

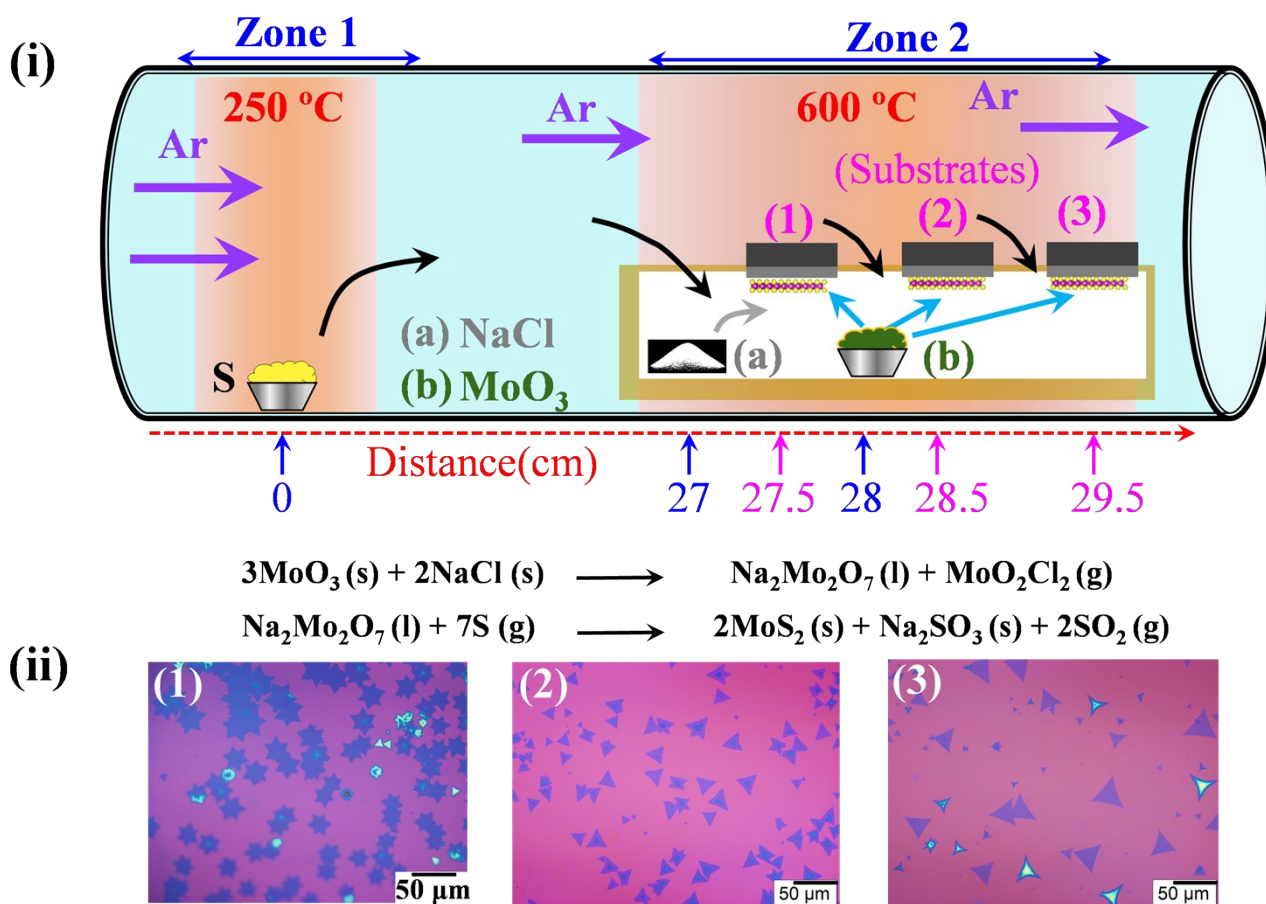
## Supplementary Information

### **Grain Boundary Effect Unveiled in Monolayer MoS<sub>2</sub> for Photonic Neuromorphic Application**

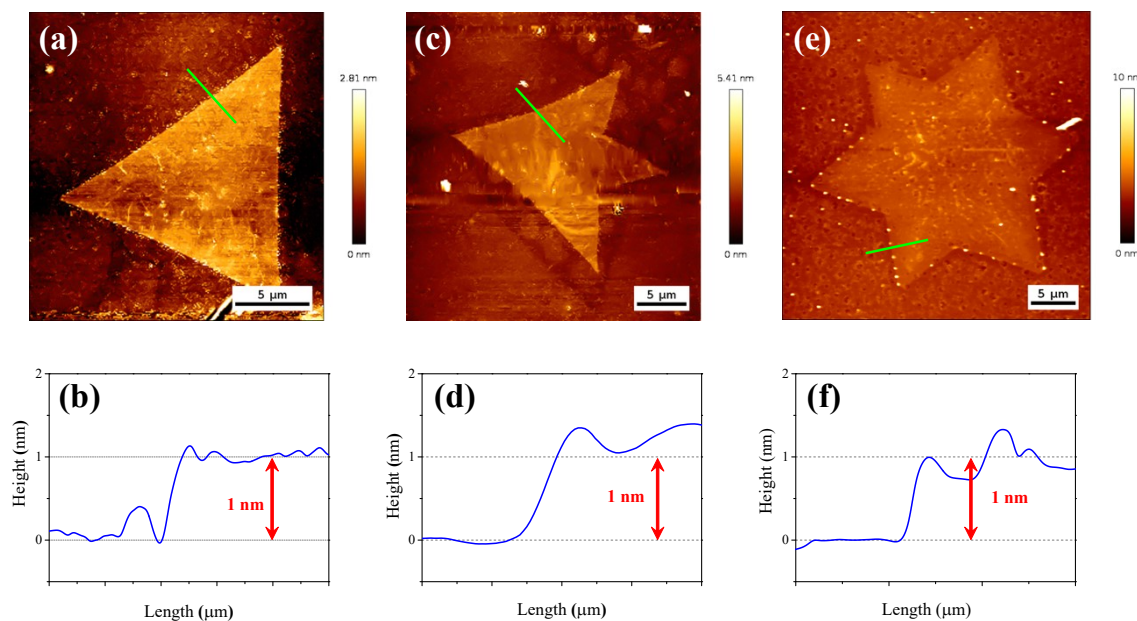
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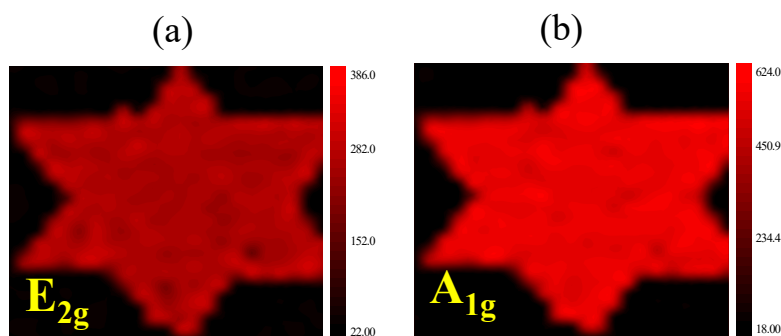
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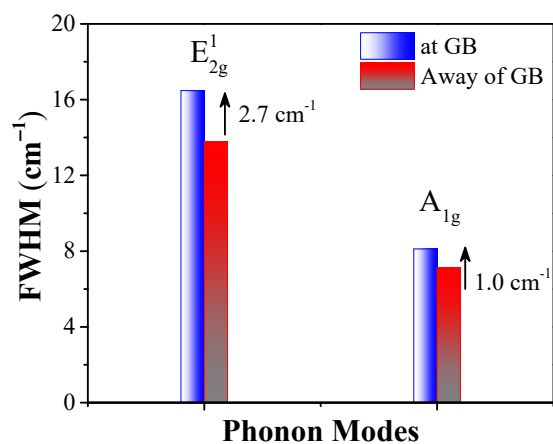
**Figure S1.** (i) This schematic illustrates the alkali halide assisted chemical vapor deposition process of MoS<sub>2</sub> using MoO<sub>3</sub> and S as precursors, with NaCl acting as a seeding promoter at 600 °C. Positions (1), (2), and (3) denote different substrate placements, positioned at distances of 27.5 cm, 28.5 cm, and 29.5 cm downstream from the sulfur (S) precursor located at 0 cm, while NaCl is situated 1.0 cm upstream of the MoO<sub>3</sub> precursor. The equations depict the MoS<sub>2</sub> growth steps inside the CVD chamber. (ii) Optical microscope images show 2D monolayer MoS<sub>2</sub> samples of different shapes at positions (1), (2), and (3) respectively.



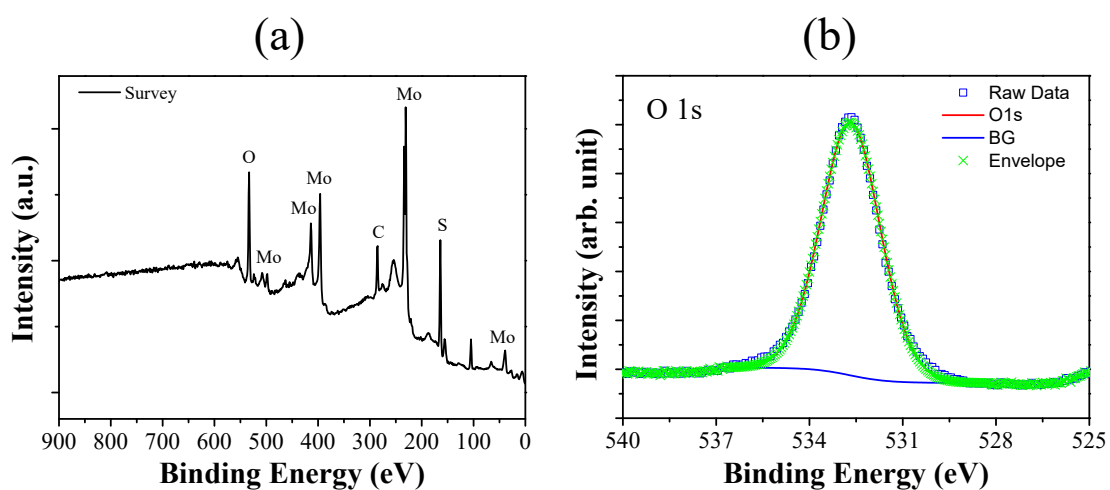
**Figure S2.** Atomic force microscopy was utilized to capture topographic images of monolayer MoS<sub>2</sub> samples with varying shapes recorded immediately after the growth, alongside the corresponding height profiles extracted along marked lines. Specifically, (a and b) depict triangular shapes, (c and d) showcase four-point star samples, and (e and f) illustrate six-point star samples. The presence of white spots represent the unreacted precursors and/or seeding promoter NaCl, which are removed using focused ion beam (FIB) after device fabrication.



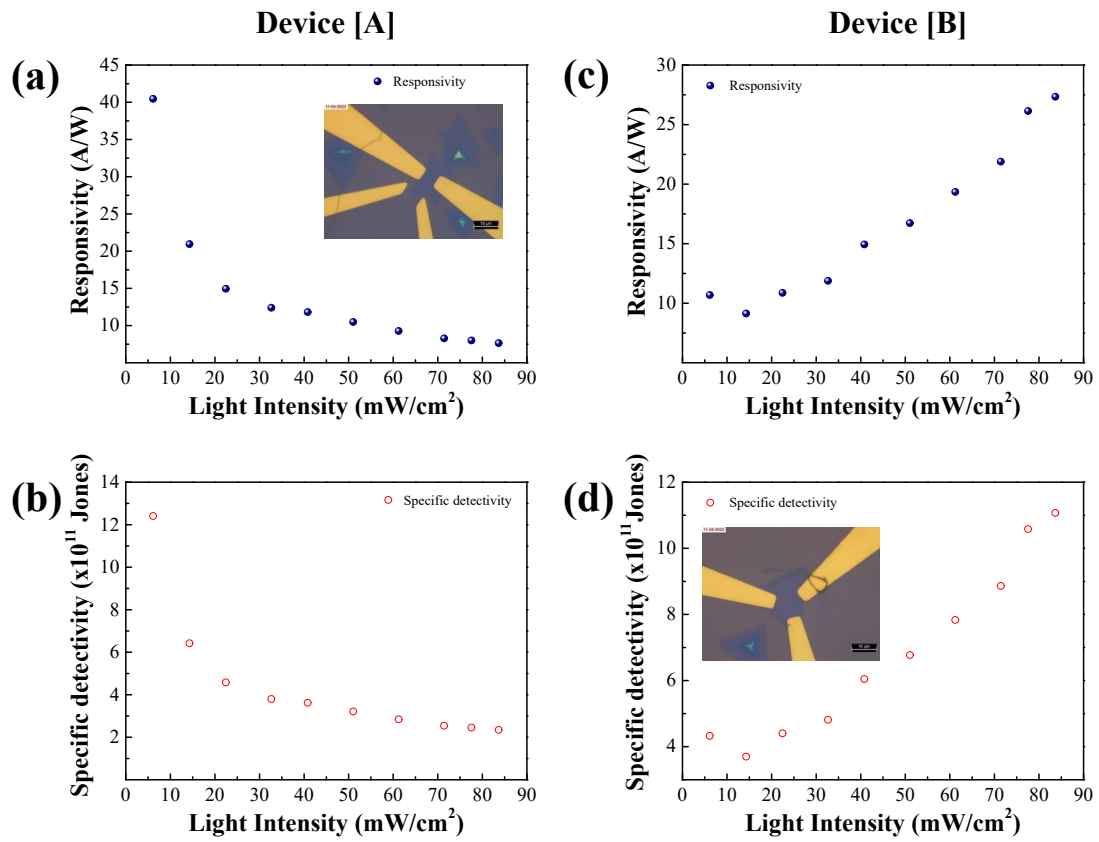
**Figure S3.** Raman mapping images of six-point star ML MoS<sub>2</sub> sample with 532 nm laser excitation. (a) Depicts in-plane ( $E_{2g}^1$ ) vibrations and (b) Shows the out-of-plane ( $A_{1g}$ ) vibrations.



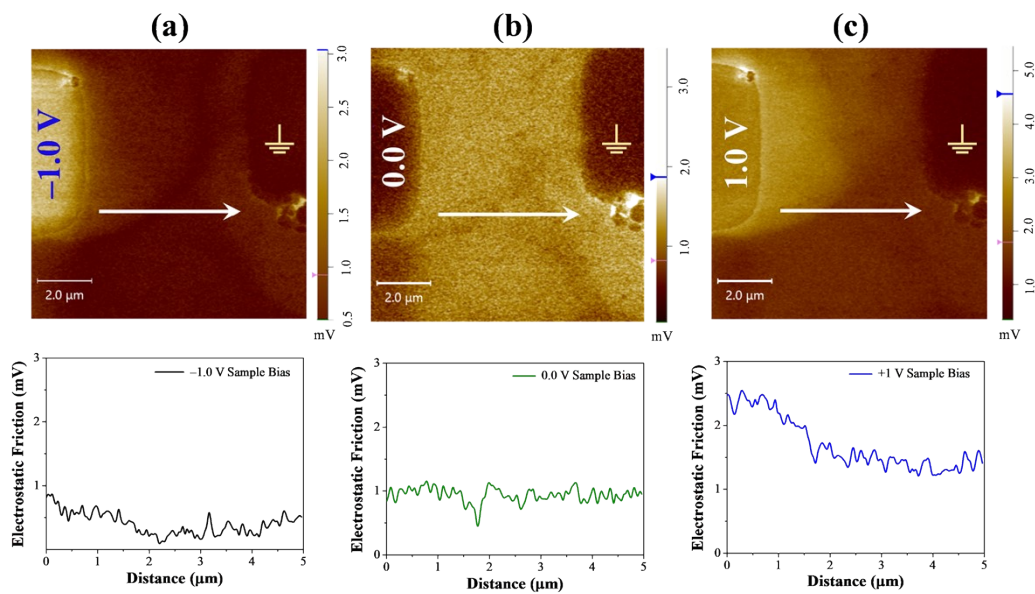
**Figure S4.** The variation in full-width half-maxima (FWHM) for the  $E_{2g}^1$  and  $A_{1g}$  phonon modes between the vicinity of the grain boundary (GB) and regions farther from it, as illustrated in Figure 2(a) of the main manuscript.



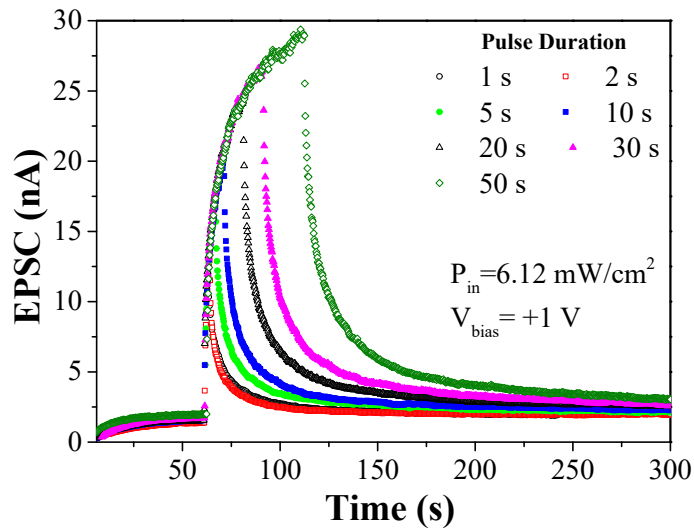
**Figure S5.** (a) XPS survey spectrum of the CVD grown six-point star ML  $\text{MoS}_2$  sample. (b) High-resolution spectral line of O 1s electrons originating from the substrate  $\text{Si/SiO}_2$ .



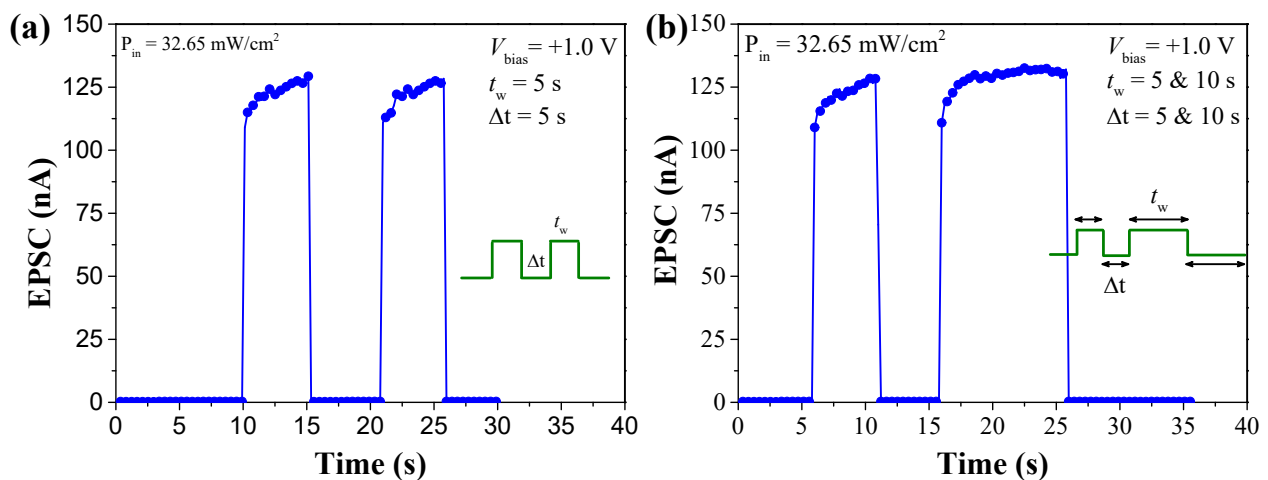
**Figure S6.** (a and b) Light intensity dependent R and D\* for the device [A]. (c and d) Light intensity dependent R and D\* for the device [B]. Insets show the optical microscope images of the corresponding devices.



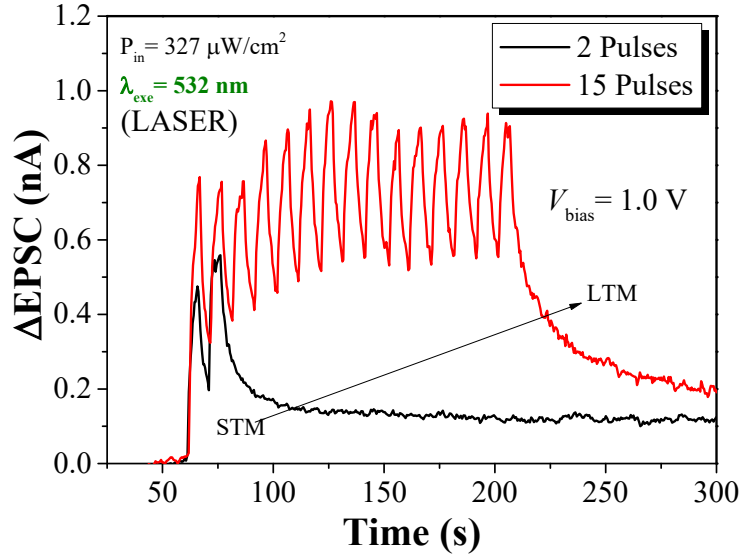
**Figure S7.** Electrostatic force microscopy (EFM) was employed to map the surface potential of device [A] under light illumination, using different biasing polarities. (a) A biasing voltage of  $-1.0$  V was applied, (b) no biasing voltage was applied, and (c)  $+1.0$  V was applied during scanning. The corresponding line profiles along the marked arrow line reveal that the electrostatic friction, represented by the mV potential unit, is higher when  $+1.0$  V is applied compared to  $0$  V biasing, and lower when  $-1.0$  V is applied compared to  $0$  V biasing.



**Figure S8.** Normalized EPSC responses were obtained by adjusting the width of the light pulses, while maintaining a constant power density of  $6.12$   $\text{mW}/\text{cm}^2$ .



**Figure S9.** Measurements of Paired Pulse Facilitation (PPF) for device [B] involved employing a pair of light pulses with a power density of  $32.65$   $\text{mW}/\text{cm}^2$  and an applied bias of  $+1.0$  V. This was carried out in two scenarios: (a) maintaining a pulse width ( $t_w$ ) and temporal gap ( $\Delta t$ ) of  $5$  s, and (b) utilizing two consecutive pulses with pulse widths ( $t_w$ ) of  $5$  s and  $10$  s, respectively, while keeping the temporal gap ( $\Delta t$ ) constant at  $5$  s.



**Figure S10.** By utilizing sequential laser light pulses ( $\lambda= 532$  nm,  $P_{in}= 327 \mu\text{W}/\text{cm}^2$ ) lasting 5 s each, with a temporal gap of 5 s between pulses, we aim to demonstrate synaptic weight potentiation (P) through rehearsal via photonic modulation of EPSC.

### Section S1: Photodetector Figure of Merit (FOM) Calculations

The figure of merits (FOM) of a photodetector are responsivity (R), specific detectivity ( $D^*$ ), signal to noise ratio (SNR), noise equivalent power (NEP) and detectivity (D) and they are defined as follows,

#### a) Responsivity (R)

Responsivity is the ratio of the photocurrent ( $I_{ph}$ ) to the incident optical power and is expressed in  $\text{A}/\text{W}$ .<sup>1, 2</sup>

$$R = \frac{I_{ph}}{(P_{light}A_{effe})} \quad (1)$$

Where,  $I_{ph}=I_{light}-I_{dark}$ ,  $I_{light}$  is the current under light illumination and  $I_{dark}$  is the dark current.  $A_{effe}$  is the effective area of the device and  $P_{light}$  is the optical power density.

#### b) Specific detectivity ( $D^*$ )

The ability to identify the lowest optical signals is characterized as specific detectivity ( $D^*$ ). Given the assumption that shot noise from the dark current accounts for the majority of the total noise, then the  $D^*$  can be found as follows and it is expressed in  $\text{cm Hz}^{1/2}\text{W}^{-1}$ (Jones).<sup>3</sup>

$$D^* = \frac{R\sqrt{A_{effe}}}{\sqrt{(2eI_{dark})}} \quad (2)$$

Where, R is the responsivity of the photodetector.

### c) Signal to Noise Ratio (SNR)

The ratio of signal power to noise power in a photodetector is referred to as the signal to noise ratio. It is expressed as follows:<sup>2</sup>

$$SNR = \frac{\text{Signal power}}{\text{Noise power}}$$

$$SNR = \frac{\langle i_{ph}^2 \rangle}{\langle i_{noise}^2 \rangle} \quad (3)$$

### d) Noise Equivalent Power (NEP) and Detectivity (D)

The minimal incident radiation power required to achieve SNR of 1 in a 1 Hz bandwidth is known as noise equivalent power. Typically, it is expressed as  $\text{WHz}^{-1/2}$ . It is determined as

$$NEP = \frac{\sqrt{\langle i_{noise}^2 \rangle}}{R} \quad (4)$$

Where R is the responsivity and  $\langle i_{noise}^2 \rangle$  is the mean square noise current is the sum of shot noise current ( $\langle i_{sh}^2 \rangle$ ) and thermal noise current ( $\langle i_{th}^2 \rangle$ ), they are depending on the bandwidth (B) of the photodetector and described as,

$$\text{Shot noise, } \langle i_{sh}^2 \rangle = 2qB \langle i_d \rangle \quad (5)$$

$$\text{Thermal noise, } \langle i_{th}^2 \rangle = \frac{4kTB}{r} \quad (6)$$

By substituting equation (5) and (6) in (4) as

$$NEP = \frac{\sqrt{\langle i_{sh}^2 \rangle + \langle i_{th}^2 \rangle}}{R} \quad (7)$$

$$NEP = \frac{\sqrt{2qB \langle i_d \rangle + \frac{4kTB}{r}}}{R} \quad (8)$$



Where, B is the bandwidth of the photodetector which is given by  $B = \frac{0.35}{\tau_{rise}}$ , q is the electronic charge,  $\tau_{rise}$  is the rise time of the photodetector,  $\langle i_d \rangle$  is average dark current obtained from the temporal response of the device, kT is the thermal energy and r is the resistance of the device and is given by

$$r = \frac{V}{I_{dark,2}}$$

For an entire bandwidth (B), NEP is expressed in W and the reciprocal of the NEP is given by the detectivity (D) of the photodetector and is expressed in  $W^{-1}$ .

By considering the above mentioned equations, Device [A] and Device [B] figure of merits are found as below.

### For Device A:

From the temporal response of the device given in main manuscript, the average dark current is

$$\langle i_d \rangle = 1.36631 \times 10^{-9} A$$

From the temporal response the rise time of the Device [A] is 12.88 s, therefore the bandwidth is given

$$B = \frac{0.35}{\tau_{rise}} = 27.1 \text{ mHz}$$

By substituting the values in equation (5),

$$\langle i_{sh}^2 \rangle = 2qB \langle i_d \rangle = 1.1881 \times 10^{-29} A^2$$

The resistance (r) of the Device [A] is given by  $r = \frac{V}{I_{dark}} = 0.899 \text{ G}\Omega$ , where  $I_{dark} = 1.112 \text{ nA}$  at 1 V applied bias.

The signal power that is square mean of the photocurrent, obtained from the temporal response of the Device [A] is

$$\langle i_{ph}^2 \rangle = 3.5853 \times 10^{-14} A^2$$

The calculated thermal noise by substituting the values of B, r, kT in equation (6) is

$$\langle i_{th}^2 \rangle = 5.00883 \times 10^{-31} A^2$$

By adding the shot noise and thermal noise power will give the total noise power i.e.

$$\langle i_{noise}^2 \rangle = 1.23818 \times 10^{-29} A^2$$

Therefore the signal to noise ratio is,

$$SNR = \frac{\langle i_{ph}^2 \rangle}{\langle i_{noise}^2 \rangle} = 2.8956 \times 10^{15} = 154.462 \text{ dB}$$

The Responsivity and Specific detectivity are estimated for Device [A] at different light intensities as shown in Table S1.

**Table S1:** Variation of Responsivity and Specific detectivity with a function of light intensity for device [A].

Intensity (mW/cm <sup>2</sup> )	R (A/W)	D* × 10 <sup>11</sup> (Jones)
6.12	40.5	12.4
12.49	20.9	6.42
22.45	14.9	4.58
32.65	12.4	3.80
40.82	11.8	3.62
51.02	10.5	3.21
61.22	9.27	2.84
71.43	8.28	2.54
77.55	8.00	2.45
83.67	7.64	2.34

The NEP (for bandwidth 1 Hz) and NEP (for entire bandwidth) are estimated for Device [A] at different light intensities as shown in Table S2. The detectivity (D) is the reciprocal of NEP (for entire bandwidth) also included in Table S2.

**Table S2:** NEP for B of 1 Hz, for entire bandwidth and detectivity of Device [A]

Intensity (mW/cm <sup>2</sup> )	NEP (W/√Hz)	NEP (W)	Detectivity (W <sup>-1</sup> )
6.12	$5.27 \times 10^{-16}$	$8.69 \times 10^{-17}$	$1.15 \times 10^{16}$
12.49	$1.02 \times 10^{-15}$	$1.68 \times 10^{-16}$	$5.94 \times 10^{15}$
22.45	$1.43 \times 10^{-15}$	$2.36 \times 10^{-16}$	$4.23 \times 10^{15}$

32.65	$1.72 \times 10^{-15}$	$2.84 \times 10^{-16}$	$3.52 \times 10^{15}$
40.82	$1.81 \times 10^{-15}$	$2.98 \times 10^{-16}$	$3.35 \times 10^{15}$
51.02	$2.03 \times 10^{-15}$	$3.35 \times 10^{-16}$	$2.98 \times 10^{15}$
61.22	$2.30 \times 10^{-15}$	$3.80 \times 10^{-16}$	$2.63 \times 10^{15}$
71.43	$2.58 \times 10^{-15}$	$4.25 \times 10^{-16}$	$2.35 \times 10^{15}$
77.55	$2.67 \times 10^{-15}$	$4.40 \times 10^{-16}$	$2.27 \times 10^{15}$
83.67	$2.79 \times 10^{-15}$	$4.61 \times 10^{-16}$	$2.17 \times 10^{15}$

**For Device B:**

From the temporal response of the device given in main manuscript, the average dark current is

$$\langle i_d \rangle = 2.86538 \times 10^{-10} A$$

From the temporal response the rise time of the Device [A] is 256 ms, therefore the bandwidth is given

$$\text{by } B = \frac{0.35}{\tau_{rise}} = 1.3671 \text{ Hz}$$

By substituting the values in equation (5),

$$\langle i_{sh}^2 \rangle = 2qB \langle i_d \rangle = 1.25352 \times 10^{-28} A^2$$

The resistance (r) of the Device [A] is given by  $r = \frac{V}{I_{dark}} = 1.234 \text{ G}\Omega$ , where  $I_{dark} = 0.8102 \text{ nA}$  at 1V applied bias.

The signal power that is square mean of the photocurrent, obtained from the temporal response of the Device [A] is

$$\langle i_{ph}^2 \rangle = 1.78478 \times 10^{-14} A^2$$

The calculated thermal noise by substituting the values of B, r, kT in equation (6) is

$$\langle i_{th}^2 \rangle = 1.83869 \times 10^{-29} A^2$$

By adding the shot noise and thermal noise power will give the total noise power i.e.,

$$\langle i_{noise}^2 \rangle = 1.43716 \times 10^{-28} A^2$$

Therefore the signal to noise ratio is,

$$SNR = \frac{\langle i_{ph}^2 \rangle}{\langle i_{noise}^2 \rangle} = 1.24188 \times 10^{14} = 140.94 \text{ dB}$$

The Responsivity and Specific detectivity are estimated for Device [B] at different light intensities as shown in Table S3.

**Table S3:** Variation of Responsivity and Specific detectivity with a function of light intensity for the device [B].

<b>Intensity (mW/cm<sup>2</sup>)</b>	<b>R (A/W)</b>	<b>D* (Jones)</b>
6.12	10.7	$4.33 \times 10^{11}$
12.49	9.14	$3.70 \times 10^{11}$
22.45	10.9	$4.40 \times 10^{11}$
32.65	11.9	$4.81 \times 10^{11}$
40.82	14.9	$6.05 \times 10^{11}$
51.02	16.7	$6.77 \times 10^{11}$
61.22	19.3	$7.83 \times 10^{11}$
71.43	21.9	$8.86 \times 10^{11}$
77.55	26.1	$1.06 \times 10^{12}$
83.67	27.3	$1.11 \times 10^{12}$

The NEP (for bandwidth 1 Hz) and NEP (for entire bandwidth) are estimated for Device [B] at different light intensities as shown in Table S4. The detectivity (D) is the reciprocal of NEP (for entire bandwidth) also included in Table S4.

**Table S4:** NEP for B of 1 Hz, for entire bandwidth and detectivity of Device [B]

<b>Intensity (mW/cm<sup>2</sup>)</b>	<b>NEP (W/<math>\sqrt{Hz}</math>)</b>	<b>NEP (W)</b>	<b>Detectivity (W<sup>-1</sup>)</b>
6.12	$9.58 \times 10^{-16}$	$1.12 \times 10^{-15}$	$8.92 \times 10^{14}$
12.49	$1.12 \times 10^{-15}$	$1.31 \times 10^{-15}$	$7.62 \times 10^{14}$
22.45	$9.41 \times 10^{-16}$	$1.10 \times 10^{-15}$	$9.09 \times 10^{14}$

32.65	$8.62 \times 10^{-16}$	$1.01 \times 10^{-15}$	$9.92 \times 10^{14}$
40.82	$6.88 \times 10^{-16}$	$8.05 \times 10^{-15}$	$1.24 \times 10^{15}$
51.02	$6.14 \times 10^{-16}$	$7.18 \times 10^{-16}$	$1.39 \times 10^{15}$
61.22	$5.31 \times 10^{-16}$	$6.21 \times 10^{-16}$	$1.61 \times 10^{15}$
71.43	$4.68 \times 10^{-16}$	$5.48 \times 10^{-16}$	$1.83 \times 10^{15}$
77.55	$3.93 \times 10^{-16}$	$4.59 \times 10^{-16}$	$2.18 \times 10^{15}$
83.67	$3.76 \times 10^{-16}$	$4.39 \times 10^{-16}$	$2.28 \times 10^{15}$

### Supporting References:

- (1) Tamalampudi, S. R.; Lu, Y. Y.; Kumar, U. R.; Sankar, R.; Liao, C. D.; Moorthy, B. K.; Cheng, C. H.; Chou, F. C.; Chen, Y. T. High Performance and Bendable Few-Layered InSe Photodetectors with Broad Spectral Response. *Nano Letters* **2014**, *14* (5), 2800-2806.
- (2) Wang, F., Zhang, T., Xie, R. *et al.* How to characterize figures of merit of two-dimensional photodetectors. *Nat Commun* **2023**, *14* (2224).
- (3) Wang, F.; Wang, Z. X.; Yin, L.; Cheng, R. Q.; Wang, J. J.; Wen, Y.; Shifa, T. A.; Wang, F. M.; Zhang, Y.; Zhan, X. Y.; et al. 2D library beyond graphene and transition metal dichalcogenides: a focus on photodetection. *Chemical Society Reviews* **2018**, *47* (16), 6296-6341.