# Supporting Information for "Granular polymer composites"

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#### 1 Characteristic ratio for restricted-bond-angle chains

A Matlab computer program was written to generate random walks of chains having *N* monomers, restricted bond angle  $\theta$ , and fixed bond length *l*. The characteristic ratio  $C_{\infty} = R_0^2/[(N-1)l^2]$  is plotted in figure 1 versus *N* for  $\theta \leq \pi = 180^{\circ}$  (ideal chains) and  $\theta \leq \pi/5 = 36^{\circ}$ . The standard deviations of fluctuations about the mean, obtained from  $10<sup>4</sup>$  random chain configurations for each *N*, are indicated by the error bars. With  $\theta \leq 180^{\circ}$ , the data with  $N \geq 64$  is well described by a two-parameter model  $C_{\infty}$  =  $C_{\infty}(N \to \infty) - c_1 N^{-1}$ , furnishing  $C_{\infty}(N \to \infty) \approx 1.001$  (with  $c_1 \approx 1.247$ ). With  $\theta \leq 36^{\circ}$ , however, the data with  $N \geq 64$  is better described by a three-parameter model  $C_{\infty} = C_{\infty}(N \to \infty) - c_1 \exp(-N/c_2)$ , furnishing  $C_{\infty}(N \to \infty) \approx 19.50$  (with  $c_1 \approx 6.694$ and  $c_2 \approx 81.41$ ). Note that the standard deviation of the fluctuations in the mean-squared end-to-end distance  $R_0^2$  scale as  $Nl^2$  as  $N \to \infty$ .

Limiting bond angles to  $\theta < 36^{\circ}$  furnished a characteristic ratio that increases from  $\approx$  5 when *N* = 10 toward a plateau  $C_{\infty}(N \to \infty) \approx 19.5$  when  $N \gtrsim 300$ . Quantifying

chain dimensions with  $R_0 = l\sqrt{C_{\infty}N} \approx 9.8\sqrt{N}$  mm shows that  $R_0 \gtrsim D$  when  $N \gtrsim 6$  with  $D = 2.5$  cm, and  $N \gtrsim 50$  with  $D = 7$  cm.



Figure 1: The characteristic ratio  $C_{\infty}$  versus the number of monomers *N* for ideal chains  $(\theta \leq 180^{\circ}, \text{ top})$  and chains with restricted bond angles  $\theta \leq 36^{\circ}$  (bottom). Error bars indicate the standard deviations of fluctuations about the mean, obtained by averaging over 10<sup>4</sup> randomly generated chain configurations. The characteristic ratios as  $N \to \infty$ , obtained by fitting empirical models (lines) to the data with  $N \geq 64$  (lines) are  $C_{\infty}(N \rightarrow$  $\infty) \approx 1.001$  ( $\theta \le 180^{\circ}$ ) and 19.50 ( $\theta \le 36^{\circ}$ ).

### 2 Virial coefficients

The scaled partial molar sphere volume

$$
\bar{V}_s \equiv v_s^{-1} \left( \frac{\partial V}{\partial n_s} \right)_{n_b} = \phi^{-1} - (1 - x_s)[x_s + (1 - x_s)v_b/v_s]\phi^{-2} \left( \frac{\partial \phi}{\partial x_s} \right). \tag{1}
$$

The virial coefficients in the main text

$$
\bar{V}_s^0 = \phi_c^{-1} - \frac{v_b}{v_s} \phi_c^{-2} \left(\frac{\partial \phi}{\partial x_s}\right)_{x_s=0} \tag{2}
$$

and

$$
\bar{V}_s^1 = \frac{v_b}{v_s} \phi_c^{-1} \left(\frac{\partial \bar{V}_s}{\partial x_s}\right)_{x_s=0} \tag{3}
$$

are therefore furnished by experimental measurements of  $\phi(x_s)$ .

## 3 Supplementary thermodynamic formulas

Similarly to the main text for sphere (nanoparticle) partial molar volume, the ball (monomer) partial molar volume scaled with the intrinsic ball volume  $v_b = 4\pi a_b^3/3$  is

$$
\bar{V}_b \equiv v_b^{-1} \left(\frac{\partial V}{\partial n_b}\right)_{n_s} \tag{4}
$$

$$
= \phi^{-1} + x_s[1 + x_s(v_s/v_b - 1)]\phi^{-2}\left(\frac{\partial\phi}{\partial x_s}\right). \tag{5}
$$

Moreover, to leading order at vanishing sphere mole fraction  $(x_s \to 0)$ ,

$$
\bar{V}_b = \phi_c^{-1} + O(\phi_s^2). \tag{6}
$$

When  $a_s \gtrsim l_l$  and, thus, spheres contribute only their intrinsic volume to the mixture, without disturbing the bulk chain packing,

$$
\left(\frac{\partial \phi}{\partial x_s}\right)_{x_s=0} = \frac{v_s}{v_b} (\phi_c - \phi_c^2) \text{ when } \bar{V}_s^0 = 1.
$$
 (7)

Moreover, when  $a_s \lesssim l_l$  and, thus, spheres merely fill voids in the bulk chain packing,

$$
\left(\frac{\partial \phi}{\partial x_s}\right)_{x_s=0} = \frac{v_s}{v_b} \phi_c \text{ when } \bar{V}_s^0 = 0.
$$
 (8)

In the dilute regime,

$$
\phi_s \equiv n_s v_s V^{-1} = \frac{x_s v_s \phi}{x_s v_s + (1 - x_s)v_b} \sim x_s \phi_c \frac{v_s}{v_b} \text{ as } x_s \to 0.
$$
\n
$$
(9)
$$

Moreover,

$$
\left(\frac{\partial \bar{V}_s}{\partial x_s}\right)_{x_s=0} = -2\left(1 - \frac{v_b}{v_s}\right)\phi_c^{-2}\left(\frac{\partial \phi}{\partial x_s}\right)_{x_s=0} + \dots
$$
\n
$$
2\frac{v_b}{v_s}\phi_c^{-3}\left(\frac{\partial \phi}{\partial x_s}\right)_{x_s=0}^2 - \frac{v_b}{v_s}\phi_c^{-2}\left(\frac{\partial^2 \phi}{\partial x_s^2}\right)_{x_s=0},\tag{10}
$$

as provided in the main text.

$a_s 2\pi/l_K$	$\bar V^0$	$\bar V^1_s$	$\partial \phi / \partial x_s  _{x_s = 0}$	$\partial^2 \phi / \partial x_s^2  _{x_s=0}$
0.322	0.98	7.03	0.57	$-2.65$
0.483	1.28	$-0.62$	1.52	-6.86
0.804	1.59	$-1.84$	5.12	$-60.7$
1.13	1.76	$-1.73$	11.0	-360
1.77	1.52	$-2.05$	59.0	$-6710$
2.57	1.44	$-2.56$	198	$-22400$
3.22	1.36	$-2.19$	419	$-250000$

Table 1: Sphere-chain packing at infinite sphere dilution:  $N = 21$ ;  $\phi(x_s = 0) \approx 0.416$ .

#### 4 Sphere-chain mixture density data

The figures and tables below summarise the principal experimental data ( $\phi$  versus  $x_s$  for various *N* and *as*) and various quantities derived from it, as detailed in the main text. Note that Redlich-Kister polynomials of the form

$$
\phi = \sum_{i=0}^{n} b_i (2x_s - 1)^i \tag{11}
$$

were fit to this data using least-squares minimisation, implemented by the Matlab function polyfit. Generally, setting  $n \leq 8$  furnished robust estimates of the Redlich-Kister coefficients  $b_i$  when fitting to data with  $x_s \lesssim 0.5$ . Accordingly,

$$
\phi(x_s = 0) = \sum_{i=0}^{n} b_i (-1)^i,
$$
\n(12)

$$
\left(\frac{\partial \phi}{\partial x_s}\right)_{x_s=0} = 2\sum_{i=1}^n ib_i(-1)^{i-1},\tag{13}
$$

$$
\left(\frac{\partial^2 \phi}{\partial x_s^2}\right)_{x_s=0} = 2^2 \sum_{i=2}^n i(i-1)b_i(-1)^{i-2}, \tag{14}
$$

which, in turn, furnish the equations for  $\bar{V}_s^0$  and  $\bar{V}_s^1$  in the main text.

$a_s 2\pi/l_K$	$\bar V^0_s$	$\bar V^1_s$	$\partial \phi / \partial x_s  _{x_s = 0}$	$\partial^2 \phi / \partial x_s^2  _{x_s=0}$
0.322	0.611	8.34	0.681	$-1.93$
0.483	1.14	0.116	1.69	$-8.58$
0.804	1.84	$-2.14$	4.06	$-41.0$
1.13	2.15	$-1.75$	9.32	$-250$
1.77	1.91	$-2.29$	39.0	$-2780$
2.57	1.58	$-3.17$	179	-4990
3.22	1.44	$-2.90$	398	$-135000$

Table 2: Same as table 1, but with  $N = 46$ ;  $\phi(x_s = 0) \approx 0.384$ .

Table 3: Same as table 1, but with  $N = 100$ ;  $\phi(x_s = 0) \approx 0.377$ .

$a_s 2\pi/l_K$	$\bar V^0_s$	$\bar V^1_s$	$\partial \phi / \partial x_s  _{x_s = 0}$	$\partial^2 \phi / \partial x_s^2  _{x_s=0}$
0.322	0.288	10.0	0.778	$-1.71$
0.483	1.04	1.03	1.79	$-10.7$
0.804	2.28	$-1.48$	1.89	$-10.8$
1.13	2.44	$-1.00$	3.08	$-26.2$
1.77	2.17	$-2.33$	26.5	$-1320$
2.57	1.79	$-3.00$	145	$-6500$
3.22	1.64	$-2.87$	333	$-134000$

Table 4: Same as table 1, but with  $N = 214$ ;  $\phi(x_s = 0) \approx 0.372$ .

$a_s 2\pi/l_K$	$\bar V^0_s$	$\bar V^1_s$	$\partial \phi / \partial x_s  _{x_s = 0}$	$\partial^2 \phi / \partial x_s^2  _{x_s=0}$
0.322	0.236	12.8	0.790	$-2.29$
0.483	1.06	0.987	1.75	$-10.4$
0.804	2.34	$-1.45$	1.76	$-9.31$
1.13	2.49	$-0.930$	2.69	$-19.7$
1.77	2.21	$-2.08$	25.7	$-307$
2.57	1.81	$-3.11$	145	$-5870$
3.22	1.65	$-2.90$	326	$-141000$



Figure 2: Same as figure 3b in the main text, but with  $N = 46$ .



Figure 3: Same as figure 3b in the main text, but with  $N = 100$ .



Figure 4: Same as figure 3b in the main text, but with  $N = 214$ .



Figure 5: Same as figure 3b in the main text, but with  $N = 1000$ .

Table 5: Same as table 1, but with  $N = 1000$ ;  $\phi(x_s = 0) \approx 0.367$ .<br> $a_s 2\pi/l_K$   $\bar{V}_s^0$   $\bar{V}_s^1$   $\partial \phi/\partial x_s|_{x_s=0}$   $\partial^2 \phi/\partial x_s^2|_{x_s=0}$  $a_s 2\pi/l_K$  $\bar{V}^1_s$  $\frac{\partial^2 \phi}{\partial x_s} \Big|_{x_s=0}$   $\frac{\partial^2 \phi}{\partial x_s^2} \Big|_{x_s=0}$ 0.322 0.140 14.9 0.806 -2.53 0.483 1.01 1.58 1.80 -11.6 0.804 2.39  $-1.43$   $1.65$   $-8.80$ 1.13 2.56 -0.811 2.21 -11.0  $1.77 \qquad \quad 2.24 \quad \ -2.00 \qquad \quad \quad 25.3 \qquad \qquad -1370$ 2.57 1.81 -3.23 146 -5230  $3.22 \qquad \quad 1.66 \quad \ -3.22 \qquad \quad \ 332 \qquad \quad \ -82500$