

*Supporting Information*

**Efficient inverse CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub> separation driven by rare thermodynamic  
affinities difference in a porous MOF**

Hai-Yu Duan<sup>a</sup>, Xiu-Yuan Li\*<sup>a</sup>, Lei Hou\*<sup>b</sup>, Si-Ru Liu<sup>a</sup>, Xiang-Yu Liu\*<sup>c</sup>, Ping Wang\*<sup>a</sup>

<sup>a</sup>Shaanxi Key Laboratory of Optoelectronic Functional Materials and Devices, School of Materials Science and Chemical Engineering, Xi'an Technological University, Xi'an, 710021, P. R. China. E-mail: lixiuyuan@xatu.edu.cn, wping0922@163.com

<sup>b</sup>Key Laboratory of Synthetic and Natural Functional Molecule Chemistry of the Ministry of Education, Shaanxi Key Laboratory of Physico-Inorganic Chemistry, College of Chemistry & Materials Science, Northwest University, Xi'an 710069, P. R. China. E-mail: lhou2009@nwu.edu.cn

<sup>c</sup>State Key Laboratory of High-efficiency Coal Utilization and Green Chemical Engineering, College of Chemistry and Chemical Engineering, Ningxia University, Yinchuan 750021, P. R. China. E-mail: xiangyuli432@126.com

**Table S1** Summary of adsorption uptakes,  $Q_{st}$  values and selectivity of equimolar CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub> mixture for reported CO<sub>2</sub>-selective MOFs.

MOFs	Uptake of CO <sub>2</sub> /C <sub>2</sub> H <sub>2</sub> @273K, 100 kPa (cm <sup>3</sup> g <sup>-1</sup> )	Uptake of CO <sub>2</sub> /C <sub>2</sub> H <sub>2</sub> @298K, 100 kPa (cm <sup>3</sup> g <sup>-1</sup> )	$Q_{st}$ of CO <sub>2</sub> /C <sub>2</sub> H <sub>2</sub> (kJ mol <sup>-1</sup> )	Selectivity	Selectivity Conditions	Ref.
[Co(HL <sup>dc</sup> )]	108/-	239.5 <sup>e</sup> /140 <sup>e</sup>	\	\	\	1
[Mn(bdc)(dpe)]	46.8 <sup>a</sup> /7.3 <sup>a</sup>	\	29–30/28	8.8	273 K, 100 kPa	2
SIFSIX-3-Ni	\	2.7 <sup>c</sup> /3.3 <sup>c</sup>	50.9/36.7	7.7 <sup>j</sup>	298 K, 1 bar	3
CD-MOF-1	\	2.87 <sup>c</sup> /2.23 <sup>c</sup>	41.0/17.6	6.6 <sup>i</sup>	298 K, 100 kPa	4
CD-MOF-2	\	2.67 <sup>c</sup> /2.03 <sup>c</sup>	67.2/25.8	16.0 <sup>j</sup>	298 K, 100 kPa	4
Tm-MOF	146.3/63.0	130.6/47	45.2/17.8	17.5 <sup>j</sup>	298 K, 1 bar	5
MUF-16	\	47.78 <sup>f</sup> /3.99 <sup>f</sup>	32.3/-	510	293 K, 1 bar	6
MUF-16(Ni)	\	47.97 <sup>f</sup> /7.53 <sup>f</sup>	37.3/-	46	293 K, 1 bar	6
MUF-16(Mn)	\	50.5 <sup>f</sup> /9.69 <sup>f</sup>	36.6/-	31	293 K, 1 bar	6
Cd-NP	\	58.0/9.7	27.7/-	85	298 K, 1 bar	7
PCP-NH <sub>2</sub> -ipa	\	72/43	36.6/26.8	6.4	298 K, 1 bar	8
PCP-NH <sub>2</sub> -bdc	\	68/43	34.57/25.6	4.4	298 K, 1 bar	8

Ce(IV)-MIL-140-4F	151.7 <sup>b</sup> /53.5 <sup>b</sup>	110.3 <sup>b</sup> /41.5 <sup>b</sup>	39.5/27.4	9.5 <sup>j</sup>	298 K, 100 kPa	9
PMOF-1	47.5/9.5	\	\	\	\	10
[Zn(atz)(BDC-Cl <sub>4</sub> ) <sub>0.5</sub> ] <sub>n</sub>	60.2 <sup>b</sup> /-	19.7 <sup>b</sup> /-	32.7/25.4	2.4	285 K, 100 kPa	11
Cu-F-pymo	\	1.19 <sup>c</sup> /0.10 <sup>c</sup>	28.8/-	>10 <sup>5</sup>	298 K, 100 kPa	12
[Cu(hfipbb)(H <sub>2</sub> hfipbb) <sub>0.5</sub> ]	0.75 <sup>c</sup> /0.03 <sup>c</sup>	0.74 <sup>c</sup> /0.10 <sup>c</sup>	25.5/-	696	298 K, 1 bar	13
SU-101(Bi)	\	53.7/51.4	30.5/28.8	5.5	298 K, 100kPa	14
SU-101(Al)	\	53.1/-	31.3/-	15.5	298 K, 100 kPa	14
SU-101(In)	\	55.0/-	28.3/-	6.2	298 K, 100 kPa	14
SU-101(Ga)	\	40.2/-	27.7/-	11.1	298 K, 100 kPa	14
[Zn(odip) <sub>0.5</sub> (bpe) <sub>0.5</sub> (CH <sub>3</sub> OH)]	118.8/59.0	118.7/39.8	42.3/35.0	13.2	298 K, 100 kPa	15
ZU-610a	\	1.51 <sup>c</sup> /0.12 <sup>c</sup>	27.3/-	207	298 K, 100 kPa	16
Y-bptc	\	55/-	31.5/-	4.1	298 K, 1bar	17
SNNU-334	85.1/66.8	\	20.2/38.3	3595.4	273 K, 1atm	18
SNNU-335	78.4/63.0	\	38.07/44.23	\	\	18
SNNU-336	92.7/65.3	\	50.9/48.7	\	\	18

MOF-808-ARG (dry)	\	51.0/41.3	48.3/38.8	3.5 <sup>j</sup>	298 K, 1 bar	19
MOF-808-ARG (wet)	\	71.0/7.8	70.3/5.2	71 <sup>j</sup>	298 K, 1 bar	19
Bi-MOF-CHO	\	147.7 <sup>b</sup> /81.8 <sup>b</sup>	48.2/46.2	7.7	298 K, 100 kPa	20
Bi-MOF-COOH	\	114.7 <sup>b</sup> /-	43.6/40.6	5.3	298 K, 100 kPa	20
Bi-MOF-NO <sub>2</sub>	\	129.1 <sup>b</sup> /-	38.8/38.5	4.9	298 K, 100 kPa	20
BUCT-C19	\	40.3/6.7	\	10700	298 K, 100 kPa	21
F4_MIL- 140A(Ce)	\	2.6 <sup>c</sup> /-	35-45/-	\	\	22
MFU-4	\	3.17 <sup>c,g</sup> /-	24/-	3360	300 K, 1bar	23
Zn-DPNA	61.1/92.1	52.7/-	43.1/32.4	11.9	298 K, low pressure	24
ALF	\	86.2/3.3	\	6.5×10 <sup>5</sup>	298 K, 100 kPa	25
NKMOF-9a	57.5/4.9	46.4/2.8	69.6/-	241.9	298 K, 1 bar	26
Zn-ox-mtz	\	68.78/5.46	43.02/-	1064.9	298 K, 1.0 bar	27
Zn-ox-trz	\	89.49/67.85	38.09/38.39	1.9	298 K, 1.0 bar	27
Co-CUK-1	170 <sup>d</sup> /119 <sup>d</sup>	106/86	20.8/-	2	298 K, 100 kPa	28
Ni-CUK-1	142 <sup>d</sup> /97 <sup>d</sup>	\	21.7/-	2	298 K, 100 kPa	28

Mg-CUK-1	144 <sup>d</sup> /89 <sup>d</sup>	\	\	2	298 K, 100 kPa	28
HOF-FJU-88	\	59.6 <sup>h</sup> /6.28 <sup>h</sup>	12.3/-	1894	296 K, 1 bar	29
Cu(Qc) <sub>2</sub>	\	66.6 <sup>b</sup> /26.5 <sup>b</sup>	31.7±3.5/ 21.4±3.5	5.6	298 K, 1 bar	30
1	74.6/45.5	57.0/37.9	38.7/29.0	3.0	298 K, 100 kPa	This work

<sup>a</sup> at 273 K, 91 kPa;

<sup>b</sup> gas uptake ( $\text{cm}^3 \text{ cm}^{-3}$ );

<sup>c</sup> gas uptake (mmol g<sup>-1</sup>);

the gas uptakes of CO<sub>2</sub> and/or C<sub>2</sub>H<sub>2</sub> <sup>d</sup> at 233 K, <sup>e</sup> at 195 K, <sup>f</sup> at 293 K, <sup>g</sup> at 300 K, <sup>h</sup> at 296 K, <sup>i</sup> at 298 K and 5 bar;

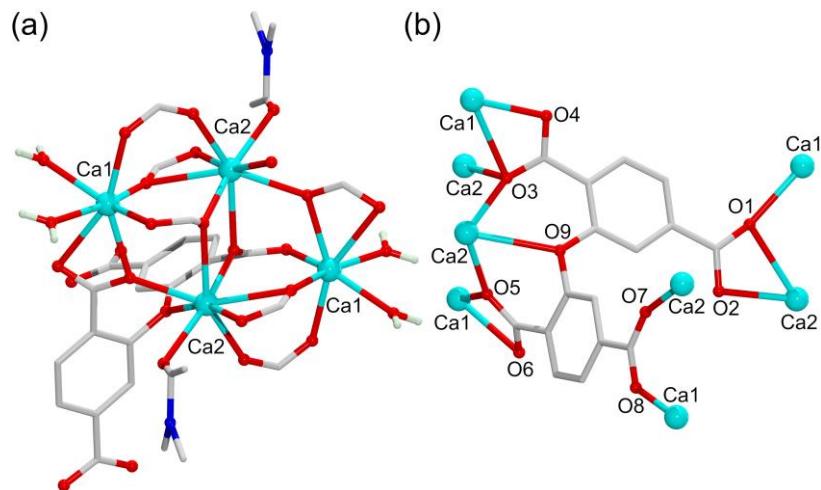
<sup>j</sup> the mixture of CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub> (1:2, v:v).

**Table S2** Structures data and selected refinement of **1**.

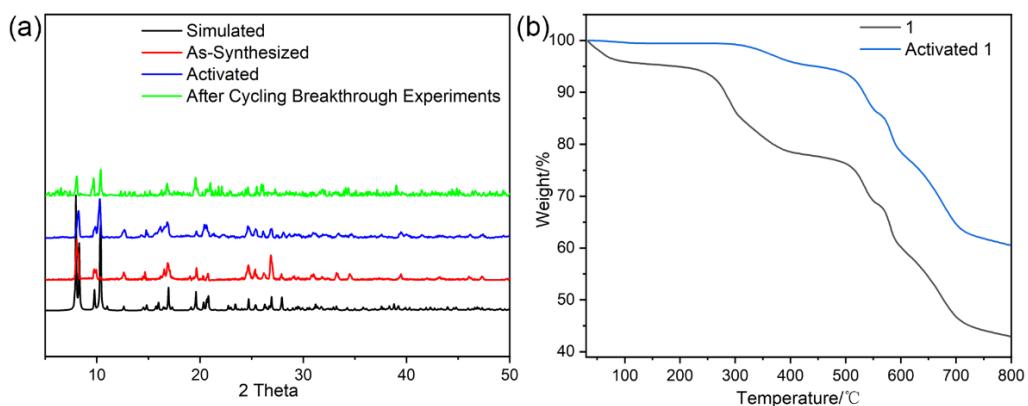
Complex	<b>1</b>
Molecular Formula	C <sub>20</sub> H <sub>19</sub> Ca <sub>2</sub> NO <sub>12</sub>
Formula Weight	545.52
Temperature (K)	293(2) K
Crystal System	Triclinic
Space Group	<i>P</i> 1̄
<i>a</i> (Å)	10.2890(4)
<i>b</i> (Å)	11.6704(6)
<i>c</i> (Å)	12.4006(10)
$\alpha$ (°)	71.553(6)
$\beta$ (°)	66.005(6)
$\gamma$ (°)	68.890(4)
<i>V</i> (Å <sup>3</sup> )	1243.56(15)

Z	2
D <sub>c</sub> (g·cm <sup>-3</sup> )	1.457
F(000)	564
Reflections collected	10350
Goodness-of-fit on $F^2$	1.049
$R_1^a[I > 2\sigma(I)]$	0.0760
wR <sub>2</sub> <sup>b</sup> [ $I > 2\sigma(I)$ ]	0.2188

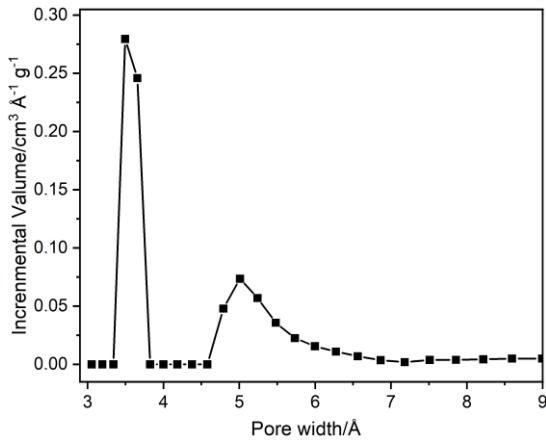
<sup>a</sup> $R_1 = \Sigma ||F_o| - |F_c|| / \Sigma |F_o|$ , <sup>b</sup>wR<sub>2</sub> = [ $\sum w(F_o^2 - F_c^2)^2 / \sum w(F_o^2)$ ]<sup>1/2</sup>



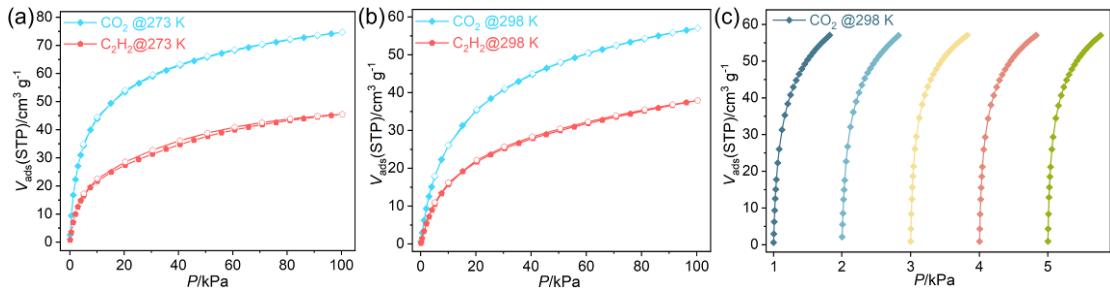
**Fig. S1** (a) Coordination environment of  $\text{Ca}^{2+}$  ion; (b) Coordination mode of  $\text{H}_4\text{odp}$ .



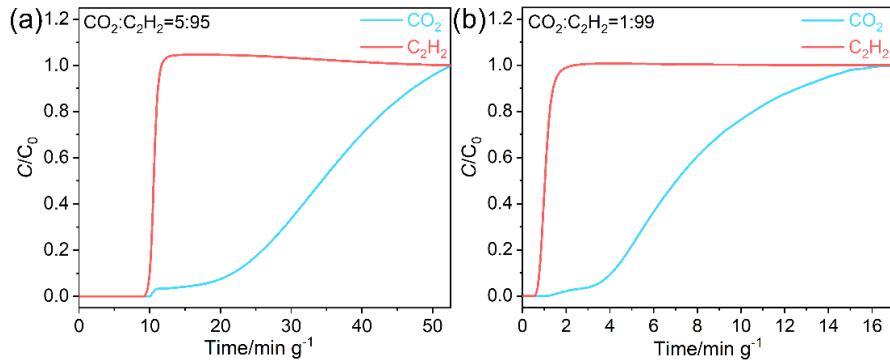
**Fig. S2** PXRD and TGA patterns.



**Fig. S3** The pore size distributions obtained by the non-local density-functional theory (NLDFT) model from CO<sub>2</sub> at 273 K.



**Fig. S4** Gas sorption isotherms (units: cm<sup>3</sup> g<sup>-1</sup>) for CO<sub>2</sub> and C<sub>2</sub>H<sub>2</sub> at (a) 273 K and (b) 298 K; (c) Cyclic CO<sub>2</sub> sorption isotherms at 298 K.

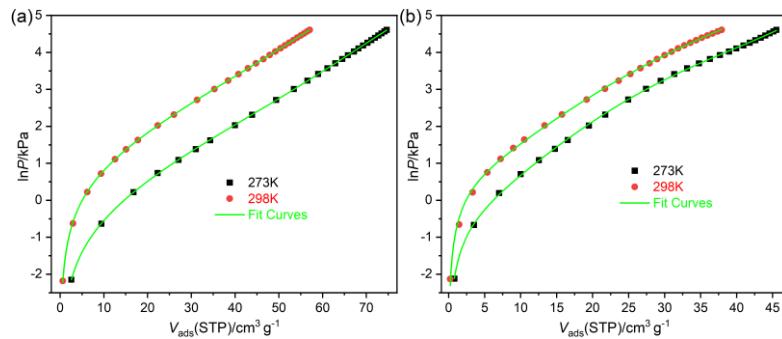


**Fig. S5** Breakthrough curves for (a) 5/95 and (b) 1/99 CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub> mixtures.

## Calculation of Sorption Heat using Virial 2 Model

$$\ln P = \ln N + 1/T \sum_{i=0}^m a_i N^i + \sum_{i=0}^n b_i N^i \quad Q_{st} = -R \sum_{i=0}^m a_i N^i$$

The above virial expression was used to fit the combined isotherm data for three frameworks at 273 and 298 K, where  $P$  is the pressure,  $N$  is the adsorbed amount,  $T$  is the temperature,  $a_i$  and  $b_i$  are virial coefficients, and  $m$  and  $N$  are the number of coefficients used to describe the isotherms.  $Q_{st}$  is the coverage-dependent enthalpy of adsorption and  $R$  is the universal gas constant.



**Fig. S6** (a) CO<sub>2</sub> and (b) C<sub>2</sub>H<sub>2</sub> adsorption isotherms of **1a** with fitting by Virial 2 model.

**Table S3** Parameters obtained from the Virial 2 model fitting of the single-component adsorption isotherms of CO<sub>2</sub> and C<sub>2</sub>H<sub>2</sub> at 273 K and 298 K.

	a0	a1	a2	a3	a4	a5	b0	b1	b2	b3	Chi <sup>2</sup>	R <sup>2</sup>
CO <sub>2</sub>	-4678.02	34.6279	-0.7279	-1.80E-04	9.81E-05	-5.12E-07	13.9894	-0.10383	0.00352	-2.30E-05	1.12E-04	1
C <sub>2</sub> H <sub>2</sub>	-3505.79	82.8451	-0.59184	-0.04199	7.24E-04	-2.06E-06	10.9831	-0.33925	0.01012	-8.08E-05	2.08E-03	0.999

## CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub> Mixtures Selectivity Prediction via IAST

The experimental isotherm data for pure CO<sub>2</sub> and C<sub>2</sub>H<sub>2</sub> were fitted using a dual Langmuir-Freundlich (L-F) model:

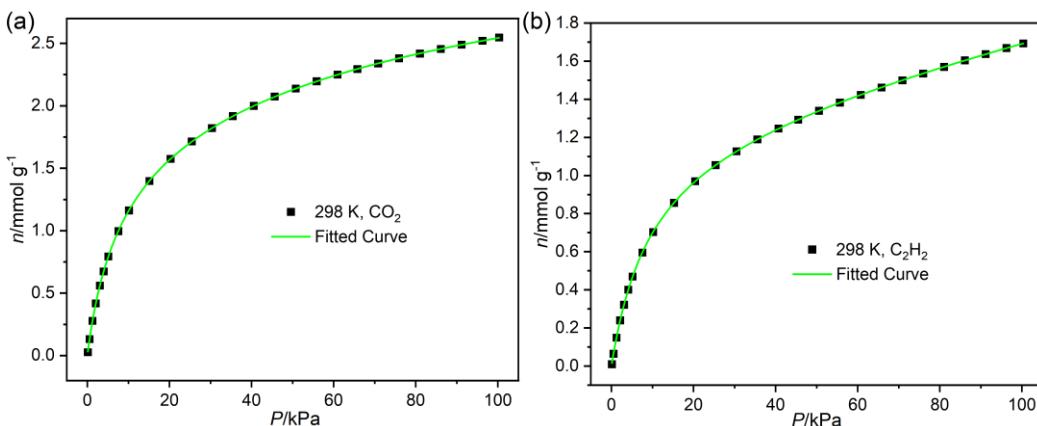
$$q = \frac{a_1 * b_1 * p^{c1}}{1 + b_1 * p^{c1}} + \frac{a_2 * b_2 * p^{c2}}{1 + b_2 * p^{c2}}$$

Where  $q$  and  $p$  are adsorbed amounts and the pressure of component  $i$ , respectively.

The adsorption selectivities for binary mixtures defined by

$$S_{i/j} = \frac{x_i * y_j}{x_j * y_i}$$

were respectively calculated using IAST. Where  $x_i$  is the mole fraction of component  $i$  in the adsorbed phase and  $y_i$  is the mole fraction of component  $i$  in the bulk.



**Fig. S7** Adsorption isotherms of **1a** fitting by dual L-F model.

**Table S4** Parameters obtained from the dual Langmuir-Freundlich fitting of the single-component adsorption isotherms.

298 K	a1	b1	c1	a2	b2	c2	Chi^2	R^2
CO <sub>2</sub>	1.52099	0.14252	0.99064	2.17614	0.01862	0.8798	1.99E-06	1
C <sub>2</sub> H <sub>2</sub>	1.18319	0.10654	1.01937	8.03444	0.00109	0.93587	2.26E-06	1

## Separation Potential Calculation

The separation potential ( $\Delta q$ ) is a combined metric, which incorporates both uptake capacity and selectivity, which is defined to evaluate the separation performances in fixed bed adsorbers for gas mixture. The separation potential  $\Delta q$ , is calculated from IAST base on the following equation:

$$\Delta q = q_1 \frac{y_2}{y_1} - q_2$$

Where  $y_1$  and  $y_2$  are the mole fractions of the CO<sub>2</sub> and C<sub>2</sub>H<sub>2</sub> in the CO<sub>2</sub>/C<sub>2</sub>H<sub>2</sub> mixture gases, respectively.  $q_1$  and  $q_2$  are CO<sub>2</sub> and C<sub>2</sub>H<sub>2</sub> uptake in the gas mixture, respectively, and predicted by the IAST theory. The physical significance of  $\Delta q$  is that it represents the maximum amount of pure C<sub>2</sub>H<sub>2</sub> that can be obtained during the adsorption phase of fixed bed separations.

## Calculation of Breakthrough Experiments

The calculation method of the C<sub>2</sub>H<sub>2</sub> purity is as follows:

$$c = \frac{q_{C_2H_2}}{q_{C_2H_2} + q_{CO_2}}$$

The gas breakthrough gas amount ( $q_i$ ) (mmol g<sup>-1</sup>) was calculated by integrating the breakthrough curve  $F_i(t)$  as following equation:

$$q_i = \frac{f_i \int_0^{t_1} F_i(t) dt}{22.4 \times m}$$

Where the  $m$  represents the adsorbent mass,  $f_i$  is the flow rate of gas  $i$  (mL min<sup>-1</sup>);  $F_i(t)$  is the function of the breakthrough curve of component  $i$ .

## Simulation Methodology

Grand canonical Monte Carlo (GCMC) simulations were performed for evaluating the gas adsorption performance. The partial charges of atoms in the framework were originated from the QEq method.<sup>31</sup> The supercell of 3×3×3 was used during the simulation. All the parameters for atoms of **1a** were modeled with the Dreiding forcefield.<sup>32</sup> CO<sub>2</sub> was modeled as a rigid linear triatomic molecule with three charged

LJ interaction sites, for which the LJ potential parameters for O atom ( $q = -0.35e$ ) and C atom ( $q = +0.70e$ ) in CO<sub>2</sub> molecule with C-O bond length  $l = 0.116$  nm were taken from the TraPPE force field.<sup>33</sup> The partial charges on the atoms of C<sub>2</sub>H<sub>2</sub> molecule was taken from the literature ( $q_C = -0.266e$  and  $q_H = +0.266e$ ), and the LJ potential parameters for C<sub>2</sub>H<sub>2</sub> was taken from the Optimized Potentials for Liquid Simulations-All Atom (OPLS-AA) force field.<sup>34</sup> A cutoff distance of 15.4 Å was used for LJ interactions, and the Coulombic interactions were calculated by using Ewald summation. For each run, the  $5 \times 10^6$  equilibration steps,  $5 \times 10^6$  production steps were employed.

The binding energy was calculated by DFT method using the Dmol<sup>3</sup> module. The calculations were performed under the generalized gradient approximation (GGA) with the Perdew-Burke-Ernzerhof (PBE) exchange-correlation functional and the double numerical plus d-functions (DND) basis set. A cutoff of 4.5 Å was used and the SCF convergence was set to  $10^{-5}$ . The binding energy of gas is evaluated by the following equation:  $E_{\text{bind}} = E_{\text{framework+gas}} - E_{\text{framework}} - E_{\text{gas}}$ , in which  $E_{\text{framework+gas}}$  is the total energy of the framework and the adsorbed gas molecule,  $E_{\text{framework}}$  and  $E_{\text{gas}}$  are the energies of the framework and gas molecule.

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