## Supporting Information

# A fully degradable epoxy resin based on a nontoxic triphenol derived from diphenolic acid and eugenol 

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## 1. Characterization

Nuclear magnetic resonance (NMR) spectra were recorded on a Bruker Avance AV400 spectrometer ( 400 MHz , Bruker Corp., Switzerland) using DMSO-d6 as solvent and tetramethylsilane (TMS) as reference. Fourier transform infrared (FTIR) spectra were obtained on a Nicolet 5700 FTIR spectrometer (Nicolet Corp., USA) with a resolution of $4 \mathrm{~cm}^{-1}$ and a scanning range of 400 to $4000 \mathrm{~cm}^{-1}$. Elemental analyses were performed on a Vario Macro cube elementar analyzer (Elementar Corp., Germany). Differential scanning calorimetry (DSC) tests were carried out on a DSC-2 (Mettler -Toledo Corp., Switzerland) with heating rate of $10^{\circ} \mathrm{C} / \mathrm{min}, \mathrm{N}_{2}$ flow rate of 45 $\mathrm{mL} / \mathrm{min}$, and a temperature range of 30 to $300{ }^{\circ} \mathrm{C}$. Dynamic mechanical analysis (DMA) was performed using a DMA-1 analyzer (Mettler-Toledo Corp., Switzerland) with a sample size of $40 \mathrm{~mm} \times 10 \mathrm{~mm} \times 1.5 \mathrm{~mm}$, heating rate of $3^{\circ} \mathrm{C} / \mathrm{min}$, and temperature range of 30 to $250^{\circ} \mathrm{C}$. Thermo gravimetric analysis (TGA) was performed on a TGA/DSC 2 (Mettler Toledo Corp., Switzerland) with heating rate of $10^{\circ} \mathrm{C} / \mathrm{min}$, $\mathrm{N}_{2}$ flow rate of $50 \mathrm{~mL} / \mathrm{min}$, and temperature range of 30 to $800^{\circ} \mathrm{C}$. Stress-strain experiments were performed on a universal testing machine (5943, INSTRON, USA) with a tensile rate of $5 \mathrm{~mm} / \mathrm{min}$. The TGA-GC/MS system consists of four components: thermal gravimetry (TGA, Mettler-Toledo corp., Switzer-land), sample storage (SRA IST16, Mettler-Toledo corp., Switzer-land), gas chromatography (GC, 7890GC, Agilent Technologies Inc., USA), and mass spectrometry (MS, 5975MSD, Agilent Technologies Inc., USA). Volatile components were collected from the TGA unit,
temporarily stored in the sample storage instrument and sequentially injected into the GC-MS unit. The GC separation was carried out using an Agilent 19091s-433 capillary column ( $30 \mathrm{~m}, 0.25 \mathrm{~mm}$ i.d., $0.25 \mu \mathrm{~m}$ thickness). The injector temperature was set at $240{ }^{\circ} \mathrm{C}$ in the split mode with the split ratio of $5: 1$ with a helium gas flow of 1.2 $\mathrm{mL} / \mathrm{min}$. MS transfer line and its oven temperatures were set at $260^{\circ} \mathrm{C}$, respectively. The decomposition products were identified using mass spectrum library attached in the GC/MS system. The fracture surface morphology and carbon fiber surface before and after degradation were tested by scanning electron microscopy (SEM) (3000 V, Vltra55, ZEISS, Germany), and the surface of the samples was gold-plated before testing. Raman spectra (Raman spectra) were obtained on inVia-Reflex (Renishaw, UK) using a laser with a wavelength of 532 nm and an energy of 12 mw to test the chemical structure indicated by the carbon fibers in the range of 500 to $4000 \mathrm{~cm}^{-1}$.

## 2. Complementary information of all compounds

EGE: Yield $=75 \%,{ }^{1} \mathrm{H}$ NMR (DMSO-d6) $\delta=8.78,6.84,6.69,3.76,3.08,2.70$ and 2.56; ${ }^{13} \mathrm{C}$ NMR (DMSO-d6), $\delta=147.94,145.59,128.94,121.49,115.84,113.61$, 56.11, 52.67, 46.54 and 38.24 ; Partially good solvents: ethanol, ethyl acetate, dichloromethane, acetone etc.

DEE: Yield $=83 \%,{ }^{1} \mathrm{H}$ NMR (DMSO-d6), $\delta=6.96,6.67,5.03,3.73,2.68,2.24$, 1.95 and $1.47 ;{ }^{13} \mathrm{C}$ NMR (DMSO-d6), $\delta=173.21,155.45,147.93,145.45,139.43$, $129.62,128.63,121.56,116.63,115.79,113.49,55.97,52.69,46.52,44.18,38.21$, 33.13, 31.09 and 27.66; elemental analyses, C 69.53, H 6.43, O 24.04 for $\mathrm{C}_{27} \mathrm{H}_{30} \mathrm{O}_{7}$;
found C 69.28, H 6.61; Partially good solvents: ethanol, ethyl acetate, acetone, etc.

DEE-EP: Yield $=81 \%,{ }^{1} \mathrm{H}$ NMR (DMSO-d6), $\delta=7.07,6.88,5.01,4.29,3.96$, 3.78, 3.31, 2.83, 2.76, 2.71, 2.32, 2.09 and $1.53 ;{ }^{13} \mathrm{C}$ NMR (DMSO-d6), $\delta=173.21$, $156.65,147.39145 .31,138.77,128.38,126.88,121.67,115.14,114.45,111.56,69.36$, $55.82,52.54,50.21,47.21,44.19,38.20,34.23,32.18$ and 27.51 ; elemental analyses, C 68.14, H 6.62, O 25.24 for $\mathrm{C}_{36} \mathrm{H}_{42} \mathrm{O}_{10}$; found C 67.78, H 6.73; EEW, experimental value 197.8 , theoretical value 212.5 ; viscosity: $10.3 \mathrm{~Pa} \cdot \mathrm{~s}$ at $50^{\circ} \mathrm{C}$; Partially good solvents: dichloromethane, ethyl acetate, acetone, ethanol, etc.

## 3. Equations for calculating Ea of the polymerization

The apparent activation energies of the polymerization reactions were calculated according to the Kissinger (eq S1) and modified Ozawa (eq S2) methods.

$$
\begin{align*}
& -\ln \left(\frac{\beta}{T_{P}^{2}}\right)=\frac{E_{a}}{R T_{P}}-\ln \left(\frac{A R}{T_{P}}\right)  \tag{S1}\\
& \ln \beta=-1.052 \times \frac{E_{a}}{R T_{P}}+c \tag{S2}
\end{align*}
$$

where $\beta$ is the heating rate, $T_{\mathrm{p}}$ is the peak exothermic temperature, and R is the gas constant.

## 4. Equation for calculating cross-linking density

According to the theory of entropic elasticity of rubber, the cross-linking density can be calculated from eq S3.

$$
\begin{equation*}
v_{e}=\frac{E^{\prime}}{3 R T} \tag{S3}
\end{equation*}
$$

where $v_{\mathrm{e}}$ is the crosslink density, $E^{\prime}$ is the energy storage modulus at $T_{\mathrm{g}}+30 \mathrm{k}, \mathrm{R}$ is the gas constant, and $T$ is the absolute temperature at $T_{\mathrm{g}}+30 \mathrm{k}$.

## 5. Supplementary Figures and Tables

Table S1. Curing process of epoxy resin/hardener mixture

| Mixtures | Mole ratio | Curing | Heating process |
| :---: | :---: | :---: | :---: |
| (epoxy/hardener) | (epoxy/hardener) | promoter |  |
| DEE-EP/SA | 1/1.5 |  | $140^{\circ} \mathrm{C}$ (2h) , $160^{\circ} \mathrm{C}$ (2h) , |
|  |  |  | $180^{\circ} \mathrm{C}$ (2h) |
| DEE-EP/DDS | 1/0.75 |  | $180^{\circ} \mathrm{C}$ (2h) , $200^{\circ} \mathrm{C}$ (2h) , |
|  |  |  | $220^{\circ} \mathrm{C}$ (2h) |
| DEE-EP/EMI | 1/0.3 |  | $90^{\circ} \mathrm{C}$ ( 1 h ) , $120^{\circ} \mathrm{C}$ (1h) , |
|  |  |  | $150^{\circ} \mathrm{C}$ (2h) |
| DGEBA/SA | 1/1 | BDMA* | $140^{\circ} \mathrm{C}$ ( 1 h ) , $160^{\circ} \mathrm{C}$ ( 1 h ) , |
|  |  |  | $180^{\circ} \mathrm{C}$ (1h) |
| DGEBA/DDS | 1/0.5 |  | $180^{\circ} \mathrm{C}$ (2h) , $200^{\circ} \mathrm{C}$ (2h) , |
|  |  |  | $220^{\circ} \mathrm{C}$ (2h) |
| DGEBA/EMI | 1/0.2 |  | $100^{\circ} \mathrm{C}$ ( 1 h ) , $130^{\circ} \mathrm{C}$ ( 1 h ) , |
|  |  |  | $150^{\circ} \mathrm{C}$ (1h) |

* BDMA dosage: $0.5 \mathrm{wt} \%$ of DGEBA.

Table S2. Degradation conditions of cured resin or composite

| Organic solvent | Organic solvent to <br> water ratio | Acid <br> concentration <br> $(\mathrm{mol} / \mathrm{L})$ | Acid type | Temperature <br> $\left({ }^{\circ} \mathrm{C}\right)$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | THF | $8 / 2$ | 1 | HCl | 25 |


| 2 | DMF | 8/2 | 1 | HCl | 25 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | DMSO | 8/2 | 1 | HCl | 25 |
| 4 | Ethanol | 8/2 | 1 | HCl | 25 |
| 5 | THF | 8/2 | 1 | HCl | 25 |
| 6 | THF | 6/4 | 1 | HCl | 25 |
| 7 | THF | 4/6 | 1 | HCl | 25 |
| 8 | THF | 2/8 | 1 | HCl | 25 |
| 9 | THF | 8/2 | 2 | HCl | 25 |
| Table S2 (continued). Degradation conditions of cured resin or composite |  |  |  |  |  |
|  | Organic solvent | Organic solvent to water ratio | Acid concentration ( $\mathrm{mol} / \mathrm{L}$ ) | Acid type | Temperature <br> $\left({ }^{\circ} \mathrm{C}\right)$ |
| 10 | THF | 8/2 | 1 | HCl | 25 |
| 11 | THF | 8/2 | 0.5 | HCl | 25 |
| 12 | THF | 8/2 | 0.05 | HCl | 25 |
| 13 | THF | 8/2 | 1 | $\mathrm{H}_{2} \mathrm{SO}_{4}$ | 25 |
| 14 | THF | 8/2 | 1 | HCl | 25 |
| 15 | THF | 8/2 | 1 | $\mathrm{H}_{3} \mathrm{PO}_{4}$ | 25 |
| 16 | THF | 8/2 | 1 | $\mathrm{CH}_{3} \mathrm{COOH}$ | 25 |
| 17 | THF | 8/2 | 1 | HCl | 25 |
| 18 | THF | 8/2 | 1 | HCl | 35 |
| 19 | THF | 8/2 | 1 | HCl | 45 |
| 20 | THF | 8/2 | 1 | HCl | 55 |

Table S3. Important DSC factors of the epoxide mixtures and their activation energy $\left(E_{\mathrm{a}}\right)$ values.

|  | $T_{\mathrm{p}}\left({ }^{\circ} \mathrm{C}\right)$ |  |  | $E_{\mathrm{a}}(\mathrm{kJ} / \mathrm{mol})$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mixture | $5^{\circ} \mathrm{C} / \mathrm{min}$ | $10^{\circ} \mathrm{C} / \mathrm{min}$ | $15^{\circ} \mathrm{C} / \mathrm{min}$ | $20^{\circ} \mathrm{C} / \mathrm{min}$ | Kissinger | Ozawa |
| DEE-EP/SA | 165 | 181 | 188 | 193 | 75.5 | 83.9 |
| DGEBA/SA | 269 | 286 | 300 | 307 | 79.1 | 89.1 |
| DEE-EP/DDS | 176 | 193 | 198 | 203 | 79.5 | 81.4 |
| DGEBA/DDS | 197 | 214 | 222 | 228 | 83.8 | 85.1 |
| DEE-EP/EMI | 96 | 109 | 116 | 119 | 64.4 | 84.9 |
| DGEBA/EMI | 113 | 120 | 128 | 132 | 67.4 | 87.2 |

Table S4. Main thermal and mechanical properties of the cured epoxy.

| Cured resin | $T_{\mathrm{g}}\left({ }^{\circ} \mathrm{C}\right)$ | $E^{\prime}\left(25^{\circ} \mathrm{C}\right)$ | $v_{\mathrm{e} \times 10^{3}}$ | $T_{\mathrm{d} 10}$ | CY | Tensile strength | Elongation |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DEE-EP/SA | 85 | 1765 | 1.53 | 354 | 22 | $57.1 \pm 2.3$ | $5.4 \pm 0.3$ |
| DGEBA/SA | 77 | 2478 | 1.38 | 372 | 12 | $50.4 \pm 2.1$ | $5.3 \pm 0.5$ |
| DEE-EP/DDS | 181 | 2943 | 1.45 | 305 | 23 | $67.9 \pm 3.4$ | $5.5 \pm 0.4$ |
| DGEBA/DDS | 168 | 2633 | 1.18 | 394 | 12 | $59.4 \pm 4.2$ | $4.3 \pm 0.2$ |
| DEE-EP/EMI | 134 | 2254 | 1.48 | 318 | 25 | $56.2 \pm 4.5$ | $4.0 \pm 0.1$ |
| DGEBA/EMI | 121 | 2530 | 1.36 | 371 | 6 | $45.5 \pm 2.7$ | $3.7 \pm 0.2$ |

Table S5. Dissolution rate of DEE-EP/SA resin in different solvents

|  | THF | DMF | Ethanol | DMSO | $\mathrm{H}_{2} \mathrm{O}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| DEE-EP/SA | 22.3 | 15.5 | 1.8 | 11.7 | 0.4 |

Table S6. Mechanical properties of composites and carbon fibers before and after recycling

| Sample | Stress (MPa) | Strain (\%) |
| :---: | :---: | :---: |
| DEE-EP/SA/CF | $713.7 \pm 12.8$ | $3.3 \pm 0.3$ |
| DEE-EP/SA/RCF | $655.6 \pm 9.8$ | $3.0 \pm 0.2$ |
| Ref 56 | $145.4 \pm 17.1$ | $19.2 \pm 0.9$ |
| Ref 57 | $622.0 \pm 17.0$ | $4.0 \pm 0.2$ |
| Ref 58 | $381.0 \pm 66.0$ | $4.2 \pm 0.6$ |
| Virgin CF | $3892.1 \pm 16.5$ | $2.1 \pm 0.3$ |
| Recycled CF | $3606.6 \pm 10.1$ | $1.9 \pm 0.2$ |



Figure S1. The ${ }^{1} \mathrm{H}$ NMR spectrum of EGE.


Figure S2. The ${ }^{13} \mathrm{C}$ NMR spectrum of EGE.


Figure S3. The ${ }^{13} \mathrm{C}$ NMR spectrum of DEE.


Figure S4. The FTIR spectra of EGE, DEE and DEE-EP.


Figure S5. The ${ }^{13} \mathrm{C}$ NMR spectrum of DEE-EP.


Figure S6. The hardeners used in this work.


Figure S7. FTIR spectra of DEE-EP before and after curing.


Figure S8. FTIR spectra of DGEBA before and after curing.


Figure S9. DSC spectra of DGEBA with different hardeners at heating rate of $10^{\circ} \mathrm{C} / \mathrm{min}$.


Figure S10. DSC thermograms of DEE-EP/SA mixture at different heating rates.


Figure S11. DSC thermograms of DEE-EP/DDS mixture at different heating rates.


Figure S12. DSC thermograms of DEE-EP/EMI mixture at different heating rates.


Figure S13. DSC thermograms of DGEBA/SA mixture at different heating rates.


Figure S14. DSC thermograms of DGEBA/DDS mixture at different heating rates.


Figure S15. DSC thermograms of DGEBA/EMI mixture at different heating rates.


Figure S16. Plots of $\mathrm{E}_{\mathrm{a}}$ values calculated using Kissing-Akahira-Sunose method.


Figure S17. Plots of Ea values calculated using Flynn-Wall-Ozawa method.


Figure S18. Storage modulus $\mathrm{E}^{\prime}$ of the cured resins.


Figure S19. DTG curves of the cured resins.


| Temperature $\left({ }^{\circ} \mathrm{C}\right)$ | Thermal degradation products |
| :---: | :---: |
| 320 | Not available |
| 360 |  |
| 400 |  |
| 440 |  |
| 480 |  |

Figure S20. The thermal degradation products detected by the TGA-GC/MS coupling system from the cured (a) DEE-EP/SA and (b) DGEBA/SA resins at a heating rate of $10^{\circ} \mathrm{C} / \mathrm{min}$.


Figure S21. GC spectrum of the cured DEE-EP/SA resin decomposed at $320^{\circ} \mathrm{C}$.


Figure S22. GC spectrum of the cured DEE-EP/SA resin decomposed at $360^{\circ} \mathrm{C}$.


Figure S23. GC spectrum of the cured DEE-EP/SA resin decomposed at $400^{\circ} \mathrm{C}$.


Figure S24. GC spectrum of the cured DEE-EP/SA resin decomposed at $440^{\circ} \mathrm{C}$.


Figure S25. GC spectrum of the cured DEE-EP/SA resin decomposed at $480^{\circ} \mathrm{C}$.


Figure S26. GC spectrum of the cured DGEBA/SA resin decomposed at $360^{\circ} \mathrm{C}$.


Figure S27. GC spectrum of the cured DGEBA/SA resin decomposed at $400^{\circ} \mathrm{C}$.


Figure S28. GC spectrum of the cured DGEBA/SA resin decomposed at $440^{\circ} \mathrm{C}$.


Figure S29. GC spectrum of the cured DGEBA/SA resin decomposed at $480^{\circ} \mathrm{C}$.


Figure S30. Stress-strain curves of the cured resins.


Figure S31. DGEBA/SA resin (a) and DEE-EP/DDS resin (b) and DEE-EP/EMI resin (c) degradation testing.


Figure S32. FTIR spectra of DEE-EP and DGEBA cured with SA.


Figure S33. Degradation time of DEE-EP/SA in different organic solvents.


Figure S34. Degradation time of DEE-EP/SA in different ratios of organic solvents and water.


Figure S35. Degradation time of DEE-EP/SA in different types of acids.


Figure S36. Degradation time of DEE-EP/SA in different temperatures.


Figure S37. Fracture surface of DEE-EP/SA/CF composites.


Figure S38. SEM images of original and recycled CF.


Figure S39. Stress-strain curves of the original and recovered CFs.


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