

Supplementary Information

Nanostructured Layered double hydroxide (NLDH) - Zn/Al-based materials: Strategy to Improve Performance for Zirconium Sorption from Acidic Sulfate Solution

Ahmed M. Masoud¹, Amal E. Mubark^{1}, Mohamed H. Taha¹, Saber Ibrahim^{2,3}*

¹ Nuclear Materials Authority, P.O. Box 530, El Maddi, Cairo, Egypt

² Packaging Materials Department, National Research Centre, 12622, Dokki, Cairo, Egypt

³ Nanomaterials Investigation Laboratory, central Laboratories Network, National Research Centre, Dokki, Cairo, 12622, Egypt

*Corresponding author: amal_mubark2014@yahoo.com, Tel.: +201018600164

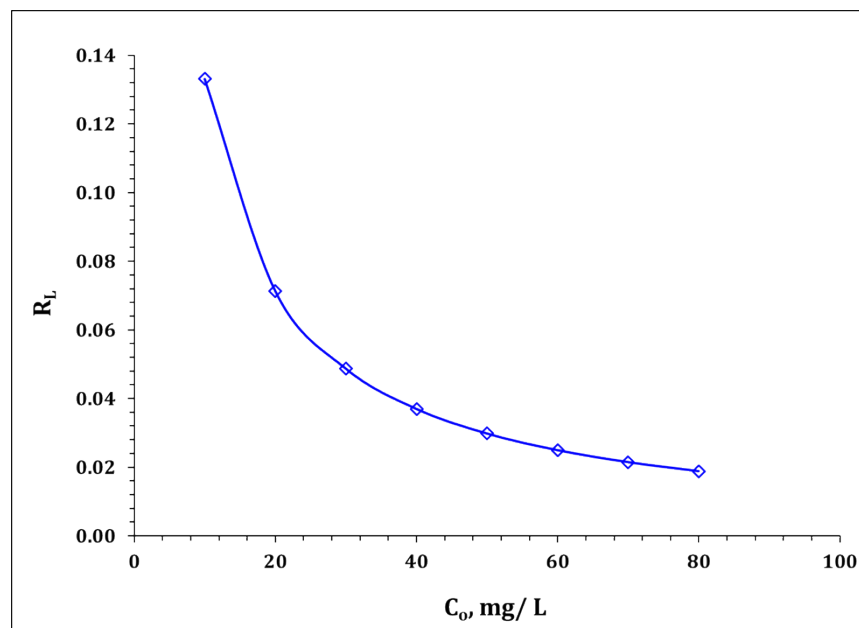


Figure S1: Separation factor R_L of Zr(IV) adsorption process.

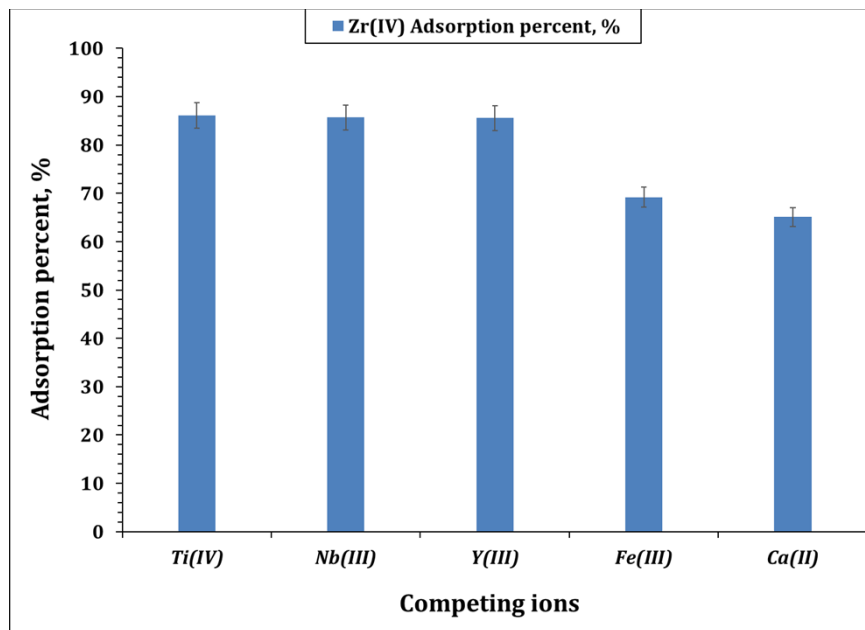


Figure S2: *Effect of co-existing elements on Zr(IV) ions adsorption process.*

Table S1: Kinetic, isotherm, and thermodynamics equations for Zr(IV) adsorption process [1-11].

Kinetics	Equations
Pseudo-first-order	$q_t = q_1(1 - e^{-k_1t})$
Pseudo-second-order	$q_t = \frac{1}{(1 k_2q_2^2) + (t q_2)}$
Intra-particle diffusion model (IPD)	$q_t = K_{id}t^{0.5} + C_i$
Isotherms	Equations
Langmuir model	$q_e = \frac{q_m k_L C_e}{1 + k_L C_e}$
Freundlich model	$q_e = K_F C_e^{1/n_F}$
Temkin model	$q_e = \frac{RT}{b_T} \ln K_T C_e$
Sips model	$q_e = \frac{q_S (k_S C_e)^{m_S}}{1 + (k_S C_e)^{m_S}}$
Thermodynamics	Equations
	$\log K_C = -\frac{\Delta H^0}{2.303 R} X \frac{1}{T} + C$ $-\Delta G^0 = 2.303 RT \log K_C$ $\Delta G^0 = \Delta H^0 - T \Delta S^0$
Fitting	Equations
Coordination coefficient (R^2)	$R^2 = 1 - \frac{\sum_1^n (q_{exp} - q_{pred})^2}{\sum_1^n (q_{exp} - q_{exp}^-)^2}$
Chi-square coefficient (χ^2)	$\chi^2 = \sum \left[\frac{(q_{exp} - q_{pred})^2}{q_{pred}} \right]$

q_e (mg g^{-1}) is the equilibrium concentration of Zr(IV) species, and q_t (mg g^{-1}) is the adsorbed amount of Zr(IV) species ions after time t (min), C_e (mg L^{-1}) is equilibrium concentration of Zr(IV) species. k_1 (min^{-1}) and k_2 (min^{-1}) are the rate constants for the pseudo first and second order, respectively. K_{id} ($\text{mg/g. min}^{0.5}$) is a rate constant, and C is the thickness of the boundary layer. q_m and q_s are the maximum sorption capacity (mg. g^{-1}) of Langmuir and Sips models. K_L (L. mg^{-1}), K_F (L/ mg), K_T (L min^{-1}), and K_S (L/ mg) are represent the constants of Langmuir, Freundlich, Temkin, and Sips models. n refer to the sorption intensity, b_T is Temkin constant that refers to the adsorption heat, m_S is Sips constant. q_s is the theoretical isotherm saturation capacity (mg/g). K_C is a non-dimensional equilibrium constant and it equals $K_d \times 1000 \times \rho$ [8-10]; T is the temperature (K), R is the universal gas constant ($8.314 \text{ J mol}^{-1} \cdot \text{K}^{-1}$), ρ is solution density g/ L , and C is a constant. R^2 and χ^2 are the coordination and Chi-square coefficients respectively, the number of test points is n , the experimental equilibrium capacity is q_{exp} (mg g^{-1}), while the predicted capacity is q_{pred} (mg g^{-1}).

References:

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Table S2: *The values of Morris-Weber model terms for Zr(IV) sorption using Zn/Al-LDH sorbent.*

Weber and Morris model	Stage I	
	k_i (mg/g min ^{1/2})	10.12
	C	18.1
	R ²	0.97
	Stage II	
	k_i (mg/g min ^{1/2})	0.88
	C	78.3
	R ²	0.96

Table S3: Zr(IV) desorption from loaded Zn/Al-LDH material using different solutions (0.5 g/L, room temperature; 120 min).

Eluent type	Sorption efficiency, %
1.0 M Hydrochloric acid	98.1
1.0 M Sulfuric acid	76.7
1.0 M Nitric	64.3

Table S4: Sorption/ desorption cycles for Zr(IV) recovery using *Zn/Al-LDH* material.

No. of cycle	Zr(IV)	
	Sorption	Desorption
1	90.6	98.0
2	90.2	98.0
3	89.9	97.8
4	89.4	97.2
5	88.9	96.7
6	88.7	95.8

Table S5. Chemical composition of the real waste solution before, and after the adsorption process, as well as the adsorption efficiency.

Constituents	C₀ mg/ L	C_e mg/ L	E%
Zr (IV)	120	15	87.5
V (IV)	100	97	3.0
Ti (IV)	66	56	15.2
Fe(III)	230	190	17.4
Na (I)	640	622	2.8
K (I)	252	239	5.2
SO ₄ (-II)	980	973	1