Supplementary information for:

Identifying the ideal thermodynamics of non-stoichiometric oxygen-carrier materials for chemical looping water-gas shift

Derivation of dimensionless number $λ_0$

The dimensionless number λ_0 , which is used extensively throughout the paper, is defined by the ratio of moles of usable oxygen in the solid phase $N_{OCM, oxygen, usable, divided by the$ moles of oxygen present in the passing gas phase stream during a half cycle $N_{\text{Gas, oxygen}}$.

$$
\lambda_O = \frac{N_{OCM, oxygen, usable}}{N_{Gas, oxygen}}
$$
 Eq. S1

The moles of oxygen present in the passing gas phase stream in a half cycle is given by the following,

$$
N_{Gas, oxygen} = F_0 t
$$
 Eq. S2

where F_o refers to the molar flowrate of oxygen in the gas phase and t refers to the duration of the half cycle.

The usable moles of oxygen in the OCM is logically given by the following,

$$
N_{OCM, oxygen, usable} = N_{OCM, oxygen, oxidation} - N_{OCM, oxygen, reduction}
$$
 Eq. S3

where $N_{OCM, oxygen, oxidation}$ and $N_{OCM, oxygen, reduction}$ refer to the moles of oxygen in the OCM at the end of the oxidation and reduction half cycles respectively.

The moles of oxygen in the OCM at the end of the oxidation and reduction half cycles are given by,

$$
N_{OCM, oxygen, oxidation} = (S - \delta_{ox}) N_{OCM}
$$
 Eq. S4

$$
N_{OCM, oxygen, reduction} = (S - \delta_{red}) N_{OCM}
$$
 Eq. S5

where N_{OCM} refers to the moles of OCM, S refers to the oxygen stoichiometry when δ is equal to 0 (e.g. for the OCM La_{0.6}Sr_{0.4}FeO_{3-*δ*} the value of S is equal to 3), and δ_{red} and δ_{ox} are the degrees of non-stoichiometry of the OCM during steady cycling at the end of the reduction and oxidation half cycles respectively.

Subtracting Eq. S4 from Eq. S5 leads to the following equation:

$$
N_{OCM, oxygen, usable} = (\delta_{red} - \delta_{ox}) N_{OCM}
$$
 Eq. S6

Substituting Eq. S2 and Eq. S6 into Eq. S1 therefore leads to the following equation for the dimensionless number λ_{O} :

$$
\lambda_O = \frac{(\delta_{red} - \delta_{ox})N_{OCM}}{F_0 t}
$$
 Eq. S7

Verifying λ_0 using different values of δ_{red} - δ_{ox} , t, N_{OCM} and F_o

The simulation results in Table S1 demonstrate that the conversions are dependant only on

the values of $log_{10} p_{O_2}$ ^{mid}, k_{grad} and λ_{o} . For example, a λ_{o} value of 0.5 gives X_{CO} and X_{H_2O} values of ~50% regardless of how λ_0 is derived with changes to δ_{red} – δ_{ox} and N_{OCM} .

Table S1: Conversions determined from the simulation using different values of λ_0 using various δ_{red} – δ_{ox} , F_{O_2} , t and N 0CM values. The values of k_{grad} and $^{log_{10}p_{O_2}$ mid are kept constant at -1.15 and -17.8 respectively. The values of conversion that are shown are those during steady cycling when the difference between $X_{\rm CO}$ and $X_{\text{H}_2\text{O}}$ is < 0.01.

Fig. S1a and Fig. S1d show that there are no noticeable changes to the shapes of the outlet concentration profiles at $\lambda_{\rm O}$ = 1 when using different $^F{\overline{o}}$ and $^{\delta_{red}-\delta_{ox}}$ values. Meanwhile the outlet concentration profile at 60s feed durations compared to 120 s feed durations in

Fig. S1a and Fig. S1d compared to Fig. S1b and Fig. S1c is a half-scaled version of the 120 s profile along the x-axis. This indicates that as expected while a greater volume of H_2 is

conversions and outlet product quality is still determined by the value of λ_0 and the specific $\log_{10} p_{O_2}$ ^{mid} and $k_{\rm grad}$ of the δ - ${}^{p_{O_2}}$ curve.

Fig. S2 shows the outlet concentration profiles corresponding to selected $\lambda_{\rm O}$ values for the optimal δ^{- p_{O_2}} relationship. As expected, $\lambda_{\rm O}$ < 1 results in less available oxygen capacity and gives a decrease in conversions and product quality. For $\lambda_0 \le 0.1$ significant quantities of unreacted feed gas start to be seen in the outlet concentration profiles. At $\lambda_0 = 1 \times 10^{-3}$ it is seen that the inlet streams pass through the reactor almost unreacted with unacceptable product quality, while at a λ_0 value of 1000 almost pure product H₂ and CO₂ can be seen Figure S1: Comparison on the effect on outlet concentration profiles for $\lambda_0 = 1$ when using a) $\delta_{red} - \delta_{ox} =$ 0.0225, F_o = 1.7361 × 10⁻⁶ mol min⁻¹, t = 60s, N_{OCM} = 0.004639 mols, b) δ_{red} – δ_{ox} = 0.0225, F_o = 8.6806 × 10⁻⁷ mol min⁻¹, t = 120s, N 0CM = 0.004639 mols, c) $^{\delta_{red} - \delta_{ox}}$ = 0.0225, F 0 = 1.7361 × 10⁻⁶ mol min⁻¹, t = 120s, N 0CM = 0.009278 mols and d) $^{\hat{\delta}_{red}-\hat{\delta}_{ox}}$ = 0.0449, Fo = 3.4722 × 10⁻⁶ mol min⁻¹, *t* = 60s, $^{N_{OCM}}$ = 0.004639 mols. The $\log_{10} p_{O_2}$ $\frac{log_{10} p_{O_2}$ $\frac{mid}{100}$ are kept constant at -1.15 and -17.8 respectively. The profiles are taken

only limited by the p_{0_2} of the inlet feeds. It would still be possible to achieve high $\log_{10} p_{O_2}$ log₁₀ p_{O_2} _{mid} are not changed, however a greater mass of OCM would need to be used to be to be able to do so which would be more expensive industrially. Alternatively an OCM with a similar δ^{- *P*0}2 relationship but with a larger maximum degree of oxygen non-stoichiometry could be used if it existed.

Figure S2: Outlet concentration profiles determined from the simulation using different values for of the δ - p_{O_2} plot at 1093 K. The values of k_{grad} and $\log_{10} p_{O_2}$ ^{mid} are kept constant at -1.15 and -17.8 respectively. The profiles are taken during steady cycling when the difference between X_{C0} and $X_{H₂0}$ is < 0.01.