

*Supporting Information*

**Efficient elimination of Hg(II) from water bodies with acid-modified magnetic biomass spent tea leaves: Conditional optimization and application**

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## 1. Materials and instruments

Sodium hydroxide (NaOH, AR, 96%), nickel chloride ( $\text{NiCl}_2 \cdot 6\text{H}_2\text{O}$ , AR, 99%), ferric chloride ( $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ , AR, 99%), ammonia (25 – 28 wt.%), potassium chloride (KCl, AR, 99.5%) and humic acid (FA  $\geq$  90%) were purchased from Macleans (Shanghai, China). Hydrochloric acid (HCl, AR, 37%) and nitric acid ( $\text{HNO}_3$ , AR, 68%) were purchased from Shanghai Lianshi Chemical Reagent co., LTD., (Shanghai, China). Sodium sulfate (AR,  $\geq$  99%), urea (AR, 99%), mercury chloride (AR, 99%) and sodium chloride (AR,  $\geq$  99.5%) were purchased from Sinopharm Chemical Reagent Co., Ltd., (Beijing, China). All of the chemicals are analytical reagent.

Digital display mechanical mixer (OS20-S) and Thermostat Magnetic stirrer (MS-H-Pr) were purchased from Dragon (Shanghai, China). Muffle burner was purchased from Kejing (KSL-1400X-A2, Heifei, China). Cold atomic absorption mercury meter was purchased from Huaguang (F732-VJ, Shanghai, China). Constant temperature drying box was purchased from Jinghong (DHG-9076A, Shanghai, China). Constant temperature water bath rocking bed was purchased from Zhicheng (ZWY-110X30/50, Shanghai, China). Water Purifier (ZRXQ015TQ) was purchased from Milli-Q (USA). Electronic balance was purchased from Sartorius (MSE524S-100-DA, Germany).

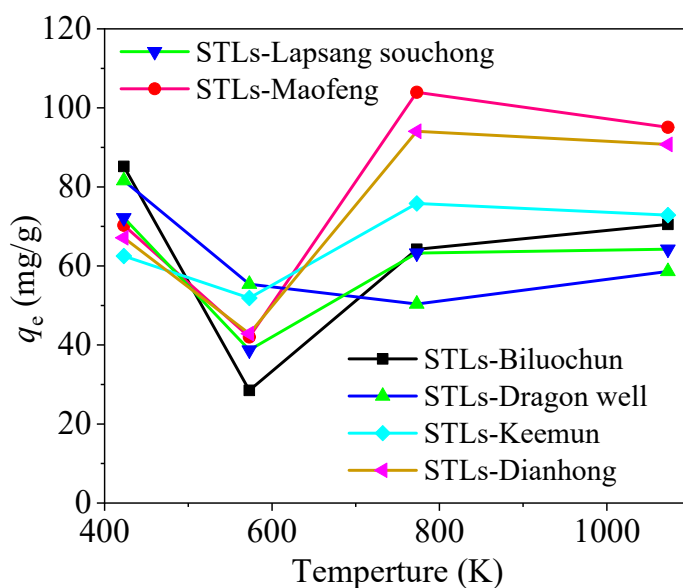
## 2. Samples characterizations

The morphology and structure character of prepared adsorbent  $\text{NiFe}_2\text{O}_4/\text{STLS}$  were characterized through Scanning Electron Microscope (SEM, Quanta FEG250, FEI, USA), X-ray diffractometer (XRD, Rigaku Ultimate IV, Japan), Fourier Transform Infrared (FT-

IR, Nicolet iN10, Thermo Scientific, USA). The Brunauer-Emmett-Teller (BET) specific surface area was conducted by automatic specific surface and porosity analyzer (BET, ASAP 2020, Micromeritics, USA), and the pore size distribution was determined by desorption isotherm via the Barret-Joyner-Halender (BJH) method.

The X-ray photoelectron spectroscopy (XPS) was used to detect the surface composition, the valence state information and superficial chemical bond state of prepared samples, which was conducted on an X-ray Photoelectron Spectroscopy (XPS, K-Alpha, Thermo Scientific, USA). The magnetic strength of NiFe<sub>2</sub>O<sub>4</sub>/STLS was measured by a Vibrating Sample Magnetometer (VSM, Qunantumpesign, MPMS3, USA). The property of charges on the NiFe<sub>2</sub>O<sub>4</sub>/STLS was determined via a Zeta potentiometer (Zeta PALS, Brookhaven, USA). The Material quality change data was obtained using thermogravimetric analysis (TGA, NETZSCH STA 449F3, Germany)

### 3. Influence of pyrolysis temperature



**Fig. S1.** Influence of pyrolysis temperature.

#### 4. Preparation schematic of NiFe<sub>2</sub>O<sub>4</sub>/STLs

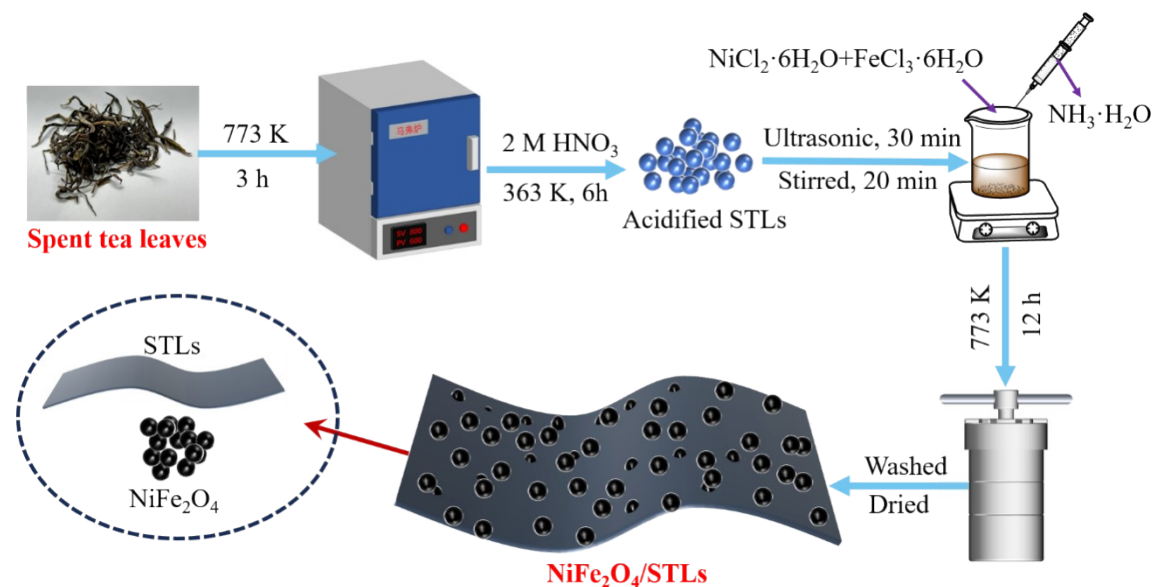


Fig. S2. Schematic diagram of NiFe<sub>2</sub>O<sub>4</sub>/STLs preparation.

#### 5. BET

Fig. S3 is the distributions of adsorption-desorption and pore size of STLs and NiFe<sub>2</sub>O<sub>4</sub>/STLs, and the corresponding data is presented in Table S1.

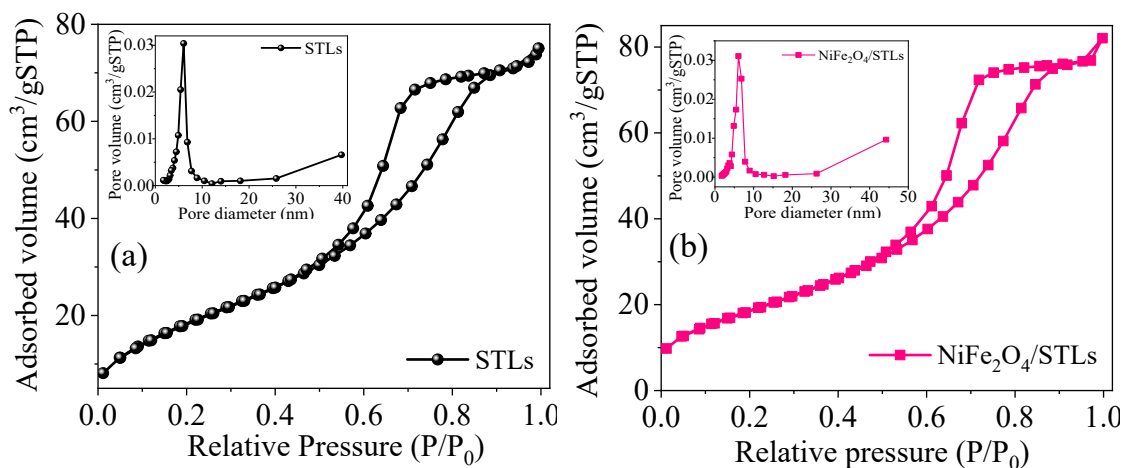


Fig. S3. Isotherm plots and pore size distribution of STLs (a), NiFe<sub>2</sub>O<sub>4</sub>/STLs (b).

From Fig. S3a, there is almost no pore on the STLs surface, but after acid modification and co-precipitation with magnetic nanoparticles of NiFe<sub>2</sub>O<sub>4</sub>, the adsorption capacity towards N<sub>2</sub> over STLs is greatly increased (Fig. S3b), which is in accord

with the change of the isothermal data in Table S1. After acid modification and loading with magnetic nanoparticles, the isothermal data of STLs material, including pore volume and pore size, are greatly enlarged, which is conducive to the promotion of adsorption capacity towards Hg(II).

In addition, the adsorption-desorption curve of NiFe<sub>2</sub>O<sub>4</sub>/STLs is a typical type-IV isotherm. The curve rises upward in low P/P<sub>0</sub> region and the adsorption of N<sub>2</sub> begins to increase rapidly. In the high P/P<sub>0</sub> region, capillary condensation occurs in NiFe<sub>2</sub>O<sub>4</sub>/STLs material, leading to an obvious H3 type hysteresis loop[1, 2]. It can be further speculated that there are certain mesoporous in NiFe<sub>2</sub>O<sub>4</sub>/STLs material, which is consistent with the results of its particle size distribution map shown in Fig. S3a and S3b (the inserted picture). The pore size of NiFe<sub>2</sub>O<sub>4</sub>/STLs is relatively small, mostly distributed between 3 - 8 nm, and essentially the same as STLs. Hence, the as-prepared NiFe<sub>2</sub>O<sub>4</sub>/STLs belongs to magnetic mesoporous composite material.

After recombination with magnetic particles NiFe<sub>2</sub>O<sub>4</sub>, the surface of STLs is covered by magnetic nanoparticles, resulting in a relative reduction in the specific surface area and an increase in total pore capacity.

**Table S1. Isothermal data of STLs and NiFe<sub>2</sub>O<sub>4</sub>/STLs.**

Samples	BET (m <sup>2</sup> /g)	Pore volume (cm <sup>3</sup> /g)	Pore size (nm)
STLs	71.87	0.116	6.461
NiFe <sub>2</sub> O <sub>4</sub> /STLs	68.28	0.127	7.437

## 6. RSM optimization results

**Table S2.** RSM optimization results of NiFe<sub>2</sub>O<sub>4</sub>/STLs.

Std.	Runs	Variables				$q_e$ (mg/g)
		pH (A)	$C_0$ (B)	$T$ (C)	Dosage (D)	
24	1	8	20	30	0.09	182.94
22	2	8	40	30	0.09	204.1
20	3	7	10	35	0.1	152.6
3	4	6	40	40	0.09	140.4
2	5	6	40	30	0.09	173.2
14	6	7	30	35	0.1	196
11	7	7	50	35	0.1	178.9
30	8	9	30	35	0.1	164.6
17	9	7	30	35	0.1	195
18	10	7	30	35	0.1	190
21	11	7	30	35	0.12	160.26
15	12	7	30	35	0.1	191
28	13	8	20	30	0.11	181.4
12	14	7	30	25	0.1	171.2
16	15	7	30	35	0.1	194
6	16	6	40	30	0.11	167.6
1	17	5	30	35	0.1	119.8
19	18	7	30	45	0.1	136.5

Std.	Runs	Variables				$q_e$ (mg/g)
		pH (A)	$C_0$ (B)	$T$ (C)	Dosage (D)	
8	19	6	20	30	0.11	159.2
29	20	8	20	40	0.11	152.74
26	21	8	40	30	0.11	187.4
5	22	6	20	40	0.09	119.34
23	23	8	40	40	0.09	169
4	24	6	20	30	0.09	148
10	25	7	30	35	0.08	171.6
25	26	8	20	40	0.09	147.96
7	27	6	40	40	0.11	136
13	28	7	30	35	0.1	199
27	29	8	40	40	0.11	155.42
9	30	6	20	40	0.11	136.76

Table S3. Calculated results of four models.

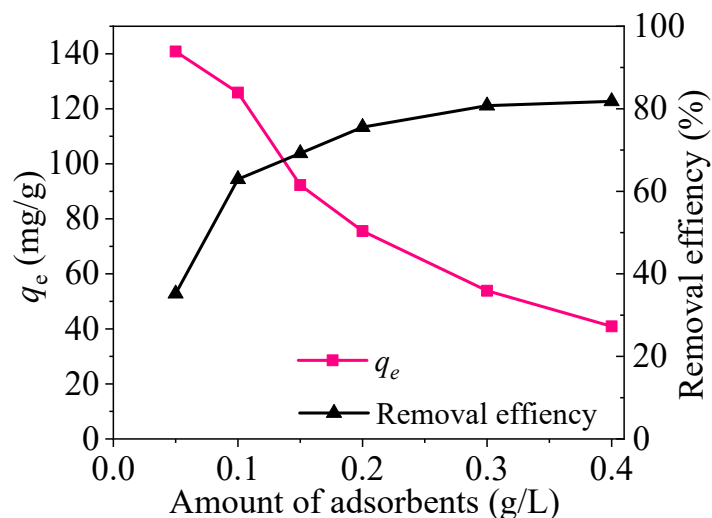
Models	Std. Dev	$R^2$	Adjusted $R^2$	Predicted $R^2$	Press.	
Linear	17.43	0.5346	0.4602	0.4174	9512.3	
2FI	19.32	0.5656	0.3370	0.3013	11407.82	
Quadratic	5.16	0.9756	0.9528	0.9239	2059.52	Suggested
Cubic	3.93	0.9934	0.9728	0.5240	7771.65	

Table S4. ANOVA analysis of Quadratic model.

Source	Sum of Squares	df	Mean square	F-value	P-value	
Model	15928.20	14	1137.73	240.89	<0.0001	Significant
A-pH	3505.62	1	3505.62	131.90	<0.0001	
B-C0	4150.67	1	4150.67	156.17	<0.0001	
C-T	1032.02	1	1032.02	99.21	<0.0001	
D-Dosage	40.30	1	40.30	1.52	0.2371	
AB	14.48	1	14.48	0.5447	<0.0001	
AC	0.57	1	0.57	0.0214	<0.0001	
AD	130.3	1	130.3	4.9	<0.0001	
BC	17.51	1	17.51	0.659	<0.0001	
BD	17.77	1	17.77	0.6684	<0.0001	
CD	325.26	1	325.26	12.24	0.0032	
A <sup>2</sup>	4261.89	1	4261.89	160.35	<0.0001	
B <sup>2</sup>	2502.97	1	2502.97	94.17	<0.0001	
C <sup>2</sup>	1186.73	1	1186.73	44.65	<0.0001	
D <sup>2</sup>	1170.55	1	1170.55	44.04	<0.0001	
Residual	398.68	15	26.58			
Lack of Fit	343.85	10	34.38	3.14	0.1095	Insignificant
Pure Error	54.83	5	10.97			
Cor Total	16326.88	29				



## 7. Effect of adsorbent dosage



**Fig. S4.** Effect of dosage on Hg(II) removal. Conditions: dosage = 0.05 – 0.4 g/L,  $C_0 = 20$  mg/L,  $T = 298$  K, reaction time  $t = 24$  h, solution volume  $V = 100$  mL,  $\text{pH} = 8$ .

From Fig. S4, the increase of adsorbent dosage can significantly improve the removal rate of Hg(II). With the addition of dosage rising from 0.05 g/L to 0.4 g/L, the Hg(II) removal rate increases from 22.5% to 85.8%. However, the adsorption capacity of NiFe<sub>2</sub>O<sub>4</sub>/STLS towards Hg(II) decreases from 140.85 mg/g to 40.91 mg/g. It indicates that as the NiFe<sub>2</sub>O<sub>4</sub>/STLS dosage increases, although the overall adsorption active sites increase and more effectively removal of Hg(II) has been achieved, the adsorption saturation occurs and active sites are gradually occupied. Meanwhile, condensation occurs on the adsorbent surface. Hence, under the high dosage, the mercury removal rate has instead decreased.

Considering the adsorption amount and adsorption efficiency of NiFe<sub>2</sub>O<sub>4</sub>/STLS towards Hg(II), the dosage of 0.1 g/L was selected as the optimal adsorbent amount of the subsequent experiments.

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**Table S5.** Comparison of adsorption capacity of Hg(II) with reported adsorbents.

Adsorbents	BET (m <sup>2</sup> /g)	pH	T (°C)	Kinetic fitting models	Isotherm fitting models	Thermodynamics	Q <sub>m</sub> (mg/g)	Ref.
MWCNTs-COOH	97	7.8	25	Pseudo-first-order	Langmuir	$\Delta H^0 > 0$ , $\Delta G^0 < 0$	91.74	[3]
Biochar with 3-MPTS	—	7	—	Pseudo-second-order	Langmuir	—	126.62	[4]
MNP-CD-PBTCA	13.84	4	55	Pseudo-second-order	Langmuir	$\Delta H^0 > 0$ , $\Delta G^0 < 0$	77.59	[5]
CoFe <sub>2</sub> O <sub>4</sub> @mSiO <sub>2</sub> -NH <sub>2</sub>	17.08	7	25	Pseudo-second-order	Langmuir	$\Delta H^0 < 0$ , $\Delta G^0 < 0$	149.3	[6]
Ball-milled biochar 700	296.3	5	45	Intra-particle diffusion	Langmuir	$\Delta H^0 > 0$ , $\Delta G^0 < 0$	127.4	[7]
E-ZFA-Ag	128.7	2.5	2.5	-	Langmuir	—	107.4	[8]
Humic acid/biochar	2.85	—	55	Pseudo-second-order	Freundlich	—	38.33	[9]
Boehmite@Fe <sub>3</sub> O <sub>4</sub> @PLA@SiO <sub>2</sub>	—	7	25	Pseudo-second-order	Langmuir	—	36.94	[10]
Elatin@SiO <sub>2</sub>	675.92	6	40	Pseudo-second-order	Langmuir	$\Delta H^0 > 0$ , $\Delta G^0 < 0$	43.85	[11]
CNFs/GO/Fe <sub>3</sub> O <sub>4</sub>	55	7	25	Pseudo-second-order	Langmuir	—	36.70	[12]
NiFe <sub>2</sub> O <sub>4</sub> /STLS	68.28	8	39	Pseudo-second-order	RSM	$\Delta H^0 < 0$ , $\Delta G^0 < 0$	204.42	This work
NiFe <sub>2</sub> O <sub>4</sub> /STLS	68.28	8	35	Pseudo-second-order	Langmuir	$\Delta H^0 < 0$ , $\Delta G^0 < 0$	189.64	This work

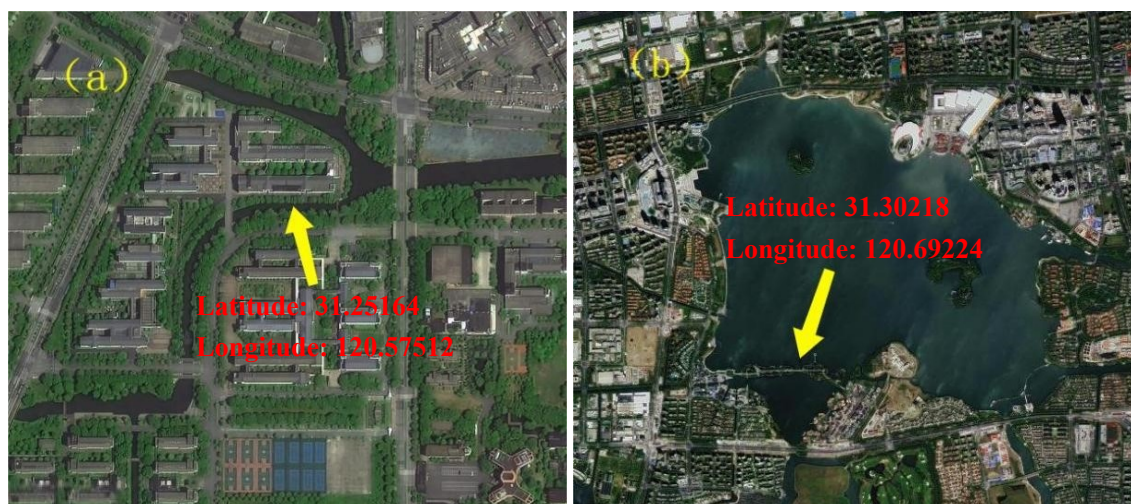
### 3 8. Water quality parameters of actual water samples

4 **Table S6.** Water quality of Biyu river, lake water and effluent of sewage treatment plant.

Water quality	Biyu river	Lake water	Effluent of sewage treatment plant
COD <sub>Mn</sub> (mg/L)	20.91	19.45	24.51
BOD <sub>5</sub> (mg/L)	2.03	2.49	3.02
TN (mg/L)	4.12	5.35	6.38
TP (mg/L)	0.21	0.11	0.15
TOC (mg/L)	4.01	3.31	2.45
Ammonia nitrogen (mg/L)	0.71	0.82	0.64
pH	7.16	7.63	7.45
Conductivity (μS/cm)	420.12	460.05	680.26

5

6

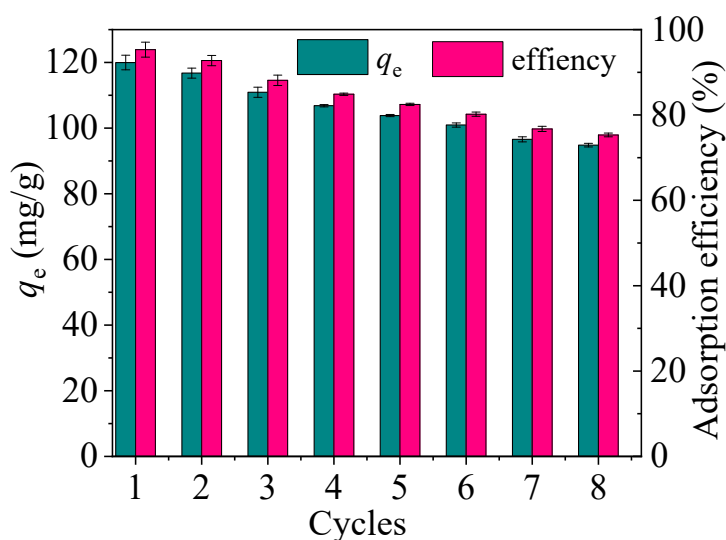


**Fig. S5.** Sample location of Biyu river (a) and lake water in Suzhou city (b).

## 11 9. Regeneration

12 To test the potential of composite material NiFe<sub>2</sub>O<sub>4</sub>/STLS in practical application, 0.1  
13 mol/L HCl was used as the regenerative agent. The spent material of 0.2 g/L was placed  
14 in the above acidic environment for 4 h with ultrasonic vibration at 298 K, then was  
15 separated by external magnetic field, washed with pure water and dried. The treated  
16 regenerative adsorbent was reused for the next mercury adsorption, and the process was  
17 repeated a certain time to evaluate the regenerative performance of composite adsorbent  
18 NiFe<sub>2</sub>O<sub>4</sub>/STLS.

19 As shown in Fig. S6, the adsorption capacity of NiFe<sub>2</sub>O<sub>4</sub>/STLS towards Hg(II)  
20 achieves 103.82 mg/g after five adsorption-desorption cycles. Accordingly, the adsorption  
21 capacity decreases by only 13.5%. After 8 cycles, the adsorption capacity towards Hg(II)  
22 still obtains 94.81 mg/g. The results indicate that the prepared adsorbent has good  
23 recyclability.



24  
25 **Fig. S6.** Regeneration cycles of NiFe<sub>2</sub>O<sub>4</sub>/STLS.  
26  
27

## 28 10. Models of adsorption kinetics

29 Pseudo-first-order model:

$$30 \quad \ln(q_e - q_t) = \ln q_e - K_1 t \quad (S1)$$

31 If  $\log(q_e - q_t)$  is plotted against  $t$  and a straight line is obtained, the adsorption  
32 conforms to the pseudo-first-order model. In many cases, the pseudo-first-order model is  
33 not consistent with the experimental data for the whole adsorption time and is only  
34 suitable for the initial stage of the adsorption process.

35 Pseudo-second-order model:

$$36 \quad \frac{t}{q_t} = \frac{1}{K_2 q_e^2} + \frac{t}{q_e} \quad (S2)$$

37 If  $t/q_t$  is plotted against  $t$  to obtain a straight line, the adsorption process conforms to  
38 the pseudo-second-order model. The larger the value of  $q_e$  and  $K_2$ , the faster the  
39 adsorption rate, and the adsorption is easy to reach equilibrium.

40 Intra-particle diffusion model:

$$41 \quad q_t = K_d t^{1/2} + C \quad (S3)$$

42 The slope of the straight part is the diffusion rate constant  $K_d$ . The intercept can  
43 represent the boundary layer thickness, that is, the larger the intercept, the thicker the  
44 boundary layer.

45 Elovich model:

$$46 \quad q_t = \frac{1}{\beta} \ln(\alpha\beta) + \frac{1}{\beta} \ln t \quad (S4)$$

47 Elovich equation can be applied to the process where the activation energy varies  
48 greatly during the reaction.

49 Two constant equation:

$$50 \quad \ln q_t = \ln A + B \ln t \quad (S5)$$

51 The Two constant equation, also known as Freundlich modified formula, can  
52 describe the heterogeneity of the energy distribution on the adsorbent surface, and is also  
53 suitable for the more complex kinetic equation of the reaction process.

54 here,  $q_e$  (mg/g) is the equilibrium adsorption capacity;  $q_t$  (mg/g) is the adsorption  
55 capacity at time  $t$  (min);  $k_1$  ( $\text{min}^{-1}$ ),  $k_2$  ( $\text{mg}/(\text{g}\cdot\text{min})$ ) and  $k_d$  ( $\text{mg}/(\text{g}\cdot\text{min}^{0.5})$ ) are the rate  
56 constants of the pseudo-first order, the pseudo-second order and intra-particle diffusion  
57 model, respectively;  $\alpha$  ( $\text{mmol}/\text{g}\cdot\text{min}^{-1}$ ) and  $\beta$  ( $\text{g}/\text{mmol}$ ) are the constants of Elovich,  
58 representing the initial adsorption rate constant and desorption rate constant, respectively;  
59  $A$  and  $B$  are rate constants and  $C$  (mg/g) is the boundary layer thickness.

## 60 11. Models of adsorption isotherms

61 The Langmuir model is suitable for monolayer adsorption of homogeneous surface  
62 sites. The Freundlich model is suitable for multilayer adsorption on heterogeneous  
63 surfaces. The Temkin model considers the interaction between adsorbent and adsorbent.  
64 The Dubinin-Radushkevich (D-R) model is used to determine whether the adsorption  
65 property is physical or chemical adsorption.

66 Langmuir model:

$$67 \quad \frac{C_e}{q_e} = \frac{C_e}{q_m} + \frac{1}{q_m K_L} \quad (S6)$$

$$68 \quad R_L = (1 + K_L C_0)^{-1} \quad (S7)$$

69 The  $R_L$  value can be used to indicate whether the isotherm is of favorable ( $0 < R_L <$

70 1), linear ( $R_L = 1$ ), unfavorable ( $R_L > 1$ ), or irreversible form ( $R_L = 0$ ).

71 Freundlich model:

$$72 \quad q_e = K_F C_e^{\frac{1}{n}} \quad (S8)$$

73  $1/n$  is a heterogeneous factor characterizing the adsorption capacity and strength.

74 When the value of  $1/n$  is between 0 and 1, it indicates that the adsorption is feasible and

75 easy. When  $1/n = 1$ , the adsorption is linear, indicating that there is no interaction between

76 adsorbent and adsorbent. When the value is greater than 1, the adsorption is negative and

77 the adsorption is very difficult.

78 Temkin model:

79

$$80 \quad q_e = \frac{RT}{b_T} \ln(k_T C_e) \quad (S8)$$

81 D-R model:

$$82 \quad q_e = q_m e^{-\beta \varepsilon^2} \quad (S9)$$

$$83 \quad E = \frac{1}{\sqrt{2\beta}} \quad (S10)$$

84 Hill model:

$$85 \quad E = \frac{q_{SH} \times C_e \times n_H}{k_D + C_e \times n_H} \quad (S11)$$

86 When the  $E$  value is in the range of 8 to 16  $\text{kJ}\cdot\text{mol}^{-1}$ , the adsorption is chemisorption.

87 Less than 8  $\text{kJ}\cdot\text{mol}^{-1}$  was considered as physical adsorption.

88 Where  $q_e$  and  $q_m$  (mg/g) are the equilibrium and the maximum adsorption amount,

89 respectively;  $K_L$ ,  $K_F$ , and  $K_T$  represent the Langmuir, Freundlich and Temkin constants,

90 which are related to the adsorption energy and adsorption capacity;  $C_e$  (mg/g) denotes the  
91 equilibrium concentration;  $n$  is the parameter of the Freundlich model and depended on  
92 temperature, which relates to the adsorption performance of the adsorbent;  $R$  (8.314  
93  $\text{J}\cdot\text{mol}^{-1}\text{K}^{-1}$ ) is the gas constant;  $T$  is the Kelvin temperature (K);  $\beta$  ( $\text{mol}^2\cdot\text{J}^{-2}$ ) is a constant  
94 related to the mean energy of adsorption;  $\varepsilon$  ( $\text{kJ}^2\cdot\text{mol}^{-2}$ ) is the Polanyi potential, which can  
95 be obtained from  $\varepsilon = RT \ln(1+1/C_e)$ ;  $E$  ( $\text{kJ}\cdot\text{mol}^{-1}$ ) is the mean free energy and  $b_T$  (KJ/mL)  
96 is the Temkin constant.  $q_{\text{SH}}$  is the Hill isotherm maximum uptake saturation (mg/L).  $k_D$  is  
97 the Hill constant and  $n_H$  is the Hill cooperativity coefficient of the binding interaction.

## 98 12. Models of adsorption thermodynamics

99 Thermodynamics parameters such as the Gibbs free energy change ( $\Delta G^0$ ), entropy  
100 change ( $\Delta S^0$ ), and enthalpy change ( $\Delta H^0$ ), were calculated according to the following  
101 equations:

$$102 \quad \Delta G^0 = -RT \ln K_R \quad (\text{S12})$$

$$103 \quad \ln K_R = \frac{\Delta S^0}{R} - \frac{\Delta H^0}{RT} \quad (\text{S13})$$

$$104 \quad \Delta G^0 = \Delta H^0 - T\Delta S^0 \quad (\text{S14})$$

105 where,  $R$  (8.314 J/(mol·K)) is the ideal gas constant, and  $T$  (K) is the temperature in  
106 Kelvin.  $K_R$  is adsorption distribution coefficient ( $K_R = q_e/C_e$ ). The values of  $\Delta H^0$  and  $\Delta S^0$   
107 can be obtained from the slope and intercept of the curve  $\ln(K_R)$  vs.  $1/T$ .

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