

Supplementary Information

Thermodynamic assessment of Gd-doped CeO₂ for microwave-assisted thermochemical reduction

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1 **S1. Microwave power transfer from source to sample-loaded cavity**

2 In typical electric circuit analysis, lumped elements are used. This means that the components
3 are not affected by the physical size of the circuit. However, suppose the wavelength of the
4 high-frequency (such as RF, microwave) power source is smaller or similar to the physical size
5 of the circuit (considered distributed elements). In that case, the voltage and current can vary
6 significantly in amplitude and phase along the line length. Therefore, if these characteristics
7 are not considered, the microwave signal will be reflected from the load, resulting in a decrease
8 in the power reaching the load. Transmission line theory is utilized for the efficient delivery of
9 microwave power to load.¹

$$Return\ Loss = -20\log(|\Gamma|) = -S_{11}(f) \quad (S1)$$

$$P_{eff}(f) = P(1 - |S_{11}(f)|^2) \quad (S2)$$

$$f_0 \equiv f_{nml} = \frac{c}{2\pi\sqrt{\epsilon_r\mu_r}\sqrt{\left(\frac{P_{nm}^{TE}}{r}\right)^2 + \left(\frac{l\pi}{h}\right)^2}} \quad (S3)$$

10 **Equation (S1)** shows the expression for the return loss of the reflection coefficient Γ , where Γ
11 corresponds to the voltage ratio of reflected voltage (V_{ref}) divided by incident voltage (V_{inc}).
12 $-S_{11}$ expressed as a function of frequency is equivalent to return loss and can be measured with
13 a network analyzer. Additionally, this value can be obtained from a spectrum analyzer for a
14 single frequency used in this paper. The effective microwave power $P_{eff}(f)$ delivered to the
15 sample-loaded cavity can be expressed as **equation (S2)**, where P represents the amplified
16 microwave output power. Meanwhile, the resonant frequency f_0 for the cylindrical cavity is
17 defined only in TE (Transverse Electric) mode in this work, as shown in **equation (S3)**. The
18 term c is the speed of light, ϵ_r is the relative permittivity of the filled medium inside the cavity,
19 μ_r is the relative permeability of the filled medium inside the cavity, and P_{nm}^{TE} is m^{th} zero of the
20 n^{th} Bessel function. The values r and h represent the radius and height of the cavity,

1 respectively. Due to the nature of the resonance mode, when a driving frequency f_d different
2 from f_0 is applied to the cavity, the reflection ratio of power increases ($|S_{11}(f)|$ increases),
3 resulting in a decrease in the power transfer ratio $(1 - |S_{11}(f)|^2)$ to the cavity. For the case of
4 literature^{2,3} and our work, when the temperature of the metal oxides is increased via microwave
5 heating, f_0 of the sample-loaded cavity decreases. Therefore, $P_{eff}(f)$ is maximized by tracking
6 the continuous shift of f_0 and matching f_d to f_0 .

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δ	1000/T	$\ln(P(O_2))$	Slope	ΔH_0 (kJ/mol _O)
0.0045	1.45	-8.52		
	1.38	-5.00	-45.86	190.64
	1.34	-4.49	-14.45	60.08
	1.19	-2.28	-14.66	60.93
0.0065	1.40	-8.52		
	1.30	-5.00	-34.89	145.03
	1.25	-4.49	-11.05	45.92
	1.09	-2.28	-13.70	56.95
0.0085	1.35	-8.52		
	1.23	-5.00	-29.21	121.53
	1.18	-4.49	-9.38	39.00
	1.01	-2.28	-13.19	54.82
0.0105	1.30	-8.52		
	1.17	-5.00	-25.79	107.20
	1.11	-4.49	-8.42	35.02
0.0125	1.26	-8.52		
	1.11	-5.00	-23.54	97.85
	1.05	-4.49	-7.83	32.53
0.0145	1.22	-8.52		
	1.06	-5.00	-21.98	91.37
	0.99	-4.49	-7.43	30.89

1 **Table S1** Enthalpy changes based on slope analysis between consecutive data points in Figure
2 7 of the main text. The slope represents the $\Delta \ln(P(O_2))/\Delta(1000/T)$ obtained from the data
3 points of the previous and the corresponding rows.

References

1. Pozar, D. M. *Microwave Engineering*. (Wiley, Hoboken, NJ, 2012).
2. Catala-Civera, J. M. *et al.* Dynamic Measurement of Dielectric Properties of Materials at High Temperature During Microwave Heating in a Dual Mode Cylindrical Cavity. *IEEE Trans. Microwave Theory Techn.* **63**, 2905–2914 (2015).
3. Serra, J. M. *et al.* Hydrogen production via microwave-induced water splitting at low temperature. *Nat Energy* **5**, 910–919 (2020).