Supporting Information

Achieving low dielectric constant and high thermal conductivity polymer composites by using larger POSS functionalized boron nitride nanosheets

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1. Experimental Section

Preparation of hydroxylated boron nitride nanosheets (BN-OH). The title material was prepared by exfoliating commercial *h*-BN through hydroxide-assisted ball milling using a vertical planetary ball mill.¹ The specific operation was as follows: *h*-BN (2 g) and NaOH aqueous solution (2 M) were added into a zirconia ball mill jar with zirconia balls at ball-to-powder ratio of 50:1, and the mixture underwent milling at 500 rpm for 24 h. Subsequently, the ball-milled mixture was centrifuged at 3000 rpm for 30 min to remove unexfoliated bulk boron nitride. The resulting solid was washed three times with HCl (0.1 M) solution and deionized water to eliminate residual NaOH. After drying in a vacuum oven at 70 °C for 24 h, BN-OH was obtained as a white powder. Yield: 20%.

Instrumentation and Characterizations. ¹H NMR spectra were acquired in CDCl₃ using a Bruker 400 MHz NMR spectrometer at room temperature. Fourier transform infrared (FT-IR) spectra were recorded on a Nicolet 6700 spectrometer in attenuated total reflection model and ransmission

mode. Thermo gravimetric analysis (TGA) was tested on a TA Q500 thermo-analyzer from room temperature to 600 °C at a heating rate of 10 °C min⁻¹ under nitrogen condition. Thermal mechanical analyzer (TMA) was measured on a TA Q400EM instrument using tension mode with a pre-stress of 0.01 N and a heating rate of 5 °C min⁻¹. The atomic force microscope (AFM) images of surface morphology were measured on a Dimension Icon (Bruker, America) in Tapping mode in a 20 μ m \times 20 µm area. Scanning electron microscope (SEM) images were recorded on a Nova NanoSEM 450 field emission SEM. The accelerating voltage was 15 kV and all samples were sputter-coated with a thin layer of gold before characterization. Transmission electron microscope (TEM) images were recorded on a Thermo Scientific Talos F200i TEM instrument with an accelerating voltage of 80 kV. Water contact Angle (WCA) was measured with a Kruss DSA25 instrument at ambient temperature. The water drop volume in each test was $2 \mu L$, and the WCA value was calculated from three measurements. Wide-angle X-ray diffraction (WAXD) was performed on a Rigaku Ultima IV X-ray diffractometer with a Cu K α radiation (40 kV and 40 mA) and in the diffraction angle (2 θ) range from 2 to 60°. Xray photoelectron spectroscopy (XPS) spectra were performed on an Axis Ultra DLD, UK with an Al Ka radiation (15 kV) to analyze functionalization and element content of filler. The dielectric constant and dielectric loss of samples were tested using a Novocontrol Concept 50 broad frequency dielectric spectrometer with a frequency ranging from 1 Hz to 1 MHz. Dynamic mechanical analysis (DMA) was performed on a TA Q800 instrument from 40 to 250 °C with the ramp temperature of 5 °C min⁻¹ and the frequency of 1 Hz, and sample dimension used for each test was 30 mm \times 5 mm \times 1 mm. Tensile properties were determined on Instron 5966 instrument at room temperature with a strain rate of 10 mm min⁻¹. Density was measured on MatsuHaku MH-120E density tester at room temperature. Before measurement, the upper and lower surfaces of the samples were coated with a thin layer of gold to ensure the contact between the copper electrodes and the samples. The thermal conductivity

 (T_c) of composite materials were calculated according to the equation: $T_c = \alpha * \rho * C$, where α , ρ and *C* respectively correspond to thermal diffusivity, density ($\mathbf{g} \cdot \mathbf{cm}^{-3}$) and specific heat capacity ($\mathbf{J} \cdot kg^{-1} \cdot K^{-1}$). The test samples were thin films with a diameter of around 25 mm and a thickness of approximately 300 µm. Thermal diffusivity in both horizontal and vertical directions was measured using different test molds. Measurements were conducted at 25 °C using a thermal diffusivity analyzer (LFA467, NETZSCH), with an average of 5 data points per measurement. *C* values of PDCPD, BN-T₈N, BN-T₁₀N, and BN-T₁₂N were respectively measured by differential scanning calorimetry (DSC, TA) using sapphire as the standard. Meanwhile, the specific heat capacity of the composite material was calculated according to the equation: $C = \varphi C_{BN-T_nN} + (1 - \varphi)C_{PDCPD}$, where φ , C_{BN-T_nN} and C_{PDCPD} respectively correspond to the weight fractions (wt%) of POSS modified fillers (BN-T), the specific heat capacity of the POSS modified fillers (BN-T), and the specific heat capacity of PDCPD. Sample water absorption was calculated according to the following equation:

WA (%) =
$$\frac{m - m_0}{m_0} \times 100$$

where m_0 was the constant weight of the fully crosslinked sample after drying at 80°C for 1 day, and m was the weight of the samples immersed in deionized water for different times. Positron annihilation lifetime spectrum (PALS) was detected using an automated fast-slow coincidence system with a channel width of 6.16 ps and a time resolution of 250 ps. Two identical disk-like samples, measuring 15 mm in diameter and 1.0 mm in thickness, were sandwiched around a 2×10^5 Bq ²²Na positron source wrapped in aluminum foil. Approximately 2.5×10^6 counts were collected at room temperature for each test, and the data were analyzed using LT 9.0 software. The temperature distribution images of different samples were recorded using an infrared thermal imager (FLIR-T600). To evaluate the thermal management capability, the samples were coated with graphite to ensure similar surface optical properties, and then placed on a 90 °C hot stage.

2. Supplementary Schemes and Characterization Data

Scheme S1. Synthetic routes of T₈VS, T₁₀VS, and T₁₂VS.^{*a*}



^{*a*} Reagent and conditions: (i) DMPA, THF, R.T., UV (365nm), 15 min, yield: \sim 32% for T₈VS, \sim 28% for T₁₀VS, and \sim 31% for T₁₂VS. The existence of multi-functionalized products should be noted in addition to the mono-functionalized product.



Figure S1. ¹H NMR of (a) T_8VS , (b) $T_{10}VS$, and (c) $T_{12}VS$. Asterisk represents signal from CDCl₃, THF, methanol, and TMS.



Figure S2. XPS C1s peak-splitting results of (a) BN-OH, (b) BN- T_8N , (c) BN- $T_{10}N$, and (d) BN- $T_{12}N$.



Figure S3. Atomic percentage (%) of BN-OH, BN-T₈N, BN-T₁₀N and BN-T₁₂N obtained by XPS analysis.



Figure S4. SEM images of (a) *h*-BN and (b) BN-OH.



Figure S5. AFM height images, TEM images, HRTEM, and SAED images of (a) BN- T_8N and (b) BN- $T_{10}N$.



Figure S6. Images of DCPD monomer with 15 wt% of *h*-BN, and BN- $T_{12}N$, respectively, indicating the good dispersion and stability of BN- $T_{12}N$ in DCPD.



Figure S7. FT-IR spectra of (a) T_8V_8 , BN-OH, BN- T_8N , DCPD, PDCPD, and PBN- T_8-15 ; (b) $T_{10}V_{10}$, BN-OH, BN- $T_{10}N$, DCPD, PDCPD and PBN- $T_{10}-15$ nanocomposites.



Figure S8. WAXD patterns of (a) PBN-T₈ and (b) PBN-T₁₀ nanocomposites.



Figure S9. SEM images of PBN-T₈-2, PBN-T₈-5, and PBN-T₈-10 nanocomposites.



Figure S10. SEM images of PBN-OH-10.



Figure S11. Dielectric constant and dielectric loss of (a, c) PDCPD and PBN-T₈ with varying BN-T₈N content, and (b, d) PDCPD and PBN-T₁₀N with varying BN-T₁₀ content versus frequency at ambient temperature, where the frequency ranges from 1 to 10^6 Hz.



Figure S12. Dielectric constant of PBN-OH with varying BN-OH content versus frequency at room temperature.



Figure S13. (a) In-plane thermal diffusivity, (b) out-of-plane thermal diffusivity, and (c) out-of-plane thermal conductivity enhancement of PBN-T₈, PBN-T₁₀ and PBN-T₁₂ nanocomposites.



Figure S14. (a) In-plane thermal conductivity, and (b) out-of-plane thermal conductivity of PBN-OH with 0, 5, 10, and 15 wt% of BN-OH.



Figure S15. TGA curves of (a) PBN-T₈, (b) PBN-T₁₀, and (c) PBN-T₁₂ with varying BN-T_nN content under nitrogen atmosphere.



Figure S16. Representative storage modulus of (a) PDCPD and PBN-T₈, (b) PDCPD and PBN-T₁₀ with varying BN-T_nN content. (c) T_g of PBN-T₈, PBN-T₁₀, and PBN-T₁₂ with varying BN-T_nN content obtained from DMA testing.



Figure S17. Tan δ of (a) PDCPD and PBN-T₈, and (b) PDCPD and PBN-T₁₀ versus temperature.



Figure S18. TMA curves of PDCPD, (a) PBN-T₈, (b) PBN-T₁₀, and (c) PBN-T₁₂ with different BN- T_nN content.

Fable S1. Information	1 on T8, T10, ar	nd T ₁₂ POSS	cage sizes.
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	T_8	T ₁₀	T ₁₂
POSS Cage ^{<i>a</i>}			
$l(\text{\AA})^{b}$	3.117	3.128	3.151
$V(\text{\AA}^3)$	l ³	$\frac{5\tan 54^{\circ}}{4}l^3$	$\left(\frac{\sqrt{3}+5\tan 54^\circ}{4}\right)l^3$
	30.3	52.6	67.4

^{*a*} The structure of T_8 , T_{10} , and T_{12} POSS cages are acquired from literatures and can be simplified as polyhedrons.²⁻⁵ ^{*b*} The Si-O-Si bond lengths of T_8 , T_{10} , and T_{12} POSS were acquired from reported results.

Sample	B (%)	C (%)	N (%)	O (%)	Si (%)
<i>h</i> -BN	38.24	14.61	41.38	5.77	0
BN-OH	39.61	6.89	43.69	9.83	0
BN-T ₈	21.18	30.18	28.67	14.99	4.98
BN-T ₁₀	24.98	28.65	26.97	14.63	4.77
BN-T ₁₂	24.94	27.12	28.97	14.38	4.58

Table S2. Atomic percentage (%) obtained by XPS analysis of *h*-BN, BN-OH, BN-T₈N, BN-T₁₀N, and BN-T₁₂N.

Table S3. Specific h	eat capacity of PDCPE	, BN-T ₈ N, BN-T ₁₀ N	, and BN-T ₁₂ N	nanocomposites.
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Sample	Specific heat capacity (J g ⁻¹ K ⁻¹ , 25 °C)
PDCPD	1.57
BN-T ₈	0.93
$BN-T_{10}$	0.95
BN-T ₁₂	0.95

	Mass fraction	Volume fraction	$Density^{\mathfrak{g}}(z,z,z^{-3})$	Specific heat capacity ^b
	(wt%)	(vol%)	Density (g cm ⁺)	(J g ⁻¹ K ⁻¹ , 25 °C)
PDCPD	0.00	0.00	1.028 ± 0.003	1.57
PBN-T ₈ -2	2.00	0.84	1.056 ± 0.007	1.56
PBN-T ₈ -5	5.00	2.13	1.096 ± 0.008	1.54
PBN-T ₈ -10	10.00	4.38	1.155 ± 0.009	1.51
PBN-T ₈ -15	15.00	6.79	1.221 ± 0.008	1.47
PBN-T ₁₀ -2	2.00	0.82	1.059 ± 0.004	1.56
PBN-T ₁₀ -5	5.00	2.08	1.101 ± 0.006	1.54
PBN-T ₁₀ -10	10.00	4.29	1.152 ± 0.007	1.51
PBN-T ₁₀ -15	15.00	6.65	1.220 ± 0.008	1.48
PBN-T ₁₂ -2	2.00	0.86	1.053 ± 0.006	1.56
PBN-T ₁₂ -5	5.00	2.19	1.094 ± 0.007	1.54
PBN-T ₁₂ -10	10.00	4.52	1.148 ± 0.005	1.51
PBN-T ₁₂ -15	15.00	7.00	1.215 ± 0.007	1.48

Table S4. Volume fraction, density, and specific heat capacity of PDCPD, PBN-T₈, PBN-T₁₀, PBN-T₁₂, nanocomposites.

^{*a*} Determined by density meter. ^{*b*} Determined by DSC and Calculated by the formula: $C_{composites} = C_1 \times \varphi_1 + C_2 \times (1 - \varphi_1)$,⁶ where $C_{composites}$, C_1 , C_2 , and φ_1 respectively represent the specific heat capacity of the composite material, the specific heat capacity of the filler, the specific heat capacity of the polymer, and the mass fraction of the filler.

Materials	T_{d5} (°C)	$T_{\rm d10}~(^{\rm o}{\rm C})$	$R_{ m w}$ (%)
PDCPD	443.2	452.5	15.5
PBN-T ₈ -2	440.9	452.4	18.0
PBN-T ₈ -5	436.3	452.5	21.8
PBN-T ₈ -10	408.8	454.1	28.9
PBN-T ₈ -15	413.9	457.0	31.6
PBN-T ₁₀ -2	439.9	452.5	17.5
PBN-T ₁₀ -5	440.2	452.6	21.5
PBN-T ₁₀ -10	440.4	453.0	28.3
PBN-T ₁₀ -15	433.2	454.0	33.3
PBN-T ₁₂ -2	439.3	452.8	17.0
PBN-T ₁₂ -5	441.8	452.7	21.3
PBN-T ₁₂ -10	443.4	452.5	27.7
PBN-T ₁₂ -15	438.2	452.2	35.2

Table S5. 5% weight loss temperature (T_{d5}), 10% weight loss temperature (T_{d10}), and residual weight (R_w) of PBN-T₈, PBN-T₁₀ and PBN-T₁₂ nanocomposites.

References

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