \frac{\partial}{\partial \rho} \left( \frac{1}{C^2 \times \rho} \right) = -\frac{1}{C^2 \times \rho^2} \quad (4)$$

### Simplifying for dominant contribution:

Given the typical situation where the uncertainty in velocity  $\sigma_c$  is much more significant than the uncertainty in density  $\sigma_\rho$ , the term involving  $\sigma_\rho$  is often negligible. Hence, the primary contribution to  $\sigma_{\beta_s}$  comes from the uncertainty in C.

Thus, we approximate:

$$\sigma_{\beta_s} \approx \left| \frac{\partial \beta_s}{\partial C} \right| \sigma_c = \left| \frac{-2}{C^3 \times \rho} \right| \sigma_c = \frac{2 \times \sigma_c}{C^3 \times \rho} \quad (5)$$

### Final formula

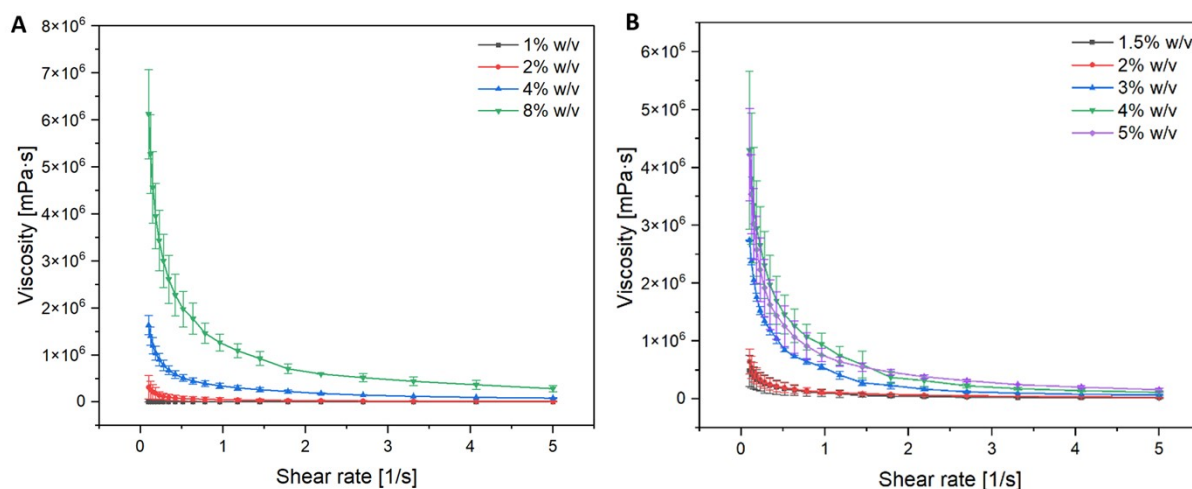
The formula used for the standard deviation of compressibility is:

$$\sigma_{\beta_s} = \frac{2 \times \sigma_c}{C^3 \times \rho} \quad (6)$$

This formula allows an estimation of how the uncertainty in the velocity  $\sigma_c$  propagates into uncertainty in the calculated compressibility  $\beta_s$ . In here, C is the average measured velocity and  $\sigma_c$  is the standard deviation of these velocity measurements, reflecting the variability or uncertainty in the velocity data.

When measuring the velocity multiple times, the average velocity C and the spread of those measurements around the average can be calculated, yielding the standard deviation  $\sigma_c$ . This standard deviation quantifies how much the individual velocity measurements differ from the average value. In the error propagation formula for compressibility  $\beta_s$ ,  $\sigma_c$  was used to estimate how the uncertainty in the velocity measurements affects the uncertainty in the calculated compressibility.

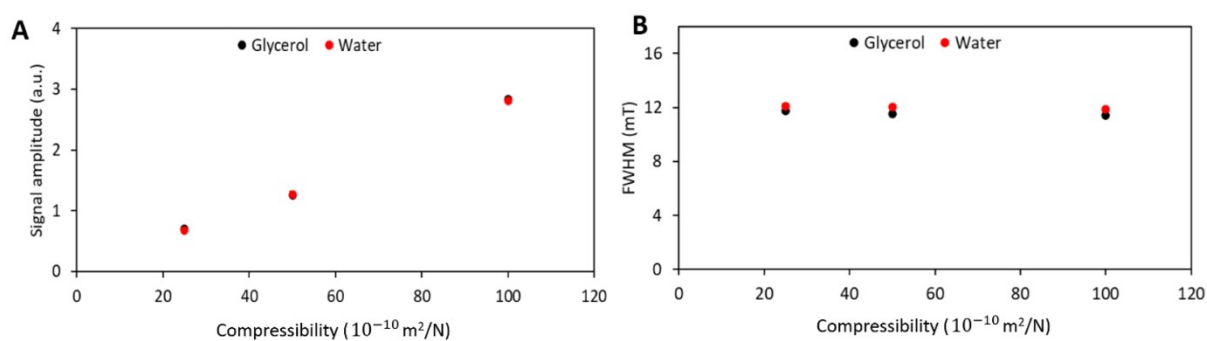
## Viscosity measurements of gelatin and BSA



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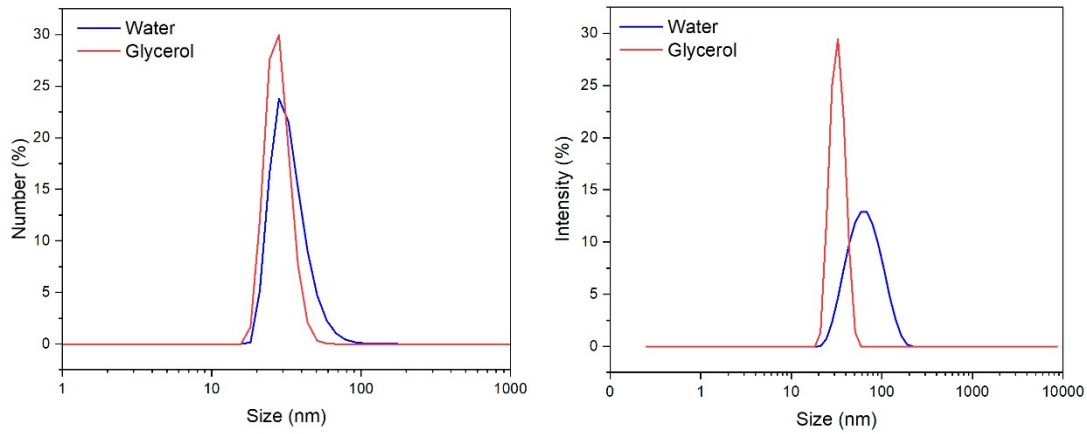
**entary Figure 2.** Viscosity measurements of (A) gelatin and (B) BSA hydrogel samples at various concentrations. Both sets of hydrogel samples exhibit shear-thinning behavior, where viscosity decreases as the shear rate increases. Error bars represent standard deviations across triplicate measurements.

MPI  
signal  
amplitude  
measurements  
of  
ferucarbotran  
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glycerol



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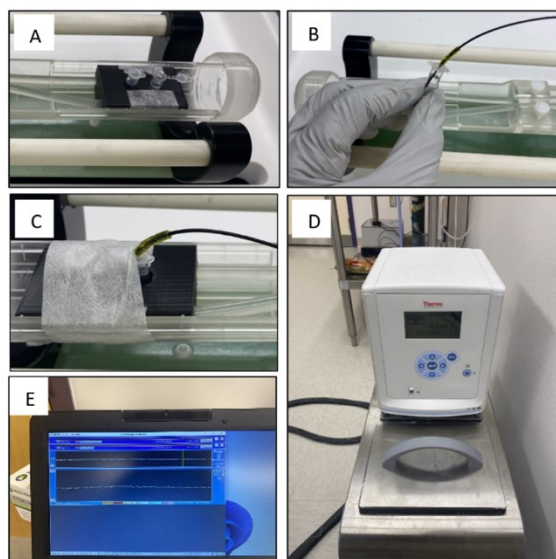
**Supplementary Figure 3.** (A) MPI signal amplitude and (B) FWHM values for ferucarbotran at different concentrations (25, 50, and 100 µg/mL) in glycerol and water. Data were obtained at room temperature and are shown as mean ± SD for three independent experiments.



### Hydrodynamic size of ferucarbotran in glycerol and water

**A****B**

**Supplementary Figure 4.** Number-based (A) and intensity-based (B) hydrodynamic size distribution of ferucarbotran in glycerol and water.



**Supplementary Figure 5.** Experimental setup for measurement of the MPI signal amplitudes of ferucarbotran (100  $\mu\text{g Fe/mL}$ ) at different temperatures (10-55  $^{\circ}\text{C}$ ). **(A)** Holder containing ferucarbotran and water vials, allowing water to flow in and out to regulate temperature. **(B)** A thermocouple thermometer inserted into the water vial to monitor the temperature of ferucarbotran indirectly. **(C)** Vials are secured in the holder for stable temperature control. **(D)** Water pump used to circulate water at different temperatures for precise regulation of the experimental conditions. **(E)** Real-time temperature monitoring display provides continuous tracking of temperature changes over time.

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