## **Supporting Information**

# Aromatic pore surface with multiple adsorption sites for one-step $C_2H_4$ acquisition from $C_2H_6/C_2H_4$ mixture

Yongqin Zhu<sup>a,b</sup>, Zhenyu Ji<sup>a,b</sup>, Yunzhe Zhou<sup>a</sup>, Mingyan Wu<sup>a,c,d\*</sup>

<sup>a</sup> State Key Lab of Structure Chemistry, Fujian Institute of Research on the Structure of Matter, Chinese Academy of Sciences, Fuzhou 350002, China

<sup>b</sup> College of Chemistry, Fuzhou University, Fuzhou, Fujian 350108, China

° University of Chinese Academy of Sciences, Beijing, 100049, China

<sup>d</sup> Fujian College, University of Chinese Academy of Sciences, Fuzhou, Fujian, 350002,

China.

\*Correspondence and requests for materials should be addressed to M.W. (E-mail: wumy@fjirsm.ac.cn).

## Calculation of selectivity via IAST

Single-site Langmuir-Freundlich (SSLF) model was used to fit the adsorption isotherm of  $C_2H_4$  and  $C_2H_6$ :

$$N = A_1 \frac{B_1 p^{c1}}{1 + B_1 p^{c1}}$$

Where N represents the adsorption capacity of gas, the unit is mmol/g; P represents pressure, the unit is atm;  $A_1$  is the saturated adsorption capacity of different adsorption sites, the unit is mmol/g;  $B_1$  is Langmuir index;  $c_1$  is the Freundlich index.

Then, according to the ideal gas solution adsorption theory (IAST), the adsorption selectivity of  $C_2H_6/C_2H_4$  (1/99, v/v) was calculated:

$$S_{ads} = \frac{\frac{x_1}{x_2}}{\frac{p_1}{p_2}}$$

#### Calculation of isosteric enthalpy of adsorption $(Q_{st})$

The isotherms of  $C_2H_4$  and  $C_2H_6$  at 298 K and 273 K are fitted to the Virial equation (Eqn(1)). Then the isovolumetric heat of adsorption ( $Q_{st}$ ) was calculated by Eqn(2) using the fitting parameters.

$$lnP = lnN + \frac{1}{T} \sum_{i=0}^{m} a_i N^i + \sum_{j=0}^{m} b_j N^j$$
(1)  
$$Q_{st} = -R \sum_{i=0}^{m} a_i N^i$$
(2)

Where P represents pressure, the unit is mmolHg; N represents the adsorption capacity, and the unit is mmol $\cdot$ g<sup>-1</sup>. T stands for temperature, the unit is K; a and b are adsorption correction coefficients; R represents the ideal gas constant, 8.314 J·mol<sup>-1</sup>·K<sup>-1</sup>.

#### **Calculation of Separation Potential**

The separation potential ( $\Delta q$ ) is a combined metric, which considering both uptake capacity and selectivity. It is defined to quantify mixture separations in fixed bed adsorbers.  $\Delta q$  is defined as  $q_1y_2/y_1 - q_2^{1-3}$ , where the  $q_1$  and  $q_2$  represent the molar loadings within the MOF that is in equilibrium with a bulk gas phase mixture with mole fractions  $y_1$ , and  $y_2 = 1 - y_1$ . The physical significance of  $\Delta q$  is that it represents the maximum amount of pure gas that can be recovered during the adsorption phase of fixed bed separations.

#### **Computational details**

The binding sites for C<sub>2</sub>H<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> in Ni-3-F were determined through classical molecular simulations. The single X-ray crystallographic structures were subject to geometry optimization through the CASTEP module implemented with the Materials Studio program, using the generalized gradient approximation (GGA) with the Perdew-Burke-Ernzerhof (PBE) functional and the double numerical plus d-functions (DNP) basis set. The energy, force, and displacement convergence criteria were set as  $1 \times 10^{-5}$  Ha,  $2 \times 10^{-3}$  Ha/Å and  $5 \times 10^{-3}$  Å, respectively. The calculated electrostatic potential for Ni-3-F was mapped onto the Connolly surface with a probe radius of 1.0 Å. Simulated annealing (SA) calculations were performed for a single molecule of C<sub>2</sub>H<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> through a canonical Monte Carlo (NVT) process, and all MOF atoms were further optimized to ensure a more efficient energy landscape scanning for every MOF-C<sub>x</sub>H<sub>x</sub> complex, and the optimized configuration having the lowest energy was used as the global minimum for the subsequent analysis and calculation. The static binding energy (at T= 0 K) was then calculated:  $\Delta E = E_{\text{MOF}} + E_{\text{gas}} - E_{\text{MOF+gas}}$ .

## Calculation of C<sub>2</sub>H<sub>4</sub> production

$$N_{C2H4} = FC_{i}t_{i} = \frac{F \times y_{C_{2}H_{4}} \times \int_{t_{1}}^{t_{2}} (\frac{C_{(t)}}{C_{0}})dt}{m} = \frac{F \times y_{C_{2}H_{4}} \times S}{m}$$

*F* refers to the flow rate of the gas mixture,  ${}^{y_{C_2H_4}}$  refers to the molar fraction of C<sub>2</sub>H<sub>4</sub>, and *m* refers to the mass of the adsorbent. *S* refer to the area of the highlight region in breakthrough curve.





Figure S1. The Powder X-ray diffraction (PXRD) patterns for simulate, as-synthesized, after adsorption and after the breakthrough experiments Ni-3-F.

Figure S2. PXRD patterns of Ni-3-F after soaking in different solvents.



Figure S3. TGA curves of Ni-3-F.







Figure S5.  $N_2$  isotherms at 77 K of Ni-3-F.



Figure S6. Five cycles C<sub>2</sub>H<sub>4</sub> adsorption isotherms at 298 K.







Figure S8. Fitting curve and calculated fitting parameters of C<sub>2</sub>H<sub>4</sub>.



![](_page_7_Figure_0.jpeg)

Figure S9. The calculated  $Q_{st}$  of Ni-3-F for C<sub>2</sub>H<sub>6</sub> (blue) and C<sub>2</sub>H<sub>4</sub> (red) respectively.

Figure S10. C<sub>2</sub>H<sub>4</sub> adsorption isotherms fitting by SSLF model at 273 K.

![](_page_7_Figure_3.jpeg)

Figure S11. C<sub>2</sub>H<sub>6</sub> adsorption isotherms fitting by SSLF model at 273 K.

![](_page_8_Figure_0.jpeg)

Figure S12. C<sub>2</sub>H<sub>4</sub> adsorption isotherms fitting by SSLF model at 298 K.

![](_page_8_Figure_2.jpeg)

Figure S13. C<sub>2</sub>H<sub>6</sub> adsorption isotherms fitting by SSLF model at 298 K.

![](_page_9_Figure_0.jpeg)

Figure S14. C<sub>2</sub>H<sub>4</sub> adsorption isotherms fitting by SSLF model at 303 K.

![](_page_9_Figure_2.jpeg)

Figure S15. C<sub>2</sub>H<sub>6</sub> adsorption isotherms fitting by SSLF model at 303 K.

![](_page_10_Figure_0.jpeg)

Figure S16. C<sub>2</sub>H<sub>4</sub> adsorption isotherms fitting by SSLF model at 308 K.

![](_page_10_Figure_2.jpeg)

Figure S17. C<sub>2</sub>H<sub>6</sub> adsorption isotherms fitting by SSLF model at 308 K.

![](_page_11_Figure_0.jpeg)

Figure S18. C<sub>2</sub>H<sub>4</sub> adsorption isotherms fitting by SSLF model at 313 K.

![](_page_11_Figure_2.jpeg)

Figure S19.  $C_2H_6$  adsorption isotherms fitting by SSLF model at 313 K.

![](_page_12_Figure_0.jpeg)

Figure S20. The comparison of  $C_2H_6$  and  $C_2H_4$  isotherms of Ni-3-F at 298 K in the 0-10 kPa pressure range.

Compound	Ni-3-F		
CCDC	2369828		
Empirical formula	$C_{24}H_{12}F_2N_2NiO_4$		
Formula weight	489.05		
Temperature (K)	100		
Crystal system	orthogonality		
Space group	Pnna		
	a = 17.2804 (4), α = 90		
Unit cell dimensions (Å, deg)	$b = 12.1294$ (3), $\beta = 90$		
	$c = 15.2030$ (3), $\gamma = 90$		
Volume (Å <sup>3</sup> )	3186.56		
Ζ	8		
Density (calculated) (g/m <sup>3</sup> )	1.024		
Absorption coefficient (mm <sup>-1</sup> )	1.191		
F <sub>000</sub>	1000		
$\theta$ for data collection (deg)	4.664 to 76.419		
Reflections collected	11649		
Goodness-of-fit on F <sup>2</sup>	0.985		
Final R indexes [I > 2sigma(I)]	$R_1 = 0.0639, wR_2 = 0.1899$		
Final R indexes [all data]	$R_1 = 0.0678, wR_2 = 0.1940$		
Largest diff. peak / hole / (e Å <sup>-3</sup> )	0.948 / -0.407		

Table S1. Crystal data and structure refinements for Ni-3-F.

Table S2. Summary of adsorption capacity of  $C_2H_6$  and  $C_2H_4$ , IAST ( $C_2H_6/C_2H_4$  (1/99)) and separation potential ( $C_2H_6/C_2H_4$  (1/99)) at different temperatures.

Temperatures	C <sub>2</sub> H <sub>6</sub> Uptake (cm <sup>3</sup> /g)	C <sub>2</sub> H <sub>4</sub> Uptake (cm <sup>3</sup> /g)	IAST	Separation potential (mmol/g)
273 К	105.89	98.58	1.86	3.64
298 K	77.44	65.13	1.80	2.21
303 K	70.93	59.13	1.76	1.90
308 K	64.98	54.28	1.72	1.64
313 K	61.39	50.11	1.69	1.45

## References

(1) PRAUSNITZ, A. L. M. a. J. M. Thermodynamics of Mixed-Gas Adsorption. *AIChE journal* **1965**, *11*, 121-130.

(2) Krishna, R. Metrics for Evaluation and Screening of Metal–Organic Frameworks for Applications in Mixture Separations. *ACS Omega* **2020**, *5*, 16987-17004.

(3) Krishna, R. Screening metal–organic frameworks for mixture separations in fixed-bed adsorbers using a combined selectivity/capacity metric. *RSC Advances* **2017**, *7*, 35724-35737.