

## Supplementary material

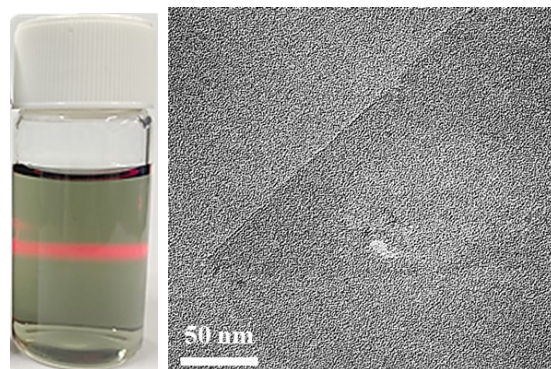


Fig. S1. Digital photograph and TEM image of MXene nanosheet. The TEM image shows the exfoliated single-layer MXene nanosheet with several hundred nanometers in lateral size.

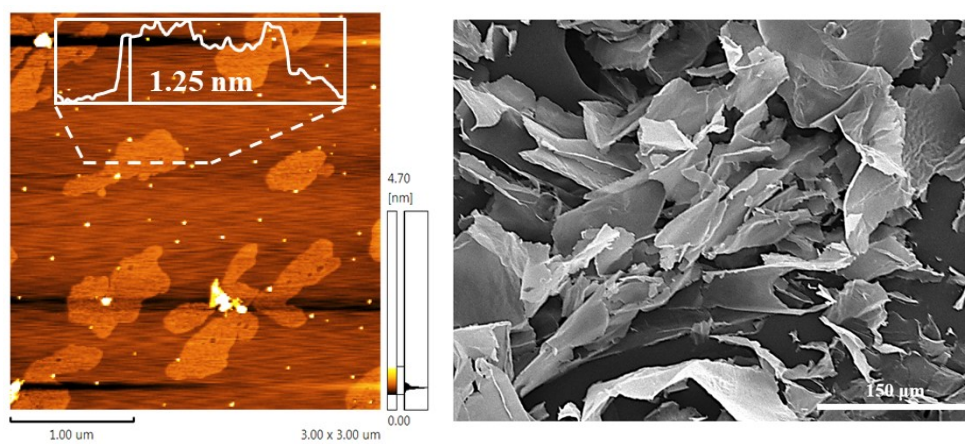


Fig. S2. AFM and SEM images of MXene nanosheet.

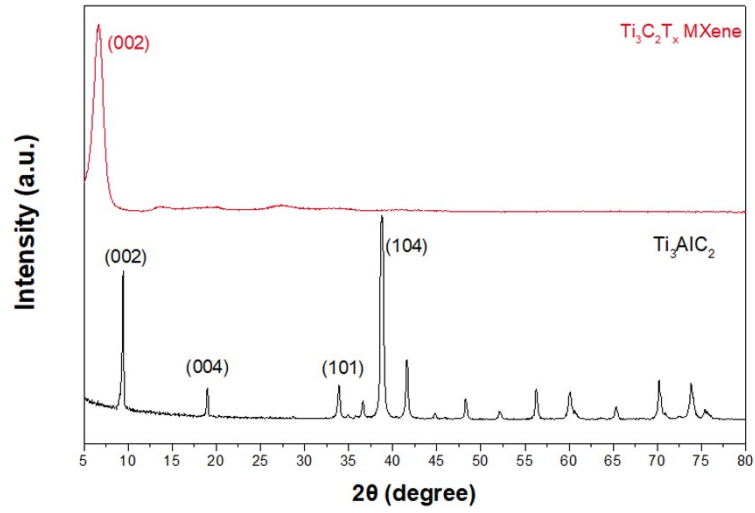


Fig. S3. XRD spectra of  $\text{Ti}_3\text{AlC}_2$  and  $\text{Ti}_3\text{C}_2\text{T}_x$  MXene.

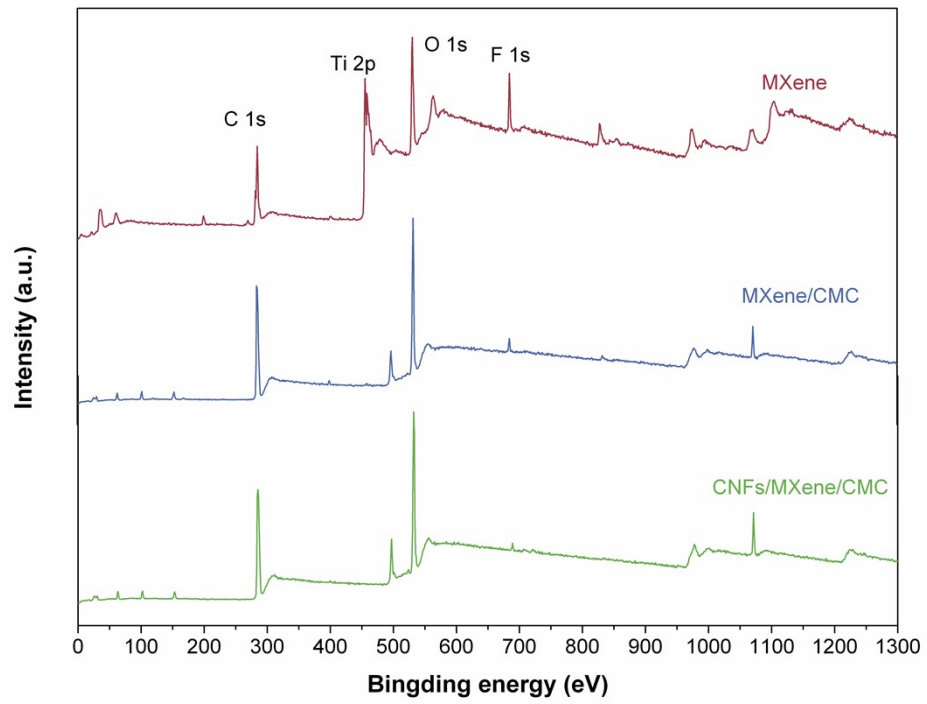


Fig. S4. XPS spectra of pure MXene, MXene/CMC, and CNFs/MXene/CMC.

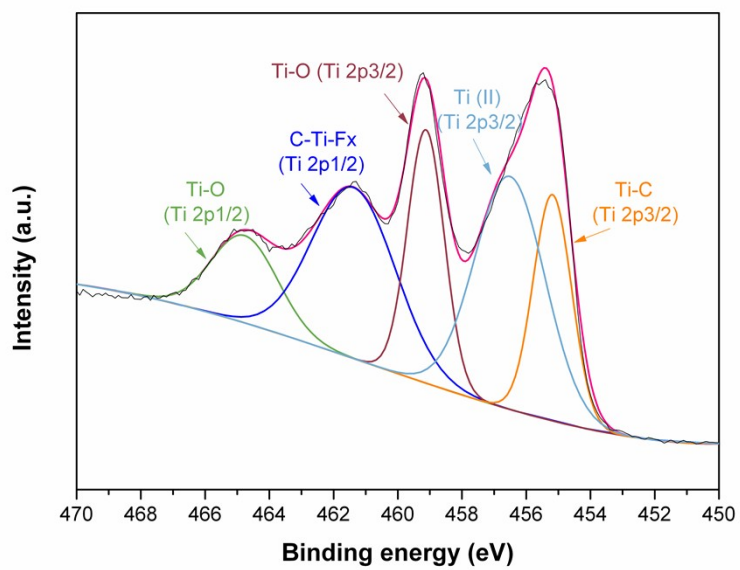


Fig. S5. Ti 2p XPS spectra of MXene.

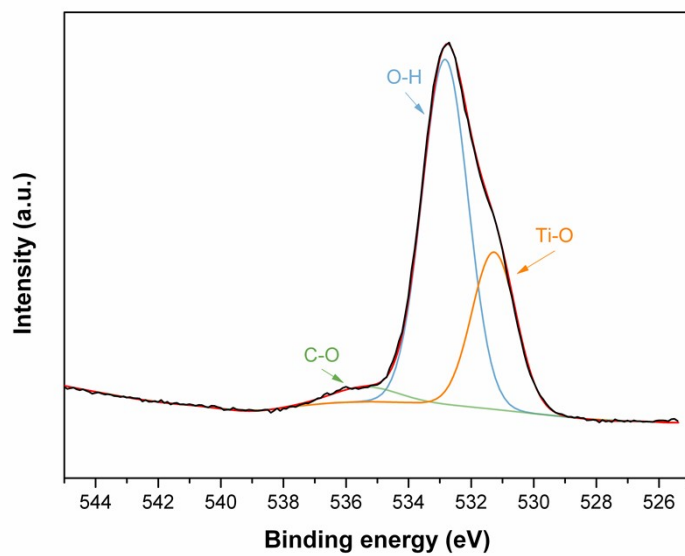


Fig. S6. O 1s XPS spectra of MXene

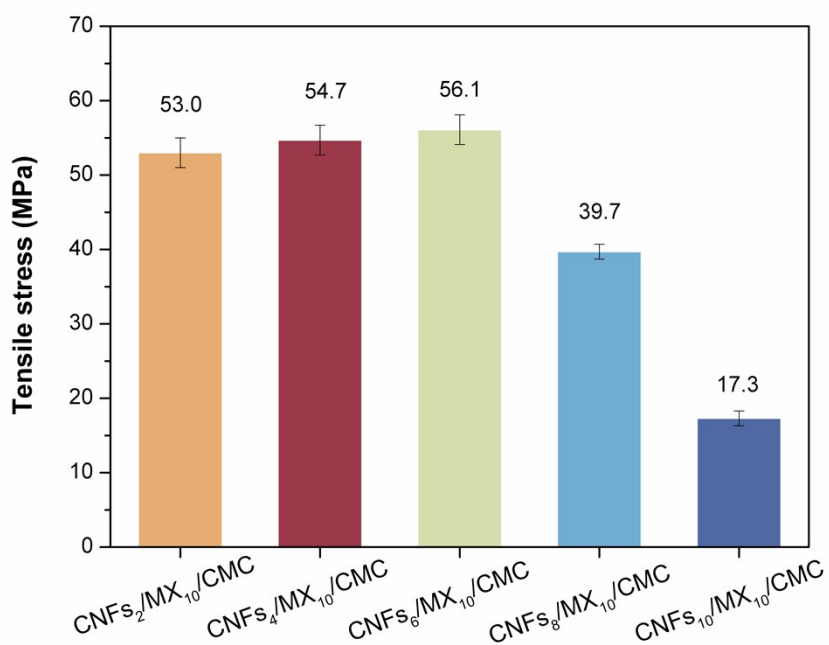


Fig. S7. Tensile stress of CNFs/MXene/CMC films containing 0, 2, 4, 6, 8 and 10 wt% CNFs.

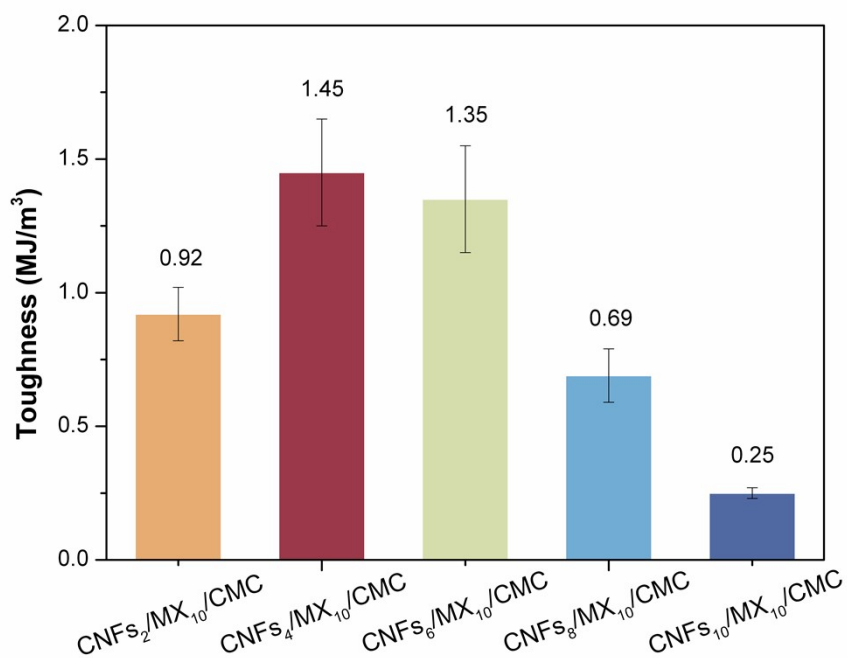


Fig. S8. Toughness of CNFs/MXene/CMC films containing 0, 2, 4, 6, 8 and 10 wt% CNFs.

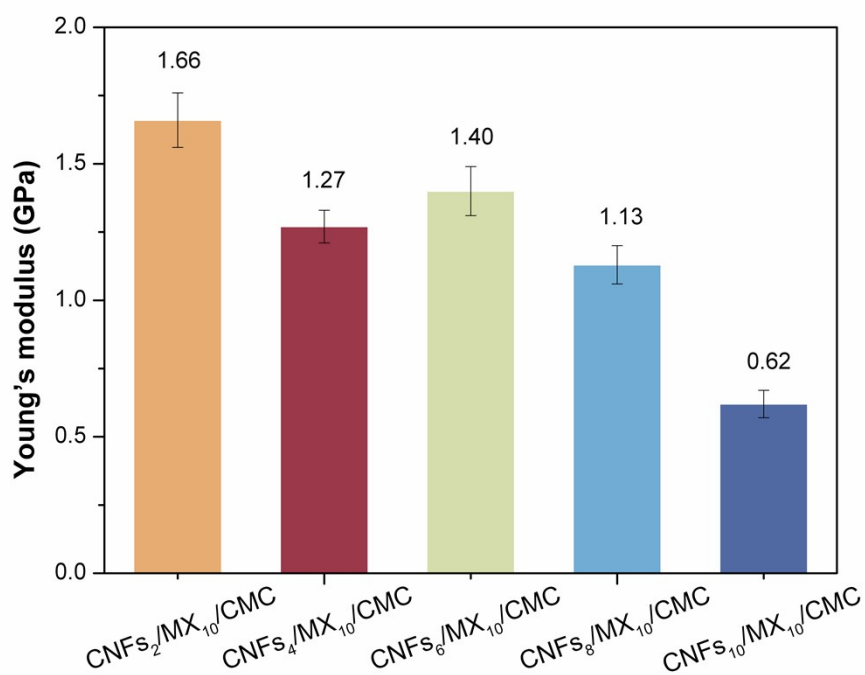


Fig. S9. Young's modulus of CNFs/MXene/CMC films containing 0, 2, 4, 6, 8 and 10 wt% CNFs.

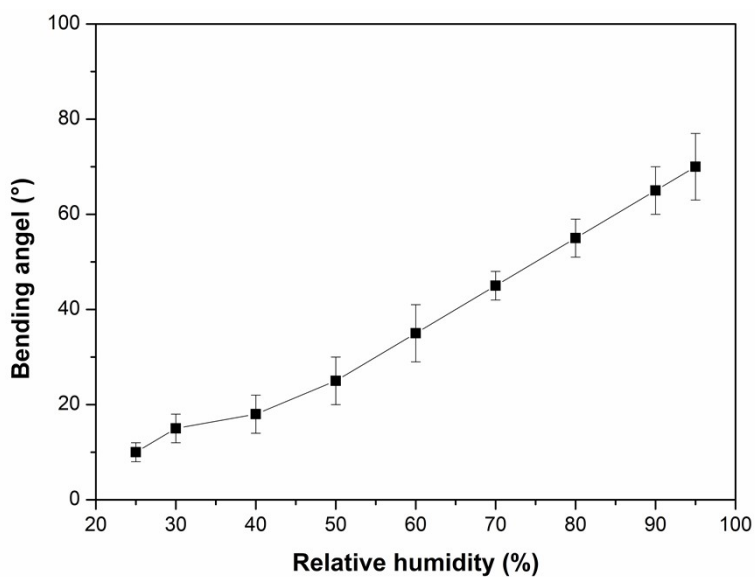


Fig. S10. The maximum bending angle of the pure MXene film at various relative humidity.

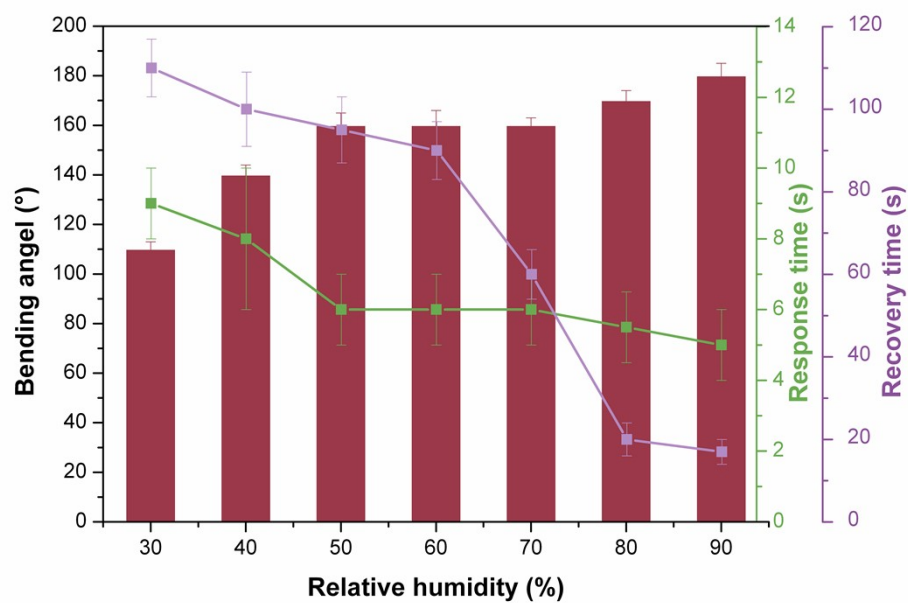


Fig. S11. Bending angles, response times and recovery times of MX<sub>10</sub>/CMC film actuator at different relative humidity

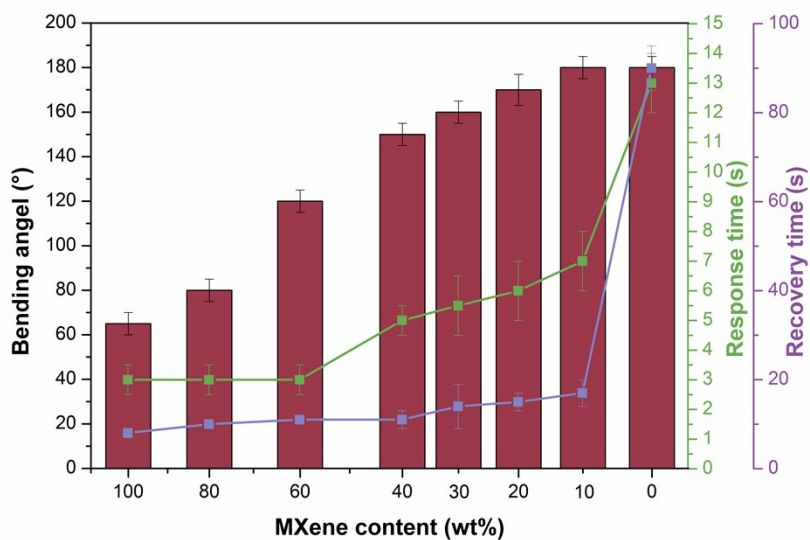


Fig. S12. Bending angles, response times and recovery times of MXene/CMC film actuators with different content of CMC at 95% relative humidity

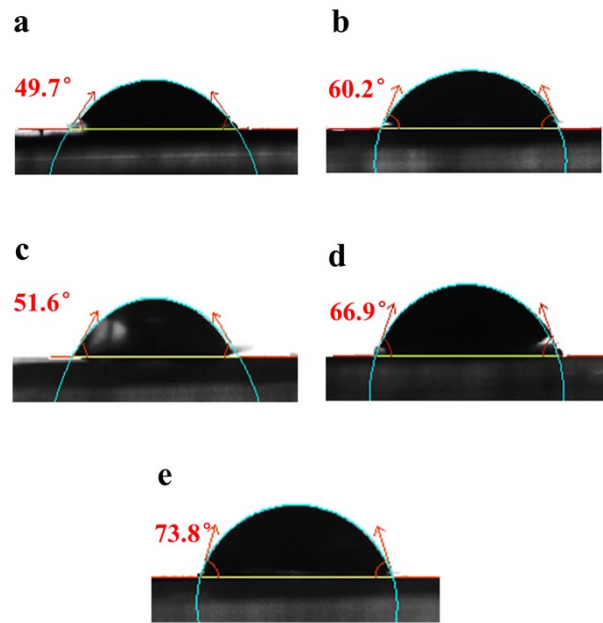


Fig. S13. Contact angle of different film (a) CMC, (b) MXene, (c) MX<sub>10</sub>/CMC, (d) CNFs<sub>6</sub>/MX<sub>10</sub>/CMC-top, and (e) CNFs<sub>6</sub>/MX<sub>10</sub>/CMC-bottom

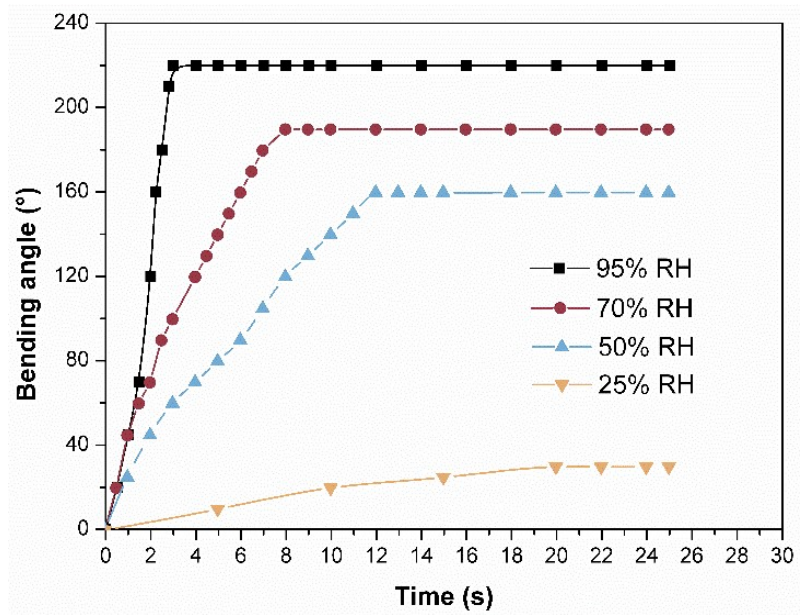


Fig. S14. The bending processes of the CNFs<sub>6</sub>/MX<sub>10</sub>/CMC composite film under different relative humidity



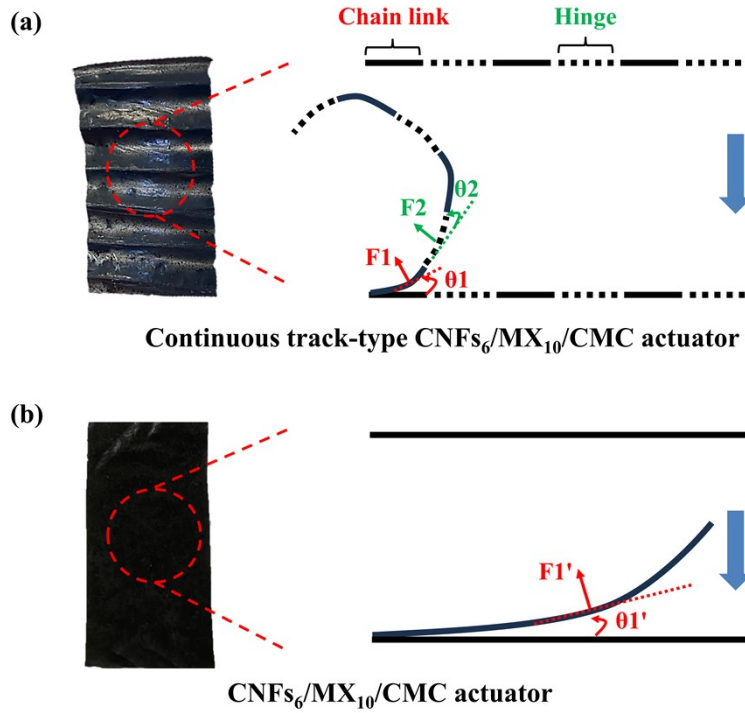


Fig. S15. Synchronous movement of bending angles of (a) continuous track-type and (b) flat CNFs<sub>6</sub>/MX<sub>10</sub>/CMC actuator.

The relationship between deformation and force can be written as Equation (1):<sup>1</sup>

$$L\varepsilon = F/k_{eq} \quad (1)$$

where  $L$  is the length,  $\varepsilon$  is the strain,  $F$  is the Von mises stress applied to the structure, and  $k_{eq}$  is the equivalent stiffness coefficient.

Based on the finite element simulation results, it is evident that due to the similar material compositions of the flat and continuous track-type (chain link section) CNFs<sub>6</sub>/MX<sub>10</sub>/CMC actuators, the Von Mises stresses generated by the humidity change are almost identical and are denoted as  $F1$  and  $F1'$  respectively. Additionally, the force on the hinge section of the continuous track-type film, which is not uniformly distributed due to its anisotropic structure, is denoted as  $F2$ . The bending angles of the corresponding deformations resulting from the stresses are denoted as  $\theta1$ ,  $\theta1'$ , and  $\theta2$ , respectively.

The bending angle of a continuous track-type CNFs<sub>6</sub>/MX<sub>10</sub>/CMC actuator is determined by the deformation of neighboring sections. For one unit cell in periodic structures, the position of the end of the continuous track-type CNFs<sub>6</sub>/MX<sub>10</sub>/CMC actuator in the coordinate system can be expressed as Equation (2):

$$\begin{cases} X=0; \\ Y=L_1\sin\theta_1 + L_2\sin(\theta_1 + \theta_2) + \dots + L_n\sin(\theta_1 + \theta_2 + \dots + \theta_n); \\ Z=L_1\cos\theta_1 + L_1\cos(\theta_1 + \theta_2) + \dots + L_n\cos(\theta_1 + \theta_2 + \dots + \theta_n). \end{cases} \quad (2)$$

The position of the end of a flat CNFs<sub>6</sub>/MX<sub>10</sub>/CMC actuator in the coordinate system can be expressed as Equation (3):

$$\begin{cases} X'=0; \\ Y'=L\sin\theta_1'; \\ Z'=L\cos\theta_1', \end{cases} \quad (3)$$

where  $L$  is the length,  $\theta$  is the bending angle.

Based on the results of finite element simulations and position calculations in the coordinate system, the continuous track-type actuator, owing to its distinctive structure of anisotropic film with periodic structures, exhibits a significantly larger bending angle compared to the flat one.

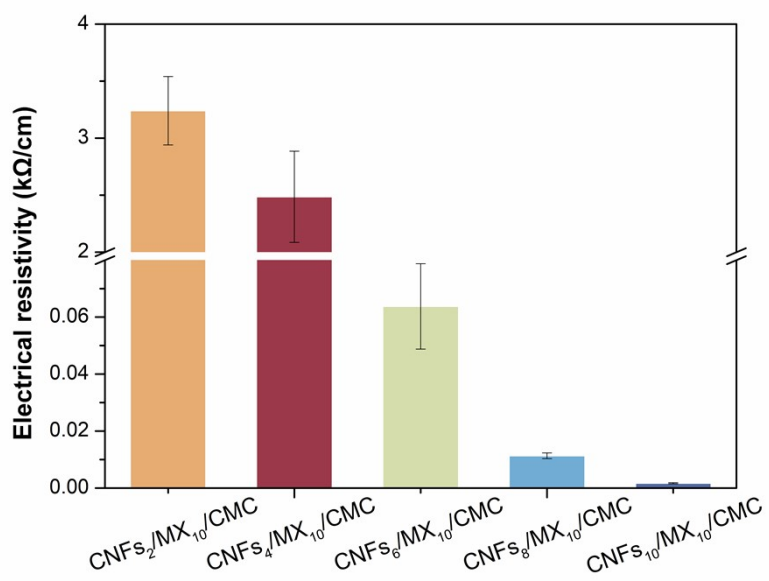


Fig. S16. Electrical resistivities of the CNFs/MX<sub>10</sub>/CMC composite film with different content of CNFs.

Table S1. The mechanical properties of films

Sample	Tensile strength (MPa)	Strain breaking (%)	Toughness (MJ/m <sup>3</sup> )	Young's modulus (GPa)
MXene	12.7±1.6	1.03± 0.05	0.050±0.003	1.3±0.2
CMC	93.3±2.1	7.34±0.06	4.49±0.68	1.28±0.1
MX <sub>10</sub> /CMC	128.6±10.1	5.61±0.08	4.20±0.63	2.30±0.4
MX <sub>20</sub> /CMC	105.7±5.8	4.57±0.04	2.49±0.32	2.23±0.3
MX <sub>40</sub> /CMC	68.4±3.6	2.90±0.06	1.01±0.02	2.10±0.3
MX <sub>60</sub> /CMC	29.1±1.9	2.42±0.03	0.23±0.01	1.21±0.1
CNFs <sub>2</sub> /MX <sub>10</sub> /CMC	53.0±2.3	3.22±0.07	0.92±0.12	1.66±0.1
CNFs <sub>4</sub> /MX <sub>10</sub> /CMC	54.7±2.1	4.31±0.08	1.45±0.19	1.27±0.06
CNFs <sub>6</sub> /MX <sub>10</sub> /CMC	56.1±1.9	4.14±0.08	1.35±0.18	1.4±0.09
CNFs <sub>8</sub> /MX <sub>10</sub> /CMC	39.7±1.4	3.53±0.04	0.69±0.14	1.13±0.07
CNFs <sub>10</sub> /MX <sub>10</sub> /CMC	17.3±1.2	2.84±0.03	0.25±0.02	0.62±0.05

Table S2. Comparison of MXene-based humidity actuators

Materials	Relative humidity difference (%)	Bending angle (°)	Response time/Recovery time (s)	Reference
GO/MXene	40-70	-100-245	20/20	2
MXene/CNF/PDA/BOPP	40-90	0-180	28/28	3
PDMM/BCNF	$\Delta$ 40	176	1.6/3.8	4
MXene-graphene oxide film	40-90	160	5/19	5
Polydopamine-treated reduced graphene oxide/MXene film	$\Delta$ 45	148	1/3	6
MXene/cellulose/PSSA composite membrane	20-97	28-130	15/20	7
CMC/MXene/Al <sup>3+</sup> composite film	$\Delta$ 20- $\Delta$ 80	180	2/2.3	8
BC/GO/MXene composite film	$\Delta$ 50	116	4/4	9
Continuous track-type CNFs/MXene/CMC	20-95	0-360	1.2/4.9	This work

GO: graphene oxide; CNF: cellulose nanofibrils; PDA: p-Phenylenediamine; BOPP: bidirectional oriented polypropylene; PDMM/BCNF: Polydopamine modified MXene/bacterial cellulose nanofiber; PSSA: polystyrene sulfonic acid; BC: Bacterial cellulose

## References

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