# **Supporting Information**

Introducing  $\pi$ -electron-rich aromatic rings into a robust Zr-MOF for efficient natural gas purification and  $C_3H_8/n$ - $C_4H_{10}$  recovery

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*Zr-MOF*; *Breakthrough*; *nature gas*; *gas separation*; n- $C_4H_{10}$  *recovery*.

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#### S1. Materials and Instrumentation

General procedures. All the reagents and solvents were commercially available and directly utilized without further purification. Powder X-ray diffraction (PXRD) was carried out with a Rigaku SmartLab diffractometer (Bragg-Brentano geometry, Cu  $K_{\alpha l}$  radiation,  $\lambda = 1.54178$  Å). Solid-state IR spectra were recorded using Nicolet/Nexus-670 FT-IR spectrometer in the region of 4000-400 cm<sup>-1</sup> using KBr pellets. Thermogravimetric analyses (TGA) were performed on a NETZSCH TG209 system in nitrogen and under 1 atm of pressure at a heating rate of 5 °C min<sup>-1</sup>. 77 K N<sub>2</sub> sorption measurements were conducted using QUADRASORB EVO gas adsorption analyzer. Gas adsorption isotherms for pressures in the range of 0-1.0 bar were obtained by a volumetric method using a Quantachrome autosorb-iQ<sub>2</sub>-MP gas adsorption analyzer. Breakthrough experiments were collected by two different instruments, BSD-MAB (Multi-component Adsorption Breakthrough Curve Analyzer) with mass spectrometer as detector, and a self-built instrument with gas chromatography (FL-9790 plus) as detector.

Synthesis of 6-(4-carboxyphenyl)-2-naphthalenecarboxylic acid (H<sub>2</sub>L). To a solution of methyl 6-bromo-2-napthoate (2.65 g, 10 mmol) in 125 mL of toluene was added the mixture of (4-(methoxycarbonyl)phenyl)boronic acid (2.34 g, 13 mmol) in 30 mL of ethanol, followed by the addition of a solution of Na<sub>2</sub>CO<sub>3</sub> (3.5 g, 33 mmol) in 10 mL water. This solution was degassed using N<sub>2</sub> for 10 min, and then Pd(PPh<sub>3</sub>)<sub>4</sub> (0.5 g, 0.43 mmol) was added. The resulting reaction mixture was stirred at 90 °C under N<sub>2</sub> overnight. The solvent was then removed using rotary evaporation, and the residue was dissolved in CH<sub>2</sub>Cl<sub>2</sub> and washed with water. The organic layer was next dried over MgSO<sub>4</sub>, filtered, concentrated, and purified by silica gel flash column chromatography with an eluent of dichloromethane: petroleum ether = 1:8 (v/v). The product was hydrolyzed by refluxing in 2 M NaOH solution (ethanol : water = 1 : 1) for 48 h followed by acidification with pH = 1 aqueous HCl to afford H<sub>2</sub>L as white solid. Yield = 2.4 g (82.2%). <sup>1</sup>H NMR (DMSO- $d_6$ ,  $\delta$  ppm): 13.08 (s, 2H, COOH), 8.65 (s, 1H, ArH), 8.40 (s, 1H, ArH), 8.24 (d, 1H, ArH), 8.13-8.06 (m, 3H, ArH), 8.04-7.97 (d, 4H, ArH).

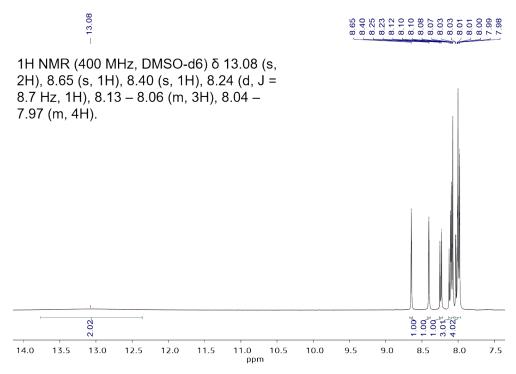


Figure S1. <sup>1</sup>H NMR spectrum of H<sub>2</sub>L.

Synthesis of  $[\mathbf{Zr_6}(\mu_3\text{-OH})_4(\mu_3\text{-O})_4(\mathbf{L})_6]$  ·xGuest (LIFM-233). ZrCl<sub>4</sub> (20.0 mg, 0.086 mmol) and H<sub>2</sub>L (25.1 mg, 0.086 mmol) were mixed with 0.2 mL of trifluoroacetic acid (TFA) in 5 mL of *N*,*N*-dimethylformamide (DMF). To this was added with stirring. The mixture was sealed in a Pyrex tube and heated to 120 °C or 72 h. The colorless block crystals obtained were filtered and washed with DMF. Yield (based on metal source) = 73.6%.

**Sample activation.** The as-synthesized sample of LIFM-233 was soaked in acetone for 3 days with acetone refreshing every 8 hours. Then, the acetone-exchanged sample was activated at 80 °C under vacuum for 10 hours to give the activated LIFM-233.

## S2. Single Crystal X-Ray Crystallography

The single-crystal of LIFM-233 was picked and coated in para tone oil, attached to a glass silk which was inserted in a stainless stick, then transferred to the Rigaku SmartLab diffractometer with the Enhance X-ray Source of Cu radiation ( $\lambda = 1.54178$  Å) using the  $\omega$ - $\phi$  scan technique. The structure was solved by direct methods and refined by full-matrix least squares against  $F^2$  using the SHELXL programs.<sup>2</sup> Hydrogen

atoms were placed in geometrically calculated positions and included in the refinement process using riding model with isotropic thermal parameters: Uiso (H) = 1.2 Ueq (-CH). All the electrons of disordered solvent molecules which cannot be determined, are removed by SQUEEZE routine of PLATON program.<sup>3</sup> Crystal data and refinement parameters are listed in Table S1.

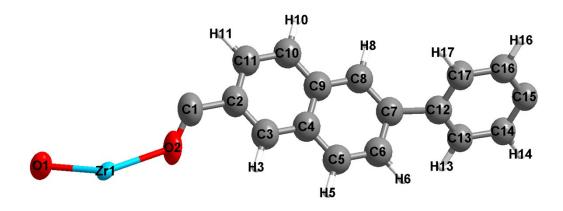
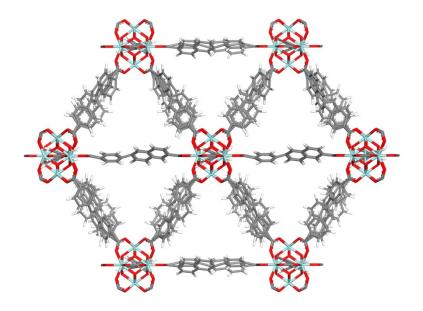
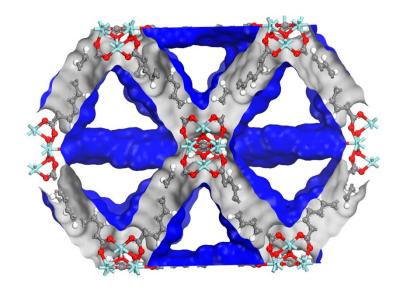


Figure S2. The asymmetric unit of LIFM-233.





**Figure S3.** The structure and corresponding solvent accessible surface in LIFM-233. Structural disorder has been removed for clarity.

# S3. PXRD, TG and IR Analysis

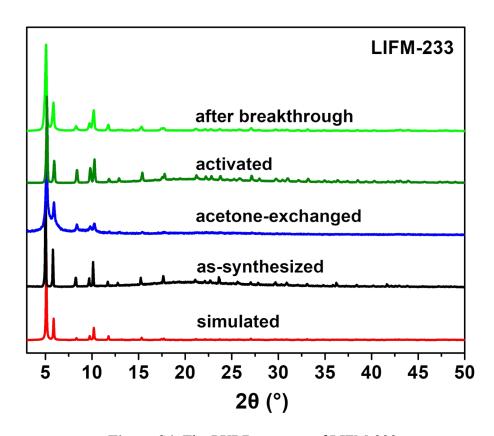


Figure S4. The PXRD patterns of LIFM-233.

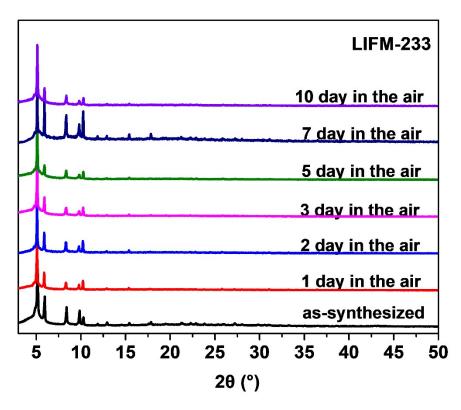
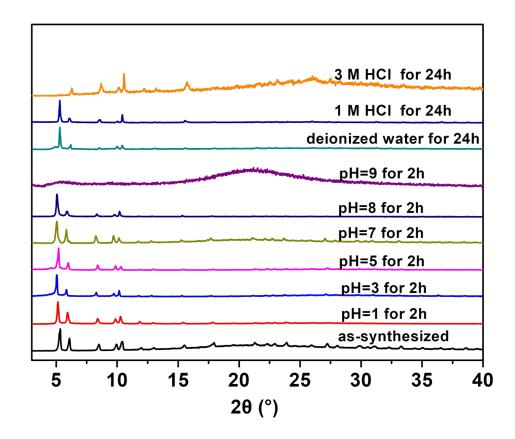


Figure S5. The stability tests of LIFM-233 in the air.



**Figure S6.** The PXRD patterns of LIFM-233 after immersing the samples into aqueous solutions with different pH values.

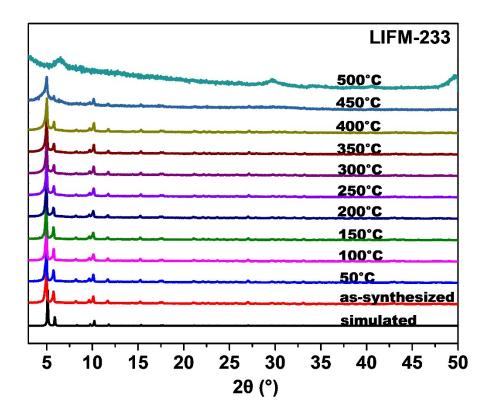


Figure S7. The variable-temperature PXRD patterns of LIFM-233.

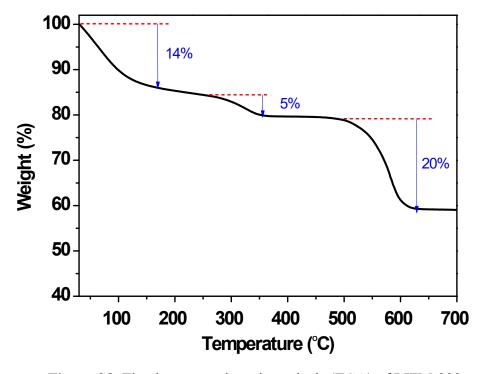


Figure S8. The thermogravimetric analysis (TGA) of LIFM-233.

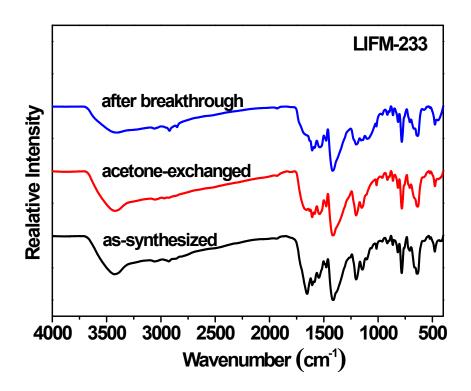


Figure S9. The infrared spectra of LIFM-233.

## S4. Gas Sorption Measurements

Gas Sorption Isotherms: The N<sub>2</sub> gas sorption isotherm of activated LIFM-233 was performed on a QUADRASORB EVO gas adsorption analyzer. Low pressure sorption isotherms of CH<sub>4</sub>, C<sub>2</sub>H<sub>6</sub>, C<sub>3</sub>H<sub>8</sub> and *n*-C<sub>4</sub>H<sub>10</sub> gases were performed on a Quantachrome autosorb-iQ2-MP gas adsorption analyzer. For all isotherms, ultra-high purity He gas was used for the estimation of the free space (warm and cold), assuming that it is not adsorbed at any of the studied temperatures. Their corresponding calculation fittings are plotted.

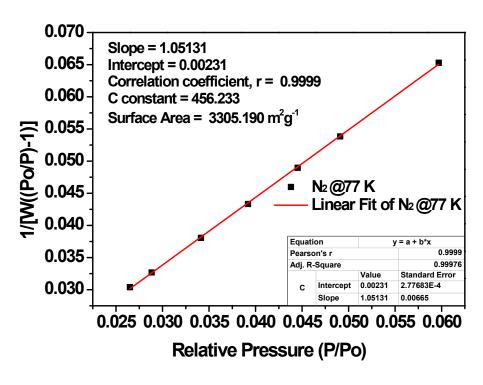
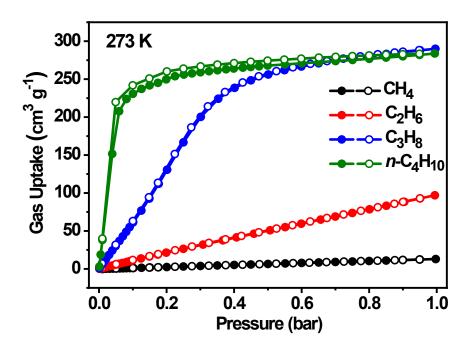


Figure S10. Plot of the linear region for BET equation of activated LIFM-233.



**Figure S11.** CH<sub>4</sub>,  $C_2H_6$ ,  $C_3H_8$  and n- $C_4H_{10}$  sorption isotherms at 273 K for activated LIFM-233.

# **S5.** Isosteric Heats of Gas Adsorption

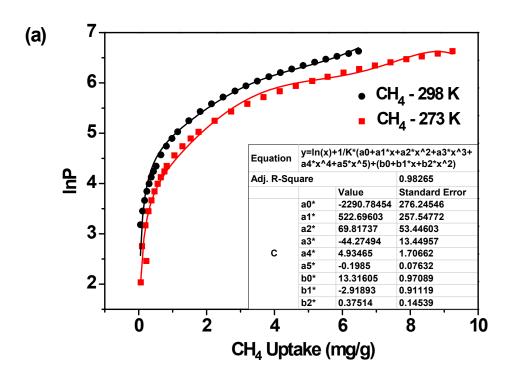
A virial-type<sup>4</sup> expression comprising the temperature-independent parameters  $a_i$  and  $b_j$  was employed to calculate the enthalpies of adsorption for CH<sub>4</sub>, C<sub>2</sub>H<sub>6</sub>, C<sub>3</sub>H<sub>8</sub> and n-C<sub>4</sub>H<sub>10</sub> (at 273 and 298 K) on activated LIFM-233. In each case, the data were fitted using the equation:

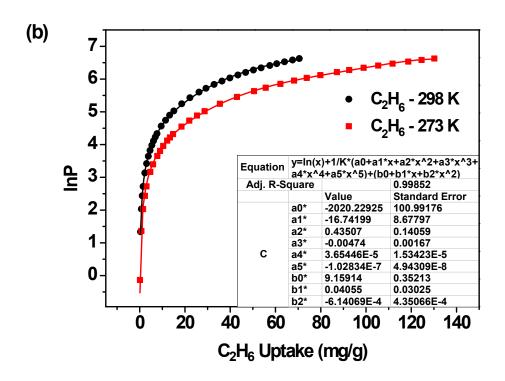
$$\ln P = \ln N + 1/T \sum_{i=0}^{m} a_i N^i + \sum_{i=0}^{n} b_j N^j$$
 (1)

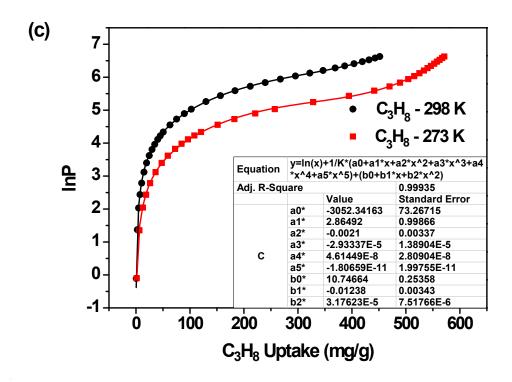
Here, P is the pressure expressed in Torr, N is the amount adsorbed in mmol/g, T is thetemperature in K,  $a_i$  and  $b_j$  are virial coefficients, and m, n represent the number of coefficients required to adequately describe the isotherms (m and n were gradually increased until the contribution of extra added a and b coefficients was deemed to be statistically insignificant towards the overall fit, and the average value of the squared deviations from the experimental values was minimized). The values of the virial coefficients  $a_0$  through  $a_m$  were then used to calculate the isosteric heat of adsorption using the following expression.

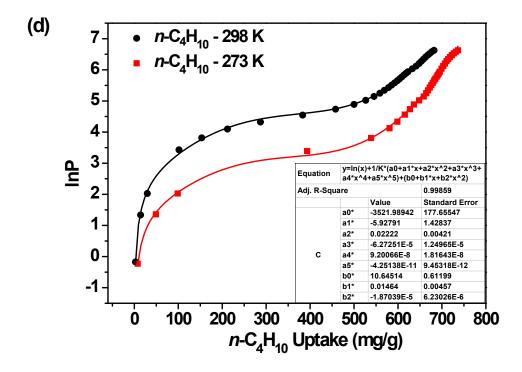
$$Q_{st} = -R\sum_{i=0}^{m} a_i N^i \qquad (2)$$

 $Q_{st}$  is the coverage-dependent isosteric heat of adsorption and R is the universal gas constant. The heat of CH<sub>4</sub>, C<sub>2</sub>H<sub>6</sub>, C<sub>3</sub>H<sub>8</sub> and n-C<sub>4</sub>H<sub>10</sub> sorption for activated LIFM-233 in the manuscript are determined by using the sorption data measured in the pressure range from 0-1 bar (273 K and 298 K), which is fitted by the virial-equation well.









**Figure S12.** (a) CH<sub>4</sub>, (b) C<sub>2</sub>H<sub>6</sub>, (c) C<sub>3</sub>H<sub>8</sub> and (d) *n*-C<sub>4</sub>H<sub>10</sub> virial fitting (lines) of the adsorption isotherms of activated LIFM-233 measured at 273 K and 298 K.

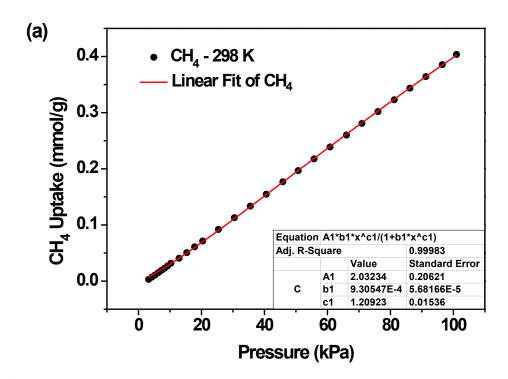
## **S6.** IAST Selectivity

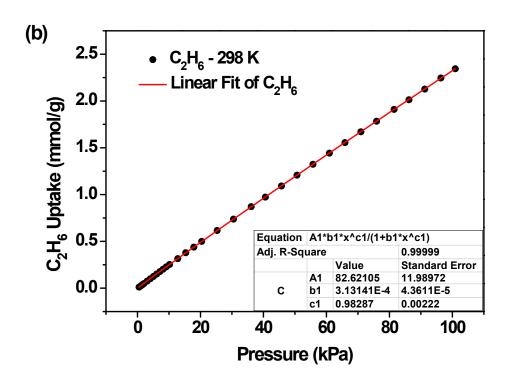
IAST (ideal adsorption solution theory)<sup>5, 6</sup> was used to predict binary mixture adsorption from the experimental pure-gas isotherms. In order to perform the integrations required by IAST, the single-component isotherms should be fitted by a proper model. In practice, several methods to do this are available. We found for this set of data that the single-site Langmuir-Freundlich equation (SSLF) was successful in fitting the data. As can be seen in Figure S12, the model fits the isotherms very well.

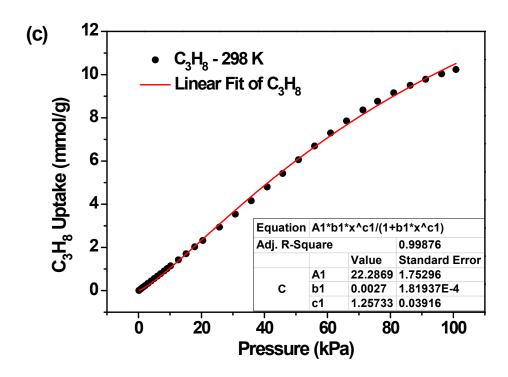
$$q = \frac{q_{m,1}b_1p^{1/n}}{1 + b_1p^{1/n}}$$
 (3)

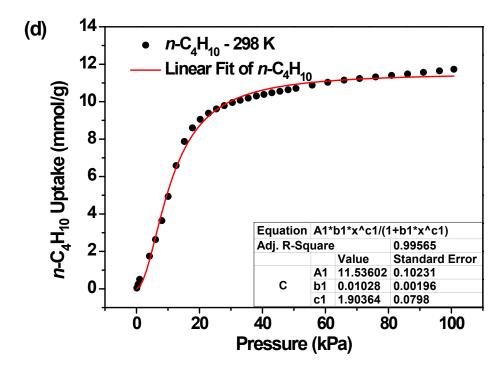
Here, P is the pressure of the bulk gas at equilibrium with the adsorbed phase (kPa), q is the adsorbed amount per mass of adsorbent (mmol/g),  $q_{m,l}$  is the saturation capacities of sites (mmol/g),  $b_l$  is the affinity coefficients of sites (1/kPa), and n represents the deviations from an ideal homogeneous surface. The fitted parameters were then used to predict multi-component adsorption with IAST.

The selectivity  $S_{A/B}$  in a binary mixture of components A and B is defined as  $(x_A/y_A)/(x_B/y_B)$ , where  $x_i$  and  $y_i$  are the mole fractions of component i (i = A, B) in the adsorbed and bulk phases, respectively.









**Figure S13.** Gas adsorption isotherms and the single-site Langmuir-Freundlich fit lines of CH<sub>4</sub>, C<sub>2</sub>H<sub>6</sub>, C<sub>3</sub>H<sub>8</sub> and *n*-C<sub>4</sub>H<sub>10</sub> in activated LIFM-233 at 298 K

### S7. Breakthrough Experiments and Recovery

Transient breakthrough experiments for the separation of CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub>/C<sub>3</sub>H<sub>8</sub> (85:10:5, v/v/v) were carried out in a fixed bed. The gas flow rates were regulated by mass flow controllers. The column (6 mm inner diameter × 150 mm) contained 0.8 g of pre-activated sample. Before filled in the column, the sample was activated at 333 K for 10 h under vacuum. After sample filling, the column was purged with an He flow (20 mL/min) for 2 h. Then the CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub>/C<sub>3</sub>H<sub>8</sub> gas mixture with 3 mL min<sup>-1</sup> was introduced to the column. The outlet composition was continuously monitored by FULI GC9790 Plus gas chromatograph until a complete breakthrough was achieved. The sample was regenerated with an He flow (20 mL/min) at 333 K for 2 h until all gas signals disappeared before each cyclic experiment.

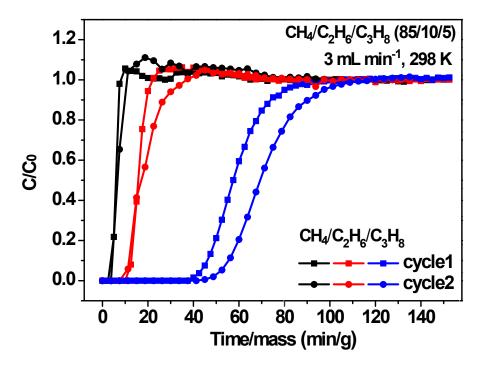
Transient breakthrough experiments for the separation of CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub>/N<sub>2</sub>/C<sub>3</sub>H<sub>8</sub>/*n*-C<sub>4</sub>H<sub>10</sub> (85:9:2:3:1, v/v/v/v/v) were carried out in a fixed bed. The column (6 mm inner diameter × 150 mm) contained 0.5 g activated sample (the same batch sample for ternary gas saparation). Before filled in the column, the sample was activated at 333 K for 10 h under vacuum conditions. After sample filling, the column was purged with an He flow (30 mL min<sup>-1</sup>) for 2 h. Then the CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub>/N<sub>2</sub>/C<sub>3</sub>H<sub>8</sub>/*n*-C<sub>4</sub>H<sub>10</sub> gas mixture with 10 mL min<sup>-1</sup> was introduced to the column. The outlet composition was continuously monitored by the mass spectrometer of BSD-MAB multi-constituent adsorption breakthrough curve analyzer until a complete breakthrough was achieved. The sample was regenerated with an He flow (30 mL/min) at 333 K for 2 h until all gas signals disappeared before each cyclic experiment.

Recovery of  $C_3H_8$  and n- $C_4H_{10}$  were carried out. An He stream was flowed over the packed column with flow rate of 20 or 30 mL min<sup>-1</sup> at 60 °C, in which the eluted gas was monitored by a gas chromatograph (for ternary mixture) or a mass spectrometer (for five-component mixture). The purity of the recovered  $C_3H_8$  and n- $C_4H_{10}$  is calculated based on the following equation.

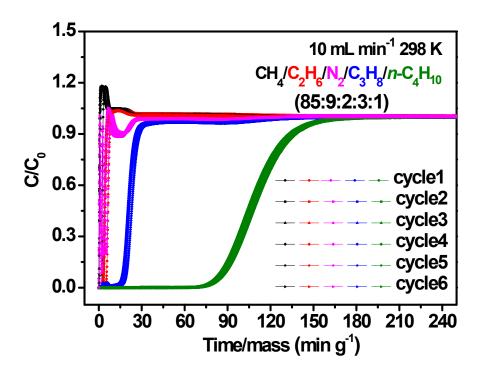
Purity(
$$C_3H_8$$
) =  $\frac{S_{C_3H_8}}{S_{C_3H_8} + S_{C_2H_6} + S_{CH_4}} \times 100\%$  (4)

Purity
$$(n-C_4H_{10}) = \frac{S_{C_3H_8}}{S_{n-C_4H_{10}} + S_{C_3H_8} + S_{C_2H_6} + S_{CH_4}} \times 100\%$$
 (5)

Where S is the integral area of the region bounded by the desorption curve of CH<sub>4</sub>,  $C_2H_6$ ,  $C_3H_8$  or n- $C_4H_{10}$  with the X-axis, respectively.



**Figure S14.** Cycling column breakthrough tests for a  $CH_4/C_2H_6/C_3H_8$  (85:10:5, v/v/v) mixture with activated LIFM-233.

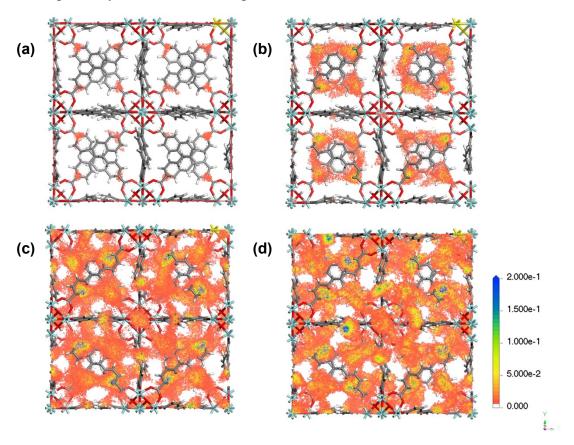


**Figure S15.** Cycling column breakthrough tests for a  $CH_4/C_2H_6/N_2/C_3H_8/n$ - $C_4H_{10}$  (85:9:2:3:1, v/v/v/v/v) mixture with activated LIFM-233.

### **S8.** Theoretical Calculations

Adsorption site simulations by grand canonical Monte Carlo simulations: The grand canonical Monte Carlo (GCMC) simulations were performed with the Sorption module of Materials Studio.<sup>7</sup> The unit cell of LIFM-233 was used for calculations. After transformed to PI space group, hydrogen atoms were added to the Zr cluster for charge balance and the coordinates of all Zr atoms were fixed. Then this initial structure was first optimized using Forcite module with universal force filed (UFF). The convergence tolerances of energy, force and displacement were  $2.0 \times 10^{-5}$  kcal mol<sup>-1</sup>,  $1 \times 10^{-3}$  kcal mol<sup>-1</sup> Å<sup>-1</sup>, and  $1 \times 10^{-5}$  Å, respectively.  $CH_4/C_2H_6/C_3H_8/n$ - $C_4H_{10}$  molecules were directly optimized with Dmol<sup>3</sup>. The partial charge of  $CH_4/C_2H_6/C_3H_8/n$ - $C_4H_{10}$  were calculated using the ESP method. The previously described optimized LIFM-233 primitive cell and  $CH_4/C_2H_6/C_3H_8/n$ - $C_4H_{10}$  was used. Atoms in LIFM-233 were fixed during GCMC simulations. The density distributions of the gases in the MOF were

calculated using the fixed pressure task mode of Sorption module under 298 K and 100 kPa (fugacity). The equilibration steps, production steps and temperature were  $1 \times 10^6$ ,  $1 \times 10^7$ , and 298 K, respectively. The Dreiding force field was used and the parameters of Zr were adopted from UFF. The van der Waals interactions with a cutoff 18.5 Å were depicted by the Lennard-Jones potential.



**Figure S16.** Density distribution of  $CH_4$  (a),  $C_2H_6$  (b),  $C_3H_8$  (c) and n- $C_4H_{10}$  (d) in activated LIFM-233 at 298 K and 100 kPa.

### S9. Tables

Table S1. Physical parameters of selected gas adsorbates.<sup>8</sup>

Adsorbate	Molecule size /Å <sup>3</sup>	Kinetic diameter/Å	Polarizability ×10 <sup>25</sup> /cm <sup>3</sup>	Dipole moment ×10 <sup>18</sup> /esu	Quadruple moment ×10 <sup>26</sup> /esu
				cm	cm <sup>2</sup>
$\mathrm{CH_4}$	$3.76 \times 3.83 \times 3.99$	3.758	25.93	0	0
$C_2H_6$	$4.08 \times 4.29 \times 4.72$	4.443	44.3-44.7	0	0.65
$C_3H_8$	$4.02 \times 4.79 \times 6.20$	4.3-5.118	62.9-63.7	0.084	<del></del>
n-C <sub>4</sub> H <sub>10</sub>	4.02×4.61×7.38	4.687	82	0.05	

 Table S2. Crystallographic data of LIFM-233.

MOFs	LIFM-233				
CCDC	2338023				
Empirical formula	$C_{108} H_{60} O_{32} Zr_6$				
Formula weight	2416.88				
Temperature[K]	240.00(10)				
Radiation Wavelength [Å]	1.54178 (Cu <i>Kα</i> )				
Crystal system	cubic				
Space group	Fm-3 $m$				
a/b/c [Å]	30.0127(4)				
$\alpha/\beta/\gamma[deg]$	90				
$V[\mathring{A}^3]$	27034.3(11)				
Z	4				
$ ho_{ m calc}[ m g\ cm^{-3}]$	0.594				
$\mu \ [\mathrm{mm}^{\text{-}1}]$	2.090				
F (000)	4816.0				
Crystal size [mm <sup>3</sup> ]	$0.2 \times 0.2 \times 0.2$				
20 range for data collection [deg]	12.856 to 80.67				
Index ranges	$-9 \le h \le 19, -7 \le k \le 20, -1 \le 1 \le 25$				
Reflections collected	1672				
Independent reflections	462 [ $R_{int} = 0.0209$ , $R_{sigma} = 0.0166$ ]				
Data/restraints/parameters	462/320/137				
Goodness-of-fit on F <sup>2</sup>	1.092				
$R_1$ , $wR_{2a}$ [ $I \ge 2\sigma(I)$ ]	0.0426, 0.1080				
$R_1$ , $wR_{2a}$ [all data]	0.0490, 0.1147				
Largest diff. peak/hole [e. Å-3]	0.23/-0.33				

<sup>&</sup>lt;sup>a</sup>  $R_1 = \Sigma ||F_o| - |F_c||/|F_o|$ ;  $wR_2 = [\Sigma w(\Sigma F_o^2 - F_c^2)^2/\Sigma w(F_o^2)^2]^{1/2}$ .

**Table S3.** Comparison of selectivities and adsorption capacities for LIFM-233 with previously reported top-performing MOFs.

Adsorbent	Adsorption selectivity		Static adsorption capacity (cm <sup>3</sup> g <sup>-1</sup> )				Т
Adsorbent	C <sub>2</sub> H <sub>6</sub> /CH <sub>4</sub>	C <sub>3</sub> H <sub>8</sub> /CH <sub>4</sub>	CH <sub>4</sub>	C <sub>2</sub> H <sub>6</sub>	C <sub>3</sub> H <sub>8</sub>	<i>n</i> -C <sub>4</sub> H <sub>10</sub>	(K)
LIFM-233	6.9	98.7	9.0	52.5	229.3	262.8	298
MgMOF-74 <sup>9-11</sup>	-	-	24.8	147.8	161.3	-	298
UIO-67(Zr) <sup>10</sup>	8.1 <sup>b</sup>	73.7 <sup>b</sup>	10.1	67.2	183.7	-	298
UIO-66(Zr) <sup>12, 13</sup>	-	71.5	11.2	51.5	89.6	100.8	298
ECUT-Th-10 <sup>13</sup>	-	54.5	9.4	38.5	64.7	60.3	298
Fe <sub>2</sub> (dobdc) <sup>14</sup>	32 <sup>b</sup>	-	17.2	112.0	127.0	-	313
PAN-p1 <sup>15</sup>	16.9	129.3	20.6	84.2	114.5	-	298
0.3Gly@HKUST-1 <sup>16</sup>	12.6	173.5	22.8	144.9	174.7	-	298
NKU-FlexMOF-1a <sup>17</sup>	-	-	11.3	69.9	65.7	70.8	298
Ni(TMBDC)(DABCO) <sub>0.5</sub> <sup>18</sup>	29 <sup>b</sup>	274 <sup>b</sup>	35.8	130.1	124.1		298
UTSA-35a <sup>19</sup>	8	80	9.5	53.7	73.2	-	296
CoMOF-74 <sup>11, 20</sup>	26.0	290.0	33.5	168.8	136.1	-	296
RT-MIL-100(Fe) <sup>21</sup>	6	33.3	8.1	49.7	151.9	-	298
MIL-101-Cr <sup>22</sup>	22.5	84.3	11.0	35.6	75.0	-	298
MIL-142A <sup>23</sup>	13.7	1300.0	12.1	85.6	119.2		298
C-PVDC-800 <sup>24</sup>	74.9	3387.2	34.5	118.5	115.8		298
CAU-3-NDCA <sup>25</sup>	8.4	879.9	7.7	52.9	177.8		298
BSF-2 <sup>26</sup>	53.0	2609.0	5.4	27.3	39.6		298
TIFSIX-Cu-TPA <sup>27</sup>	16.2	68.6	15.2	98.6	110.0		298
Ni(HBTC)(bipy) <sup>28</sup>	27.5	1857.0	20.8	131.0	138.4		298
Co-MOF <sup>29</sup>	26.0 <sup>b</sup>	290.0 <sup>b</sup>	16.6	58.6	59.4		298
CTGU-15 <sup>30</sup>	5.2	170.7	8.9	47.7	271.7		298
JUC-100 <sup>31</sup>	10.7	82.3	10.2	92.1	136.0		298
Iso-MOF-4 <sup>32</sup>	8.5	80.0	13.4	114.0	240.9		298
InOF-1 <sup>33</sup>	17.0	90.0	14.3	92.7	95.2		298

<sup>&</sup>lt;sup>a</sup> Unless otherwise stated, the data was calculated under the condition of equimolar binary mixtures and 1 bar;

<sup>&</sup>lt;sup>b</sup> IAST selectivity calculated under the condition of  $C_2H_6/CH_4 = 10/85$  or  $C_3H_8/CH_4 = 5/85$  and 1 bar.

**Table S4.** Comparison of **LIFM-233** with various other adsorbents for  $C_1$ - $C_4$  hydrocarbon separation in terms of the  $CH_4$  productivity,  $C_2H_6/C_3H_8/n$ - $C_4H_{10}$  capture capacity, and recovered  $C_3H_8/n$ - $C_4H_{10}$  purity based on a ternary  $CH_4/C_3H_8/n$ - $C_4H_{10}$  or quinary  $CH_4/C_2H_6/N_2/C_3H_8/n$ - $C_4H_{10}$  transient adsorption-desorption breakthrough experiment.

Adsorbent	Flow rate of gas mixture	CH <sub>4</sub> productivity (mmol g <sup>-1</sup> )	Dynamic adsorption  uptake  (mmol g <sup>-1</sup> )			Recovery purity	
			$C_2H_6$	C <sub>3</sub> H <sub>8</sub>	<i>n</i> -C <sub>4</sub> H <sub>10</sub>	$C_3H_8$	<i>n</i> -C <sub>4</sub> H <sub>10</sub>
LIFM-233b	10	1.17	0.12	0.33	0.48	92.7	94.0
LIFM-233	3	1.23	0.25	0.50	-	91.6	-
C-PVDC-800 <sup>24</sup>	2	15.72	-	3.02	-	-	-
CAU-3-NDCA <sup>25</sup>	10	-	0.25	0.446	-	-	-
BSF-2 <sup>26</sup>	4	-	-	0.759	-	-	-
TIFSIX-Cu-	4	5	-		-	-	-
Ni(HBTC)(bipy) <sup>28</sup>	10	-	1.21	3.0	-	-	-
Co-MOF <sup>29</sup>	2	1.59	0.78	0.50	-	-	-
MIL-101-Cr <sup>22</sup>	2	-	0.25	0.60	-	-	-
MIL-101-Fe <sup>22</sup>	3	-	0.49	0.29	-	-	-
CTGU-15 <sup>30</sup>	2	-	-	0.38	-	-	-

 $<sup>^{\</sup>rm a}$  Unless otherwise stated, the data was calculated under the condition of  $C_3H_8/C_2H_6/CH_4$  (5:10:85, v/v/v) and 1 bar;

 $<sup>^</sup>b$  The data was calculated under the condition of CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub>/N<sub>2</sub>/C<sub>3</sub>H<sub>8</sub>/n-C<sub>4</sub>H<sub>10</sub> (85:9:2:3:1, v/v/v/v) and 1 bar.

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